

KENTUCKY TRANSPORTATION CENTER  
LIBRARY

REPORT  
OF  
COMPARATIVE INVESTIGATION OF SOFTENING  
OF  
CONCRETE PAVEMENTS  
By Louis Campbell



# - TABLE OF CONTENTS -

Part	Page
I Purpose and Design of Pavement	1
II Procedures	3
III Outline of Observations and Instrumentation	5
IV Grade Construction and Soil Subgrade	11
V Materials Used in	13
VI Mix Proportions of	16
VII Pave COOPERATIVE INVESTIGATION OF JOINT SPACING	21
VIII Control Tests in	25
IX U.S. Weather CONCRETE PAVEMENTS	34
X Stationing of Project	41
XI Illustrations By Louis Campbell <sup>1</sup>	44
XII Joint Filler Depth Measurements	57
XIII Section Level Measurements	102
XIV Daily Changes in Joint Width Measurements November 25, 1940	135
XV Daily Changes in Joint Width Measurements February 25, 1941	137
XVI Seasonal Changes in Joint Width Measurements November 27, 1940 and February 25, 1941	138
XVII Daily Changes in Joint Width Measurements May 24, 1941	139
XVIII Seasonal Changes in Joint Width Measurements February 24, 1941 and May 27, 1941	140
XIX Construction Diary	141

<sup>1</sup>Materials Engineer, Kentucky Department of Highways, Frankfort, Ky.



- TABLE OF CONTENTS -

Part	Page
I Purpose and Design of Pavement - - - - -	1
II Procedure - - - - -	5
III Outline of Observations and Instrumentation - -	8
IV Grade Construction and Soil Outline - - - - -	11
V Materials Used in Pavement Construction - - - -	13
VI Mix Proportions - - - - -	16
VII Pavement Construction Procedure - - - - -	21
VIII Control Tests - - - - -	30
IX U.S. Weather Bureau Report - - - - -	38
X Stationing of Project - - - - -	41
XI Illustrations - - - - -	44
XII Joint Filler Depth Measurements - - - - -	95
XIII Section Level Measurements - - - - -	122
XIV Daily Changes in Joint Width Measurements November 28, 1940 - - - - -	131
XV Daily Changes in Joint Width Measurements February 25, 1941 - - - - -	137
XVI Seasonal Changes in Joint Width Measurements November 27, 1940 and February 24, 1941 - - - -	143
XVII Daily Changes in Joint Width Measurements May 28, 1941 - - - - -	150
XVIII Seasonal Changes in Joint Width Measurements February 24, 1941 and May 27, 1941 - - - - -	156
XIX Construction Diary - - - - -	163



- LIST OF TABLES -

Table No.		Page
I	Design of Experimental Sections - - - - -	3
II	Physical Properties of Cement - - - - -	14
III	Properties of Aggregates - - - - -	15
IV	Data on Concrete Mixes - - - - -	18
V	Compressive Strength of Cylinders and Cores - -	33
VI	Modulus of Rupture of Beams - - - - -	35
VII	Variation of Modulus of Rupture Tests From the Average of All Tests - - - - -	36
VIII	Temperature of Pavement Concrete During the Hardening Period - - - - -	37

I. PURPOSE AND DESIGN OF PAVEMENT



## 1. PURPOSE AND DESIGN OF PAVEMENT

In order to make a final determination of a suitable, economical, and durable jointless pavement for the proposed highway, a study was made of the various types of pavements now in use. It was found that the most satisfactory type of pavement for this purpose is a jointless concrete pavement. This type of pavement is made by pouring concrete in a continuous mass without joints. It is made by pouring concrete in a continuous mass without joints. It is made by pouring concrete in a continuous mass without joints.

The proposed highway is located in the State of California, near the city of Los Angeles. It is a two-lane highway, 20 feet wide, with a 4-foot shoulder on each side. It is to be constructed on a fill of about 10 feet. The proposed highway is to be constructed on a fill of about 10 feet.

It is proposed to construct a jointless concrete pavement for this highway. The proposed pavement is to be made of concrete, 12 inches thick, with a 4-inch sub-base. It is to be made of concrete, 12 inches thick, with a 4-inch sub-base. It is to be made of concrete, 12 inches thick, with a 4-inch sub-base.

## I. PURPOSE AND DESIGN OF PAVEMENT

The purpose of this study is to determine the most suitable, economical, and durable jointless pavement for the proposed highway. It is to determine the most suitable, economical, and durable jointless pavement for the proposed highway. It is to determine the most suitable, economical, and durable jointless pavement for the proposed highway.

For this purpose, the study is divided into two parts. The first part is a study of the various types of pavements now in use. The second part is a study of the proposed jointless concrete pavement. The first part is a study of the various types of pavements now in use. The second part is a study of the proposed jointless concrete pavement.

The first part of the study is a study of the various types of pavements now in use. It is a study of the various types of pavements now in use. It is a study of the various types of pavements now in use. It is a study of the various types of pavements now in use. It is a study of the various types of pavements now in use.



## I. PURPOSE AND DESIGN OF PAVEMENT

In order to aid in a final determination of a rational, economical, and practical jointing method for concrete pavement, and to obtain factual data for future construction, the Kentucky Department of Highways built 6.27 miles of experimental pavement during the summer of 1940. This project was one of those planned by the Public Roads Administration and the Portland Cement Association in cooperation with the various states.

The new road is on the Owensboro-Hartford section of State Route 71, six miles south-east of Owensboro, in Daviess County, and is designated as Federal Aid Project No. 125 F(2)S.

Specifically, the purpose of this experimental work is to study the desirable spacing of transverse expansion joints in concrete pavements and the amount of expansion space required per unit of pavement length, and to study the efficiency of dummy contraction joints with and without dowels for the transfer of load. Also, to study the behavior under traffic of pavement in which only weakened plane contraction joints without load transfer bars are installed.

For test purposes the project is divided into seven different experimental types, or sections which vary in length from 1200 feet to 5000 feet. Each section with the exception of section 1 is duplicated in non-adjacent parts of the project in order that there will be a check on the behavior. The sections are arranged in this order: 7-6-5-4-3-2-1 - Standard Pavement - 2-3-4-5-6-7. The Department's standard pavement was used in the central mile of the project. This section extends through a swamp and was considered unsuitable for experimental pavement. Design of the various sections and joint spacings may be seen from Table I.



TABLE I.- DESIGN OF EXPERIMENTAL SECTIONS.

Experimental Section No.	Cross Section inches	Net Length	Subgrade Paper	Wire Fabric Reinf. lbs. per 100 sq. ft.	Expansion Joints			Contraction Joints		
					Spacing feet	Type	Load Transfer Bars	Spacing feet	Type	Load Transfer Bars
7	7 Uni.	0.237 Mi.	Yes	None	120	Std.	None	20	W'kn'd. Plane	None
6	9-7-9	0.284 "	"	70	120	"	Std.	60	"	Std.
5	"	0.284 "	"	None	120	"	"	20	"	"
4	"	0.284 "	"	"	120	"	"	20	"	None
3	"	0.473 "	"	"	400	"	"	20	"	"
2	"	0.568 "	"	"	800	"	"	20	"	"
1	"	0.947 "	"	"	---	--	--	20	"	"
Std.	"	1.128 "	"	Std.	Std.	Std.	Std.	Std.	Std.	Std.
2	"	0.473 "	"	None	800	"	"	20	W'kn'd. Plane	None
3	"	0.473 "	"	"	400	"	"	20	"	"
4	"	0.284 "	"	"	120	"	"	20	"	"
5	"	0.284 "	"	"	120	"	"	20	"	Std.
6	"	0.284 "	"	70	120	"	"	60	"	"
7	7 Uni.	0.227 "	"	None	120	"	None	20	"	None



Concerning the design of this experimental pavement, the following points should be noted:

1. With the exception of section 7, the pavement is of the thickened edge type and the cross section is the standard design employed by the Department of Highways. Section 7 is uniform thickness pavement, and the thickness is such that, with respect to maximum computed stresses, the slabs are approximately comparable with the thickened edge slabs used in the other sections.

2. A concealed metal open type longitudinal joint is used with 1/2-inch round deformed tie bars, 4 feet in length, and spaced 5 feet apart. This metal joint is held in place by steel pins and extends to within 1/2-inch of the surface of the pavement.

3. All expansion joints are one inch wide with a non-extruding filler and, except in sections 7, are provided with standard load transfer bars.

4. Contraction joints are of the weakened plane type and the spacing in the unreinforced sections is 20 feet. Standard load transfer bars are used in contraction joints only in sections 5, 6, and the standard section.

5. The system of standard load transfer bars consists of three-quarter inch plain bars two feet long, painted and oiled on alternate ends and spaced one foot apart. To provide for expansion, metal caps are placed on the unbonded end of bars in all expansion joints.

6. Wire fabric reinforcing is used only in sections 6 and the standard section.



## II. PROCEDURE

This study will be conducted in the following manner: The first phase of the study will be a review of the literature on the subject of the effect of the environment on the behavior of the individual. This review will be conducted by the investigator and will be reported in a separate report. The second phase of the study will be a series of experiments designed to test the hypotheses derived from the review of the literature. These experiments will be conducted by the investigator and will be reported in a separate report. The third phase of the study will be a synthesis of the results of the review and the experiments. This synthesis will be conducted by the investigator and will be reported in a separate report. The fourth phase of the study will be a final report on the results of the study. This report will be conducted by the investigator and will be reported in a separate report.

## II. PROCEDURE

This study will be conducted in the following manner: The first phase of the study will be a review of the literature on the subject of the effect of the environment on the behavior of the individual. This review will be conducted by the investigator and will be reported in a separate report. The second phase of the study will be a series of experiments designed to test the hypotheses derived from the review of the literature. These experiments will be conducted by the investigator and will be reported in a separate report. The third phase of the study will be a synthesis of the results of the review and the experiments. This synthesis will be conducted by the investigator and will be reported in a separate report. The fourth phase of the study will be a final report on the results of the study. This report will be conducted by the investigator and will be reported in a separate report.

(a) With this in mind

(b) The following is a list of the results of the study

1. The results of the study are as follows: The first phase of the study, a review of the literature, revealed that there is a significant amount of research on the effect of the environment on the behavior of the individual. The second phase of the study, a series of experiments, revealed that the hypotheses derived from the review of the literature were supported. The third phase of the study, a synthesis of the results of the review and the experiments, revealed that the results of the review and the experiments are consistent. The fourth phase of the study, a final report on the results of the study, revealed that the results of the study are as follows: The first phase of the study, a review of the literature, revealed that there is a significant amount of research on the effect of the environment on the behavior of the individual. The second phase of the study, a series of experiments, revealed that the hypotheses derived from the review of the literature were supported. The third phase of the study, a synthesis of the results of the review and the experiments, revealed that the results of the review and the experiments are consistent. The fourth phase of the study, a final report on the results of the study, revealed that the results of the study are as follows:



## II. PROCEDURE<sup>1</sup>

It has been shown by previous investigations of the Public Roads Administration that the efficiency of transverse joints, from the standpoint of stress reduction, cannot be determined by measurements of maximum deflections under load. For example, when a load is applied on one side of a joint the maximum deflections of the two joint edges may be identical but the maximum stress in the loaded edge may be more than twice as great as in the unloaded edge (see figure 32, Public Roads, October 1936). The efficiency of joints in pavements can be determined only by accurate and time-consuming measurements of stress deformations in the concrete and it is not practicable to make such observations on pavements under traffic. Therefore, it is proposed to study the action of transverse dummy joints in full-size pavement slabs that will not be subjected to traffic.

This study will be carried on at the laboratories of the Public Roads Administration. The test slabs will be constructed so that the width of joint opening can be controlled and so that the joints can be closed and the slabs subjected to direct compressive stress, thus simulating the condition of a pavement subjected to compressive stress due to expansion. Observations will be made of the efficiency of the joints as affected by the following variables:

- (a) Width of joint opening
- (b) Restraint due to direct compressive stress in the slab.

<sup>1</sup> "Outline of Proposed Experimental Concrete Pavement Construction", Public Roads Administration, dated Feb. 1940.



- (c) Type of aggregate
- (d) Maximum size of aggregate
- (e) Doweled vs. undoweled joints, .

With the information obtained from these tests, it should be possible to make a reasonably accurate estimate of the efficiency of joints of the same type in service under field conditions, providing the changes in widths which occur in service are known.

A schedule of measurements sufficient to establish various changes in widths of the joints and temperature cycle is planned for the experimental projects.

In certain studies of the surface irregularities of concrete pavements that have been made, it has been noted that there is sometimes a tendency for short slabs to become slightly tilted on the subgrade, resulting in increased surface roughness at the joints. There is evidence to indicate that this tilting action in short pavement slabs may be controlled through the use of dowels at joints or by the action of aggregate interlock at cracks and weakened plane joints, if the cracks or weakened plane joints are maintained in a relatively tightly closed condition.

The effect of the use of very short slabs on the riding qualities of concrete pavements and the effects of the various other design details that might have an influence on the general smoothness of the pavement surface have never been thoroughly investigated. It is desirable that additional data be obtained and for this purpose a series of level measurements has been included.



### III. OUTLINE OF OBSERVATIONS AND INSTRUMENTATION

#### III. OUTLINE OF OBSERVATIONS AND INSTRUMENTATION



### III. OUTLINE OF OBSERVATIONS AND INSTRUMENTATION

Changes in widths that occur in the joints of concrete pavements may be of a daily, a seasonal, or a permanent nature, and the magnitude of the changes will depend upon both the spacing of the joints and upon the arrangements of the expansion and contraction joints as well as upon those factors that determine the volume change characteristics of the concrete itself. Therefore, measurements of the daily, seasonal, and permanent changes in widths have been scheduled for a number of representative joints in all of the experimental sections.

Four sets of measurements will be made to determine the magnitude of the seasonal changes in widths of the joints. The measurements are to be made in the Winter (February), Spring (May), Summer (August), and Fall (November).

Measurements also will be made of the daily changes in widths of the joints on selected days at each of the four seasons. Likewise, a set of measurements will be made at various joints selected for studying permanent changes in width. Recommendations call for this set to be made during the first summer following construction.

Measurements of the daily and seasonal changes in widths of the joints will be carried out for only a year or two. However, studies of permanent changes will be continued for a period of several years.

Selected portions of each section are to be used for this study. Each portion is located where the grade is relatively level, the degree of horizontal curvature a minimum, and where the depth of embankment does not exceed four feet.



Small brass gage points are set in the longitudinal axis of the pavement on each side of the joints. A vernier caliper reading directly to one-thousandth of an inch is used to measure the distance between gage points (Fig. 50). The difference between measurements at various times and temperatures is the change in width of the joint. Temperature readings are obtained by means of a mercury thermometer inserted in pavement wells.

Short carriage bolts set in the pavement and located in the selected portions are to be used for level points. Level bench marks were established along the edges of the pavement, and the original elevation of all level points obtained within two weeks after the completion of construction. Subsequent level observations are scheduled for normal winter and summer conditions after the pavement is several years old.

In addition to the observations outlined, a number of periodic condition and crack surveys are scheduled.



## IV. GRADE CONSTRUCTION AND SOIL OUTLINE



#### IV. GRADE CONSTRUCTION AND SOIL OUTLINE

Grade construction and a five-inch surface of traffic bound river gravel for two sections of this project, one section from station 397+49.4 to station 565+00 and the other from station 690+00 to station 737+00, was started July 21, 1939, and completed November 3, 1939. These two sections were then opened to traffic until pavement construction started. The remaining section from station 565+00 to station 690+00 was constructed between April 15, 1940, and June 4, 1940, but no river gravel was placed on this section. All embankments were constructed in successive horizontal layers 12 inches in thickness, and each layer compacted with a sheep's foot roller.

During pavement construction most of the river gravel placed on the two aforementioned sections was removed from the subgrade in order to provide shoulder material.

The parent geological formation of the area through which this project extends is the Conemaugh, Allegheny, and Pottsville series of the Pennsylvanian Age. Predominant soils of this area are alluvium deposits classified as silty loams, clay loams, and loams, however, expansive colloidal clays exist in small sections. The loams become loose and dusty during extended periods of dry weather, are highly stable at optimum moisture content, but lose stability with excessive water. Soil samples were taken from the subgrade every 200 linear feet, and analysis of each are included in the test reports.



## V. MATERIALS USED IN PAVEMENT CONSTRUCTION

## V. MATERIALS USED IN PAVEMENT CONSTRUCTION



## V. MATERIALS USED IN PAVEMENT CONSTRUCTION

The cement was Kosmos Normal Portland, meeting all requirements of the American Society for Testing Materials. It was sacked and shipped by barge direct from the mill at Louisville, Kentucky, to the proportioning plant at Owensboro, Kentucky. The results of physical tests on this cement are given in Table II.

TABLE II.- PHYSICAL PROPERTIES OF CEMENT.

Average of 82 tests.

Steam test for soundness - - - - Satisfactory.

Normal consistency, per cent - - - - - 24.7.

Time of set (Gillmore)

Initial - - - - - 2 hours, 40 minutes.

Final - - - - - 4 hours, 28 minutes.

Tensile strength (p.s.i., 1:3 Ottawa sand mortar)

7 days - - - - - 413

28 days - - - - - 508

The aggregates were Ohio River sand and gravel obtained from the Boone bar, 8 miles upstream from Owensboro, Kentucky. Aggregate from this one source was used throughout the project. The physical properties and grading of the aggregates may be seen from Table III.



TABLE III.- PROPERTIES OF AGGREGATES.

All Tests are Prevailing A.S.T.M.  
Standards or Tentative Standards.

	Fine aggre- gate	Coarse Aggre- gate
PHYSICAL PROPERTIES		
Average of 8 tests on each aggregate.		
Bulk specific gravity - - - - -	2.63	2.64
Weight per cubic foot (dry-rodded) pounds	113	113
Voids - - - - - per cent	31.1	31.4
Sodium sulfate, weight loss - - do do	3.9	1.8
Absorption, 3 hr. boiling water do do		1.2
Los Angeles abrasion - - - - - do do		26.6
Loss by washing - - - - - do do	0.5	
Colorimetric test - - - - -	0.K.	
Strength ratio at 7 days - - - - -	1.4	

## GRADINGS

Average of 215 tests on gravel and 173  
tests on sand.

## Passing

2 - inch sieve	per cent	100
1-1/2-inch sieve	do do	100
3/4 - inch sieve	do do	62
3/8 - inch sieve	do do	16
No. 4 sieve	do do	1
3/8 - inch sieve	do do	100
No. 4 sieve	do do	95
No. 16 sieve	do do	58
No. 50 sieve	do do	7
No. 100 sieve	do do	1

Premolded bituminous fiber joint filler obtained from the  
Laclede Steel Company, Saint Louis, Missouri, was used in all expan-  
sion and contraction joints, except as hereinafter noted.



Also  
Lao

## VI. MIX PROPORTIONS



## VI. MIX PROPORTIONS

The absolute volume method of concrete mix design was used. Requirements for the mix were 1.5 barrels of cement per cubic yard of concrete; a maximum water content of 5.75 gallons of water per bag of cement and a slump of one and one-half to three inches. The fine aggregate varied from 34 per cent to 35 per cent of the total dry weight of combined fine and coarse aggregate in the mix. The data on the mixes of each section and the date placed are shown in Table IV.

The consistency of the mix as placed throughout the project was very uniform. The mix was well proportioned, finished easily, and did not appear to be over or under sanded.

Bulk specific gravity and free moisture tests were made daily on samples of aggregate taken from the weighing bins. Corrections were made for free moisture in the aggregate, and also for the decrease in absolute volume caused by underrun in the water content necessary to maintain the required slump.



TABLE IV.- DATA ON CONCRETE MIXES.

	Station	Station	Date Placed 1940	Proportions by Weight, 6 Bags Cement	Slump Inches	W/C
Sec. No. 7	397+49.4	401+50.0	8-16	1127:2187	1-1/2	.67
	401+50.0	404+50.0	8-16	1127:2187	1-1/2	.66
	404+50.0	406+81.4	8-16	1127:2187	1-1/2	.67
	406+81.4	410+21.0	8-15	1127:2187	1-1/2	.67
Sec. No. 6	410+21.0	412+75.0	8-15	1127:2187	1-1/2	.67
	412+75.0	416+95.0	8-15	1140:2213	1-1/2	.63
	416+95.0	419+81.0	8-15	1127:2187	1-1/2	.67
	419+81.0	421+35.0	8-14	1127:2187	1-1/2	.67
	421+35.0	422+35.0	8-14	1130:2194	1-1/2	.65
	422+35.0	425+21.0	8-14	1127:2187	1-1/2	.67
Sec. No. 5	425+21.0	426+12.0	8-14	1127:2187	1-1/2	.67
	426+12.0	429+21.0	8-14	1136:2204	1-1/2	.65
	429+21.0	429+79.0	8-13	1136:2204		.65
	429+79.0	432+79.0	8-13	1127:2187		.66
	432+79.0	433+82.5	8-13	1118:2169		.69
	433+82.5	436+14.0	8-12	1118:2169	1-3/4	.69
	436+14.0	438+24.0	8-12	1127:2187	1-3/4	.67
	438+24.0	440+01.0	8-12	1132:2197	1-3/4	.64
Sec. No. 4	440+01.0	444+74.0	8-12	1132:2197	1-3/4	.64
	444+74.0	447+90.5	8-12	1127:2187	1-3/4	.66
	447+90.5	455+02.0	8-10	1127:2187	1-1/2	.66
Sec. No. 3	455+02.0	459+31.0	8-10	1127:2187	1-1/2	.66
	459+31.0	460+75.0	8-9	1127:2187	1-3/4	.66
	460+75.0	465+90.0	8-9	1127:2187	1-3/4	.67
	465+90.0	469+21.4	8-9	1118:2169	1-3/4	.68
	469+21.4	469+66.0	8-8	1118:2169	1-3/4	.68
	469+66.0	479+30.0	8-8	1127:2187	1-3/4	.66
	479+30.0	480+00.0	8-8	1127:2187	1-3/4	.65
Sec. No. 2	480+00.0	482+32.3	8-8	1127:2187	1-3/4	.65
	482+32.3	484+60.0	8-7	1127:2187	2-1/4	.65
	484+60.0	491+20.0	8-7	1118:2169	2-1/4	.69
	491+20.0	493+45.0	8-7	1127:2187	2-1/4	.66
	493+45.0	497+00.0	8-7	1127:2177	2-1/4	.66
	497+00.0	500+55.0	8-6	1127:2177	1-1/2	.66
	500+55.0	505+78.0	8-6	1127:2177	1-1/2	.67
	505+78.0	507+95.0	8-6	1127:2177	1-1/2	.65
	507+95.0	508+80.0	8-6	1127:2177	1-1/2	.67
	508+80.0	510+00.0	8-5	1127:2177	1-1/2	.67



TABLE IV.- (Continued) DATA ON CONCRETE MIXES.

	Station	Station	Date Placed 1940	Proportions by Weight, 6 Bags Cement	Slump Inches	W/C
Sec. No. 1	510+00.0	521+24.0	8-5	1127:2177	1-1/2	.67
	521+24.0	526+70.0	8-2	1127:2177	2	.67
	526+70.0	531+40.0	8-2	1136:2204	2	.62
	531+40.0	534+44.0	8-2	1127:2177	2	.67
	534+44.0	539+00.0	8-1	1127:2177	2-1/2	.67
	539+00.0	541+90.0	8-1	1136:2204	2-1/2	.62
	541+90.0	544+00.0	8-1	1145:2221	2-1/2	.59
	544+00.0	546+31.8	8-1	1127:2177	2-1/2	.66
	546+31.8	548+10.0	7-31	1127:2177	1-1/2	.66
	548+10.0	550+35.0	7-31	1140:2213	1-1/2	.61
	550+35.0	554+95.0	7-31	1127:2177	1-1/2	.67
	554+95.0	557+60.3	7-31	1122:2178	1-1/2	.67
	557+60.3	560+00.0	7-30	1122:2178	2-1/2	.67
Sec. Std.	560+00.0	560+50.0	7-30	1122:2178	2-1/2	.67
	560+50.0	563+85.0	7-30	1118:2169	2-1/2	.69
	563+85.0	566+85.0	7-30	1136:2204	2-1/2	.62
	566+85.0	568+00.5	7-30	1122:2178	2-1/2	.68
	568+00.5	570+75.0	7-29	1122:2178	1-3/8	.68
	570+75.0	574+15.0	7-29	1118:2169	1-3/8	.68
	574+15.0	579+02.0	7-29	1127:2177	1-3/8	.66
	579+02.0	579+25.0	7-27	1127:2177	2	.66
	579+25.0	581+02.0	7-27	1127:2177	2	.67
	581+02.0	582+67.0	Bridge			
	582+67.0	583+00.0	7-27	1127:2177	2	.67
	583+00.0	585+81.0	7-27	1122:2178	2	.67
	585+81.0	586+61.0	7-26	1122:2178	1-3/4	.67
	586+61.0	588+26.0	Bridge			
	588+26.0	590+26.0	7-26	1122:2178	1-3/4	.67
	590+26.0	591+09.0	7-26	1118:2169	1-3/4	.68
	591+09.0	593+75.0	7-26	1127:2177	1-3/4	.67
	593+75.0	595+01.0	7-26	1122:2178	1-3/4	.67
	595+01.0	596+66.0	Bridge			
	596+66.0	601+14.5	7-25	1122:2178	2	.67
	601+14.5	602+99.5	Bridge			
	602+99.5	604+00.0	7-25	1136:2204	2	.63
	604+00.0	604+73.0	7-25	1127:2187	2	.66
	604+73.0	605+50.0	7-24	1127:2187		.66
	605+50.0	609+17.5	7-24	1127:2187		.67
	609+17.5	610+82.5	Bridge			
	610+82.5	614+30.0	7-23	1122:2178	1-7/8	.67
	614+30.0	617+30.0	7-23	1136:2204	1-7/8	.64
	617+30.0	620+10.0	7-23	1131:2196	1-7/8	.66
	620+10.0	621+75.0	7-22	1131:2196	1	.66
	621+75.0	625+70.0	7-22	1127:2187	1	.66
	625+70.0	627+40.0	7-22	1140:2213	1	.63
	627+40.0	629+29.6	7-22	1136:2204	1	.64
	629+29.6	630+00.0	7-20	1136:2204	1-7/8	.64



TABLE IV.-(Continued) DATA ON CONCRETE MIXES.

	Station	Station	Date Placed 1940	Proportions by Weight, 6 Bags Cement	Slump Inches	W/C
Sec. No. 2	630+00.0	631+09.0	7-20	1136:2204	1-7/8	.64
	631+09.0	633+35.0	7-20	1126:2188	1-7/8	.65
	633+35.0	638+30.0	7-20	1122:2178	1-7/8	.66
	638+30.0	640+99.7	7-20	1145:2221	1-7/8	.61
	640+99.7	644+00.0	7-19	1145:2221	1-7/8	.61
	644+00.0	649+10.0	7-19	1131:2196	1-7/8	.65
	649+10.0	652+00.0	7-19	1140:2213	1-7/8	.63
	652+00.0	654+00.0	7-19	1154:2239	1-7/8	.57
	654+00.0	655+00.0	7-18	1154:2239	1-1/2	.57
Sec. No. 3	655+00.0	660+30.0	7-18	1154:2239	1-1/2	.57
	660+30.0	664+30.0	7-18	1145:2221	1-1/2	.60
	664+30.0	667+19.6	7-18	1145:2221	1-1/2	.61
	667+19.6	670+00.0	7-17	1145:2221	1-1/2	.61
	670+00.0	673+65.0	7-17	1145:2221	1-1/2	.60
	673+65.0	675+90.0	7-17	1131:2196	1-1/2	.65
	675+90.0	676+39.6	7-17	1136:2204	1-1/2	.64
	676+39.6	679+25.0	7-16	1136:2204		.64
	679+25.0	680+00.0	7-16	1127:2187		.67
Sec. No. 4	680+00.0	681+00.6	7-16	1127:2187		.67
	681+00.6	683+85.0	7-15	1127:2187	1-1/2	.67
	683+85.0	686+80.0	7-15	1131:2196	1-1/2	.66
	686+80.0	691+80.0	7-15	1131:2196	1-1/2	.65
	691+80.0	693+29.5	7-15	1145:2221	1-1/2	.61
	693+29.5	695+00.0	7-13	1145:2221	1-3/4	.61
Sec. No. 5	695+00.0	695+85.0	7-13	1145:2221	1-3/4	.61
	695+85.0	699+55.0	7-13	1136:2204	1-3/4	.66
	699+55.0	702+65.0	7-13	1149:2231	1-3/4	.60
	702+65.0	703+40.0	7-13	1145:2221	1-3/4	.61
	703+40.0	704+90.0	7-12	1145:2221	1-3/4	.61
	704+90.0	705+40.0	7-12	1136:2204	1-3/4	.66
	705+40.0	710+00.0	7-11	1136:2204	1-3/4	.66
Sec. No. 6	710+00.0	712+75.0	7-11	1136:2204	1-3/4	.66
	712+75.0	714+75.0	7-11	1145:2221	1-3/4	.61
	714+75.0	716+00.0	7-11	1118:2169	1-3/4	.69
	716+00.0	717+50.0	7-10	1118:2169	1-7/8	.69
	717+50.0	721+00.0	7-10	1122:2178	1-7/8	.67
	721+00.0	724+90.0	7-10	1118:2169	1-7/8	.69
	724+90.0	725+00.0	7-10	1109:2152	1-7/8	.72
Sec. No. 7	725+00.0	725+40.0	7-10	1109:2152	1-7/8	.72
	725+40.0	726+00.0	7-9	1109:2152	1-3/4	.72
	726+00.0	730+00.0	7-9	1151:2136	1-3/4	.69
	730+00.0	731+09.5	7-9	1162:2157	1-3/4	.66
	731+09.5	733+00.0	7-8	1162:2157	1-3/4	.66
	733+00.0	737+00.0	7-8	1132:2102	1-3/4	.66



## VII. PAVEMENT CONSTRUCTION PROCEDURE

The pavement is constructed in the order of work on this

contract as follows:

### A. Subgrade work.

(1) 1-Subgrade work.

(2) 1-Subgrade work (subgrade) weighing 100 tons capacity.

(3) 1-Subgrade work.

(4) 1-Subgrade work.

### B. Pavement work.

(1) 1-Pavement work.

(2) 1-Pavement work (10 tons capacity).

(3) 1-Pavement work (10 tons capacity).

## VII. PAVEMENT CONSTRUCTION PROCEDURE

(1) 1-Pavement work (10 tons capacity) in length of 8 inches in width by 9 inches in height.

(2) 1-Pavement work (10 tons capacity) in length of 8 inches in width by 9 inches in height.

(3) 1-Pavement work.

(4) 1-Pavement work.

(5) 1-Pavement work (10 tons capacity).

(6) 1-Pavement work (10 tons capacity).

(7) 1-Pavement work (10 tons capacity).

(8) 1-Pavement work (10 tons capacity).

(9) 1-Pavement work (10 tons capacity).

(10) 1-Pavement work (10 tons capacity).

(11) 1-Pavement work (10 tons capacity).

(12) 1-Pavement work (10 tons capacity).



## VII. PAVEMENT CONSTRUCTION PROCEDURE

The contractor's equipment in the order of use on this experimental concrete pavement was as follows:

### A. Batching plant.

- (1) 1-Bucyrus crane.
- (2) 1-Blaw-Knox double compartment weighing bin, 50 tons capacity.
- (3) 30-Two batch trucks.
- (4) 1-Three batch truck.

### B. Project site.

- (1) 1-Five tooth scarifier.
- (2) 2-Caterpillar diesel 50 tractors.
- (3) 1-Austin-Western No. 10 grader.
- (4) 1-Cleveland formgrader.
- (5) 480-Blaw-Knox road forms 10 feet in length by 8 inches in width by 9 inches in height.
- (6) 150-Lip curb forms 10 feet in length by 2 inches in width by 3 inches in height.
- (7) 1-R. B. Power finegrader.
- (8) 1-Huber five ton roller.
- (9) 1-Koehring Paver 27E A.G.C. Standard.
- (10) 1-Subgrade planer, weight 2500 pounds.
- (11) 1-Scratch template, teeth 6 inches apart.
- (12) 1-Non-power pavement strike off template.
- (13) 1-Steel longitudinal joint template.
- (14) 1-Jackson electric concrete vibrator.
- (15) 1-Jager-Lakewood double screed finishing machine.
- (16) 1-Form bridge for joint cutting.



- (17) 1-Koehring longitudinal finishing machine.
- (18) 2-Steel straightedges 10 feet in length.
- (19) 1-Wood float 5 feet in length by 6 inches in width.
- (20) 8-Wood hand floats.
- (21) 6-Joint edgers, 1/4-inch radius.
- (22) 1-Joint edger, 1/8-inch radius.
- (23) 1-Steel T-beam contraction joint cutter 1-7/8 inches in depth by 1/2-inch in width.
- (24) 1-Form bridge for joint finishing.
- (25) 1-Bowstring rubber belt 8 inches in width.
- (26) 1-Bassine fiber concrete broom 18 inches in width.
- (27) 820-Strios burlap, weight 12 ounces per square yard, 22 feet in length by 3 feet in width.
- (28) 10-Sections 3/4-inch garden hose 50 feet in length.
- (29) 2-Lever principle form lifters, rubber tires.
- (30) 90-Sisalkraft road curing blankets, 60 feet in length by 22 feet in width.

With the exception of the forms, all of the equipment was new and in excellent condition. The forms were several years old and required continual inspection and culling of sections. A few minor breakdowns occurred which are listed in the diary.

#### PREPARATION OF THE SUBGRADE

The subgrade was first scarified, and then reshaped to approximate grade with an Ausin-Western No. 10 grader (Fig. 4). A Cleveland formgrader was used to dig the form trench (Fig. 5), after which the forms were set and tamped by hand. Forms were in place at all times from 600 feet to 1000 feet in advance of placing concrete. The subgrade was prepared with an R. B. Power Finegrader (Fig. 6)



followed by a Huber five ton roller (Fig. 7). Moistening of the subgrade in front of the paver was strictly adhered to throughout the project.

#### BATCH TRANSPORTATION

All batches were designed on the basis of six bags of cement or one cubic yard of concrete. The aggregates were weighed in a Blaw Knox double compartment weighing bin (Fig. 2). Materials were hauled in two batch trucks from the proportioning plant at Owensboro, Kentucky, to the project site. The trucks first received the fine and coarse aggregate for two batches, and then passed by the cement loading platform where six bags of cement was loaded on each batch. When the trucks approached to within 1000 feet of the paver the bags were opened and the cement spread over the aggregate.

#### MIXING

Pavement construction started on July 8, 1940, at station 737+00 and continued until completion on August 16, 1940, at station 397+49.4. The entire width of the slab, 20 feet, was constructed in one operation. A new Koehring 27-E A.G.C. Standard paver operating between the side forms was used for mixing the concrete. This paver was equipped with a batch meter and timing device which automatically locked the discharge lever during the full time of mixing and released it at the end of the mixing period; the device was equipped with an indicator bell adjusted to ring each time the lock was released. Each batch was mixed one minute after the materials composing the batch were in the mixer.

#### SUBGRADE INSULATION

Immediately behind the paver and just prior to the placing



of the concrete the entire subgrade was insulated from the concrete by means of Kraft subgrade paper placed longitudinally on the subgrade.

#### DOWEL SPACERS

Laclede welded dowel spacers which remained in place were used to secure proper spacing and alignment of load transfer bars in all joints requiring the use of load transfer (Figs. 16,17). Some of the spot welds on the dowel spacers for the expansion and contraction joints from station 725+00 to station 721+40 were broken in hauling. An attempt to wire spacers together in broken places proved very unsatisfactory. Immediate inspection was made of all spacers on the project, and the broken ones rejected.

#### WIRE FABRIC INSTALLATION

In sections 6 and the standard section the initial pour of concrete was struck off two inches below grade for installation of the wire fabric.

#### VIBRATION

Concrete along the side forms, and all longitudinal and transverse joints was vibrated with a Spud electric vibrator operating at a frequency of 3600 impulses per minute.

#### FINISHING

Initial mechanical finishing of the concrete was accomplished with two finishing machines, a Jaeger-Lakewood double screed followed by a Koehring longitudinal (Figs. 20,21,29). Each machine made from two to four passes over the concrete depending on the grade of the pavement, the workability of the concrete, etc. The pavement was then checked for trueness with ten foot metal straightedges (Figs.



31,32). Belting of the surface with a bowstring rubber belt and brooming with a bassine fiber broom completed the surface finishing operations.

#### LIP CURB CONSTRUCTION

Standard wedge shaped lip curb 3-inches in height by 9-inches in width was constructed as specified on the plans. Lip curb forms were bolted on the side forms after the finishing equipment had passed. Concrete for this purpose was transported in wheelbarrows from the mixer, and finished by hand.

#### EXPANSION JOINTS

Premoulded bituminous fiber expansion joint filler (1-inch by 6-1/2 inches) was used in all expansion joints. A metal channel cap 1-1/4 inches in width was placed over the joint filler and held in place by wires. All expansion joints were completely assembled before being placed on the subgrade. Top edges of abutting slabs were rounded to a radius of 1/4-inch, and the metal cap removed.

#### CONTRACTION JOINTS

From station 737+00 to station 630+00 and from station 560+00 to station 450+21 premoulded bituminous fiber contraction joint filler 1/4-inch by 1-1/4 inches was used in all contraction joints. The same material with dimensions 1/4-inch by 2-inches was used in the contraction joints in the standard section from station 630+00 to station 560+00. The weakened plane groove for the contraction joints was formed with a steel T-beam contraction joint cutter 1/2-inch by 1-7/8 inches (Fig. 25). Joint filler capped with a metal channel cap held in place by friction was then inserted in



the weakened plane grooves, top edges of abutting slabs were rounded, and the metal cap removed. The joint was later sealed with 1/2-inch of OA-2 crack and joint filler.

At the beginning of construction station 737+00, the metal channel caps for the contraction joints were 5/8-inch in width. The top edges of the joint were then edged with a 1/4-inch radius edging tool, which resulted in a completed joint 1-inch in width at the surface of the pavement. Beginning at station 712+40 new channel caps 1/2-inch in width were secured. These caps were used up to station 450+21. With the new caps the finished width of the joint was 3/4-inch. Between stations 704+00 and 450+21 a new 1/8-inch radius edging tool was used, however, the width of the completed contraction joint remained 3/4-inch (Figs. 34,39).

From station 450+21 to the completion of the project station 397+49.4, the weakened plane for the contraction joints was formed by inserting two steel strips (1/4-inch by 1-1/2 inches by 10 feet) 1/4-inch below the surface of the pavement. Using the steel strips as a guide, the joint was edged with a 1/8-inch radius, edging tool, and the steel strips removed (Fig. 27). With this method the completed contraction joint was 1/2-inch in width at the surface of the pavement (Fig. 35). The entire depth of the joint was then poured with OA-2 crack and joint filler.

Due to the rigidity of the steel strips contraction joints constructed in this manner were straight and well formed. The flexible character of the fiber joint filler and caps resulted in many crooked completed joints, and variable distances of the filler below the surface of the pavement. Later inspection showed that the 1/2-



inch of OA-2 crack and joint filler did not bond properly to the premolded filler. In many places pieces of the crack and joint filler had been worked out of the joint by the action of traffic, leaving the premoulded fiber exposed, and the joint open to the infiltration of water and foreign material. In the section where the entire depth of the joint was poured the material was in place and the joint better protected.

Forming weakened plane contraction joints with steel templates and subsequent pouring of the entire joint with a suitable crack and joint filler is worthy of serious consideration as a standard method.

#### CURING

As soon after the final finishing operation as the concrete had set sufficiently to prevent marring of the surface, the pavement was entirely covered with one thickness of thoroughly wetted burlap (12 ounces per square yard). This burlap was kept thoroughly wet during the day on which the pavement was laid (Fig. 37). During the following morning the burlap was removed and the pavement straight-edged. Then the pavement was thoroughly wetted and covered with Sisalkraft curing paper which remained in place from 72 to 96 hours after placement of the concrete (Fig. 41). Except for a short section this method of curing was used throughout the project.

Due to insufficient curing paper a section of pavement between stations 478+25 and 469+21.4 was covered with earth to a minimum depth of two inches. This earth was kept wet for 6 days and removed 21 days after placement of the concrete. A detailed account of the daily curing is given in the diary contained in this report.



### JOINT SEALING

Cleaning and sealing of the joints started at station 737+00, July 29, 1940. The joints were first thoroughly cleaned with steel scrapers and brooms, and then filled slightly less than flush with OA-2 crack and joint filler at a temperature of approximately 250 F. While the workmanship of sealing the joints was satisfactory, later inspection showed the seal to be very unsatisfactory for two reasons. First, the inherent quality of the OA-2, second, granular material which had been worked into the seal during shoulder construction.

### PAVEMENT INSPECTION

Close inspection of the entire project was made on September 12, 1940. This inspection showed that no scaling of the surface, spalling of the joints, or cracking of the slab had occurred at any place.



## VIII. CONTROL TESTS

### VIII. CONTROL TESTS



### VIII. CONTROL TESTS

One cylinder was made as a control specimen for each 500 linear feet of pavement. The molds were of steel 6 by 12 inches, and rested on metal base plates. Fabrication of the specimens was in accordance with A.S.T.M. Method C31-39. After 24 hours the cylinders were removed from the molds, and cured in wet earth from 18 days to 28 days. The average compressive strength of 68 specimens at 28 days was 4908 p.s.i., and 71 per cent of the specimens showed values within 10 per cent of the average.

In order to check the thickness of the pavement and the compressive strength of the concrete, one core was drilled from each 1000 linear feet of pavement. The theoretical thickness of the pavement was 7 inches, and the average actual thickness as measured by 35 cores was 7.109 inches. Compression tests on 34 of these cores at ages varying from 41 to 80 days averaged 4856 p.s.i., and 47 per cent were within 10 per cent of the average. The difference in cylinder and core strength is attributed to the different curing methods used. Results of the compression tests on cylinders and cores are shown in Table V.

Three beams were made as control specimens about midday on each pour. Steel beam molds 6 by 6 by 42 inches were used. Molding of the specimens was in accordance with A.S.T.M. Method C78-39. After 24 hours the beams were removed from the molds, and cured in wet earth for 27 days. The beams were tested in flexure on a Humboldt center loading machine of 24 inch span. The average of all



TABLE V. - SUMMARY OF RESULTS OF FLEXURAL AND TENSILE TESTS.

modulus of rupture tests at 28 days was 1002 p.s.i., and 77 per cent of the tests were within 10 per cent of the average. Results of the flexural tests and the variation of each from the average of all tests may be seen from Tables VI and VII.



TABLE V.- COMPRESSIVE STRENGTH OF CYLINDERS AND CORES.

	Compressive Strength Cylinders			Compressive Strength Cores			
	Station	28 days, psi.	Vari- ation from Average, per cent	Station	Psi.	Age days	Vari- ation from Average, per cent
Sec. No. 7	400+00	3910	20.3	398+45.0	4406	41	9.3
	405+00	5080	3.5	408+09.0	3596	42	25.9
	410+00	5440	10.8				
Sec. No. 6	415+00	5130	4.5	418+20.0	3983	43	18.0
	420+00	4330	11.8				
	425+00	5870	19.6				
Sec. No. 5	430+00	5370	9.4	428+09.6	4900	44	0.9
	435+00	4470	8.9	438+07.5	5393	45	11.1
	440+00	4740	3.4				
Sec. No. 4	445+00	4840	1.4	448+14.4	4442	47	8.5
	450+00	4420	9.9				
	455+00	4830	1.6				
Sec. No. 3	460+00	6200	26.3	458+11.5	4900	47	0.9
	465+00	4595	6.4	468+09.6	4019	49	17.2
	470+00	5905	20.3	478+72.0	4583	50	5.6
	475+00	5055	3.0				
	480+00	4895	0.3				
Sec. No. 2	485+00	4310	12.2	488+10.0	5464	50	12.5
	490+00	4370	11.0	498+10.0	4618	51	4.9
	495+00	4190	14.6	508+07.0	4829	51	0.6
	500+00	5890	20.0				
	505+00	4540	7.5				
	510+00	4880	0.6				
Sec. No. 1	515+00	5270	7.4	518+33.5	5993	52	23.4
	520+00	3890	20.7	528+11.0	6733	55	38.7
	525+00	4880	0.6	538+73.0	5288	56	8.9
	530+00	4315	12.1	548+09.4	4865	58	0.2
	535+00	3890	20.7	558+72.0	5041	59	3.8
	540+00	3930	19.9				
	545+00	4880	0.6				
	550+00	4810	2.0				
	555+00	5130	4.5				
	560+00	4950	0.9				



TABLE V.- (Continued) COMPRESSIVE STRENGTH OF CYLINDERS AND CORES.

	Compressive Strength Cylinders			Compressive Strength Cores			
	Station	28 days, psi.	Vari- ation from Average, per cent	Station	Psi.	Age days	Vari- ation from Average, per cent
Sec. Std.	565+00	4420	9.9	568+10.0	3737	60	23.0
	570+00	4950	0.9	578+19.3	5182	59	6.7
	575+00	5090	3.7	588+85.0	4477	63	7.8
	580+00	5234	6.6	598+37.5	5182	64	6.7
	585+00	4525	7.8	608+16.0	4900	64	0.9
	590+00	5300	8.0	628+05.6	5464	66	12.5
	595+00	5340	8.8				
	600+00	4950	0.9				
	605+00	5040	2.7				
	610+00	4820	1.8				
	615+00	4860	1.0				
	620+00	4930	0.4				
	625+00	5020	2.3				
	630+00	5090	3.7				
Sec. No. 2	635+00	4760	3.0	638+50.6	4759	69	2.0
	640+00	5220	6.4	648+11.0	6275	69	29.2
	645+00	4860	1.0				
	650+00	5120	4.3				
	655+00	5550	13.1				
Sec. No. 3	660+00	4630	5.7	658+30.0	3983	71	18.0
	665+00	5230	6.6	668+14.0	3243	72	33.2
	670+00	5690	15.9	678+10.1	3455	73	28.9
	675+00	4690	4.4				
	680+00	4360	11.2				
Sec. No. 4	685+00	4860	1.0	688+12.5	4759	73	2.0
	690+00	4950	0.9				
	695+00	5000	1.9				
Sec. No. 5	700+00	5220	6.4	698+13.0	4230	76	12.9
	705+00	5800	18.2	708+08.3	5605	78	15.4
	710+00	4890	0.4				
Sec. No. 6	715+00	4510	8.1	718+23.0	5605	79	15.4
	720+00	5190	5.7				
	725+00	5860	19.4				
Sec. No. 7	730+00	4620	5.9	728+11.5	5393	80	11.1
	735+00	3980	18.9	735+82.0	5816	80	19.8

Average compressive strength  
of all cylinders, 28 days 4908  
psi.

Average compressive  
strength of all cores, 60 days  
4856 psi.



TABLE VI.- MODULUS OF RUPTURE OF BEAMS.

	Modulus of Rupture, 28 days, psi.						
	Station	1	2	3	4	5	6
Sec. No. 7	402+50	1067	1087	1160	1113	1073	1067
Sec. No. 6	417+00	1100	1073	1033	1060	1053	1087
Sec. No. 5	427+00	1007	960	1047	1040	987	960
Sec. No. 4	441+00	1067	933	1153	1200	980	967
	451+50	933	1073	967	1093	1127	1033
Sec. No. 3	463+00	1000	1033	947	1120	920	960
	475+25	1040	1013	960	1040	1027	1113
Sec. No. 2	490+50	913	1067	1113	1093	1133	1080
	500+30	1013	927	1020	1000	1100	1053
Sec. No. 1	512+75	967	1067	780	1020	980	913
	523+00	960	960	987	933	907	813
	538+75	880	907	867	1013	907	1093
	547+00	973	1013	947	947	980	1000
	559+00	1053	1093	1013	1007	1087	1033
Std. Sec.	567+50	987	1073	1120	1153	1047	1133
	579+50	1067	1053	1027	1047	980	1013
	591+50	1033	1127	1040	1073	1067	1007
	600+40	1033	1000	1080	1040	1027	1000
	611+50	1047	1020	907	820	900	1053
	620+50	920	920	1087	1040	1067	1053
Sec. No. 2	634+00	987	887	1100	1233	913	980
	647+00	900	987	1060	947	840	927
Sec. No. 3	661+00	893	887	873	873	947	893
	669+75	973	853	900	953	987	920
Sec. No. 4	687+50	1000	1027	907	853	1080	993
Sec. No. 5	698+50	813	1073	827	840	960	880
	703+75	980	1047	887	1053	887	960
Sec. No. 6	710+75	893	1013	1053	1133	973	1067
	720+70	1033	1087	1067	953	1053	1080
Sec. No. 7	725+80	933	960				

Modulus of rupture average of all tests, 28 days 1002 psi.



TABLE VII.- VARIATION OF MODULUS OF RUPTURE TESTS  
FROM THE AVERAGE OF ALL TESTS.

	Station	Per Cent					
		1	2	3	4	5	6
Sec. No. 7	402+50	6.5	8.5	15.8	11.1	7.1	6.5
Sec. No. 6	417+00	9.8	7.1	3.1	5.8	5.1	8.5
Sec. No. 5	427+00	0.5	4.2	4.5	3.8	1.5	4.2
Sec. No. 4	441+00	6.5	6.9	15.1	19.8	2.2	3.5
	451+50	6.9	7.1	3.5	9.1	12.5	3.1
Sec. No. 3	463+00	0.2	3.1	5.5	11.8	8.2	4.2
	475+25	3.8	1.1	4.2	3.8	2.5	11.1
Sec. No. 2	490+50	8.9	6.5	11.1	9.1	13.1	7.8
	500+30	1.1	7.5	1.8	0.2	9.8	5.1
Sec. No. 1	512+75	3.5	6.5	22.2	1.8	2.2	8.9
	523+00	4.2	4.2	1.5	6.9	9.5	18.9
	538+75	12.2	9.5	13.5	1.1	9.5	9.1
	547+00	2.9	1.1	5.5	5.5	2.2	0.2
	559+00	5.1	9.1	1.1	0.5	8.5	3.1
Std. Sec.	567+50	1.5	7.1	11.8	15.1	4.5	13.1
	579+50	6.5	5.1	2.5	4.5	2.2	1.1
	591+50	3.1	12.5	3.8	7.1	6.5	0.5
	600+40	3.1	0.2	7.8	3.8	2.5	0.2
	611+50	4.5	1.8	9.5	18.2	10.2	5.1
	620+50	8.2	8.2	8.5	3.8	6.5	5.1
Sec. No. 2	634+00	1.5	11.5	9.8	23.1	8.9	2.2
	647+00	10.2	1.5	5.8	5.5	16.2	7.5
Sec. No. 3	661+00	10.9	11.5	12.9	12.9	5.5	10.9
	669+75	2.9	14.9	10.2	4.9	1.5	8.2
Sec. No. 4	687+50	0.2	2.5	9.5	14.9	7.8	0.9
Sec. No. 5	698+50	18.9	7.1	17.5	16.2	4.2	12.2
	703+75	2.2	4.5	11.5	5.1	11.5	4.2
Sec. No. 6	710+75	10.9	1.1	5.1	13.1	2.9	6.5
	720+70	3.1	8.5	6.5	4.9	5.1	7.8
Sec. No. 7	725+80	6.9	4.2				



TABLE VIII.- TEMPERATURE OF PAVEMENT CONCRETE  
DURING THE HARDENING PERIOD.

Station	Location	Time	Temperature Concrete, F.	Temperature Air, F.
692+40.0	8 ft. rt. C.L.	9:00 a.m.	82 <sup>a</sup>	79
		12:00 m.	89	87
		3:00 p.m.	96	86
		6:00 p.m.	92	84
		9:00 p.m.	88	74
		7:00 a.m.	82	82
661+84.0	8 ft. rt. C.L.	12:00 m.	90 <sup>b</sup>	84
		3:00 p.m.	98	86
		6:00 p.m.	101	80
		7:00 p.m.	98	76
		8:00 p.m.	95	74
		9:00 p.m.	93	68
624+18.5	7 ft. rt. C.L.	3:00 p.m.	98 <sup>c</sup>	93
		6:00 p.m.	101	84
		7:00 p.m.	102	81
		8:00 p.m.	100	80
		8:30 p.m.	99	77
		9:00 p.m.	98	76
		9:30 p.m.	97	76
		10:00 p.m.	96	74

<sup>a</sup>Broom or final finish July 15, 1940.  
<sup>b</sup>Broom or final finish July 18, 1940.  
<sup>c</sup>Broom or final finish July 22, 1940.



# U. S. DEPARTMENT OF AGRICULTURE, WEATHER BUREAU

## Special Observations Meteorological Bureau

Month of July, 1900 Station 1 Mi. West of Chambers, Mo.,  
(Lewis County) on U. S. Route 66.

Date	Temperature		Precipitation			Direction of Wind	Force at Time of Observation	State of Weather at Time of Observa- tion
	Maxi- mum	Mini- mum	Amount	Time	Amount			
1	82	63				S. E.		Clear
2	82	63				S. E.		Clear
3	82	63				S. E.		Clear
4	82	63				S. E.		Clear
5	82	63				S. E.		Clear
6	82	63				S. E.		Clear
7	82	63				S. E.		Clear
8	82	63				S. E.		Clear
9	82	63				S. E.		Clear
10	82	63				S. E.		Clear
11	82	63				S. E.		Clear
12	82	63				S. E.		Clear
13	82	63				S. E.		Clear
14	82	63				S. E.		Clear
15	82	63				S. E.		Clear
16	82	63				S. E.		Clear
17	82	63				S. E.		Clear
18	82	63				S. E.		Clear
19	82	63				S. E.		Clear
20	82	63				S. E.		Clear
21	82	63				S. E.		Clear
22	82	63				S. E.		Clear
23	82	63				S. E.		Clear
24	82	63				S. E.		Clear
25	82	63				S. E.		Clear
26	82	63				S. E.		Clear
27	82	63				S. E.		Clear
28	82	63				S. E.		Clear
29	82	63				S. E.		Clear
30	82	63				S. E.		Clear
31	82	63				S. E.		Clear

## IX. U. S. WEATHER BUREAU REPORT



U. S. DEPARTMENT OF AGRICULTURE, WEATHER BUREAU

Special Observer's Meteorological Record

Month of July, 1940. Station 1 Mi. West of Owensboro, Ky.,  
(Daviness County) on U.S. Route 60.

Date	Temperature		Precipitation			Wind Direction at Time of Obser- vation	State of Weather at Time of Obser- vation
	Maxi- mum	Mini- mum	Time of Begin- ning	Time of Ending	Amount inches		
1	89	61				S.E.	Clear
2	85	64	D.N.	D.N.	1.21	S.	Cloudy
3	81	60				S.W.	Clear
4	82	58				E.	Clear
5	84	57				S.E.	Clear
6	86	58				E.	P. Cloudy
7	84	62				S.E.	Cloudy
8	80	64				S.	Cloudy
9	87	65				S.E.	Clear
10	91	65				S.	Clear
11	89	66				S.	Clear
12	85	67	D.N.	11 a.m.	0.70	N.W.	Cloudy
13	83	55			0.06	N.W.	Clear
14	84	55				S.	Clear
15	88	62				S.W.	P. Cloudy
16	78	68	9 a.m.	11 a.m.	Trace	N.	P. Cloudy
17	81	59			1.15	N.E.	Clear
18	86	59				S.E.	Clear
19	88	66				S.	Clear
20	89	66				S.	Clear
21	92	68				S.E.	Clear
22	92	70				S.	Clear
23	94	71			Trace	S.	Clear
24	93	71				S.	Clear
25	96	70				S.W.	Clear
26	96	71				S.	Clear
27	96	71				S.	Clear
28	96	71				S.	Clear
29	97	71				S.W.	Clear
30	99	72			Trace	S.	Clear
31	95	70				S.	Clear



U. S. DEPARTMENT OF AGRICULTURE, WEATHER BUREAU.

Special Observer's Meteorological Record

Month of August, 1940.

Station 1 Mi. West of Owensboro, Ky.  
(Daviness County) on U.S. Route 60.

Date	Temperature		Precipitation			Wind Direction at Time of Observation	State of Weather at Time of Observation
	Maxi-mum	Mini-mum	Time of Beginning	Time of Ending	Amount inches		
1	93	70				N.E.	Cloudy
2	92	65				N.E.	Clear
3	93	66				S.	Clear
4	92	68				S.E.	P. Cloudy
5	94	66				S.	Clear
6	86	70				S.E.	Clear
7	90	66			Trace	S.	Clear
8	92	65				S.E.	Cloudy
9	91	64				E.	Clear
10	84	70				S.E.	Cloudy
11	92	70	5 p.m.		Trace	S.E.	P. Cloudy
12	95	73		D.N.	0.07	N.E.	Clear
13	84	73			Trace	N.E.	Cloudy
14	94	64			Trace	S.	Clear
15	94	67				S.E.	Clear
16	95	68				S.E.	Clear
17	97	67	2:30 pm.	4 p.m.		S.	Clear
18	85	68			1.46	S.E.	Clear
19	76	59		D.N.	0.10	S.E.	Clear
20	77	55				N.	P. Cloudy
21	79	55				N.E.	Clear
22	82	49				N.E.	Clear
23	84	54				S.E.	Clear
24	84	60				S.	Clear
25	89	71				S.	Clear
26	91	66				S.W.	P. Cloudy
27	89	71				S.	Cloudy
28	88	66	11 a.m.		0.17	S.E.	Cloudy
29	84	67			1.00	S.E.	P. Cloudy
30	86	66			0.07	S.	Cloudy
31	84	60		D.N.	0.15	S.W.	Clear



# X. STATIONING OF PROJECT



# X. STATIONING OF PROJECT

Beginning of project	- - - - -	station 397+49.4
End of project	- - - - -	station 737+00.0
Length	- - - - -	33950.6 feet
Deduction for bridges		
station 581+02.0 to station 582+67.0	---	165.0 feet
station 586+61.0 to station 588+26.0	---	165.0 feet
station 595+01.0 to station 596+66.0	---	165.0 feet
station 601+14.5 to station 602+99.5	---	185.0 feet
station 609+17.5 to station 610+82.5	---	165.0 feet
Net length	- - - - -	33105.6 feet
Net length	- - - - -	6.27 miles

## STATIONING OF EXPERIMENTAL SECTIONS

Begin Section No. 7	- - - - -	station 397+49.4
Begin subsections for measurements joint No. 1	--	station 403+61
Temperature well 7 feet right of C. L.	--	station 406+91
End subsections for measurements joint No. 31	--	station 409+61
End Section No. 7	- - - - -	station 410+21
Begin Section No. 6	- - - - -	station 410+21
Begin subsections for measurements joint No. 1	--	station 410+81
Temperature well 7 feet right of C. L.	--	station 412+91
End subsections for measurements joint No. 11	--	station 416+81
End Section No. 6	- - - - -	station 425+21
Begin Section No. 5	- - - - -	station 425+21
Begin subsections for measurements joint No. 1	--	station 433+61
Temperature well 7 feet right of C. L.	--	station 437+11
End subsections for measurements joint No. 31	--	station 439+61
End Section No. 5	- - - - -	station 440+01
Begin Section No. 4	- - - - -	station 440+01
Begin subsections for measurements joint No. 1	--	station 448+02
Temperature well 7 feet right of C. L.	--	station 451+12
End subsections for measurements joint No. 31	--	station 454+02
End Section No. 4	- - - - -	station 455+02
Begin Section No. 3	- - - - -	station 455+02
Begin subsections for measurements joint No. 1	--	station 462+00
Temperature well 7 feet right of C. L.	--	station 464+10
End subsections for measurements joint No. 41	--	station 470+00
End Section No. 3	- - - - -	station 480+00
Begin Section No. 2	- - - - -	station 480+00
Begin subsection for measurements joint No. 1	--	station 502+00
Temperature well 7 feet right of C. L.	--	station 506+10
End subsection for measurements joint No. 41	--	station 510+00
End Section No. 2	- - - - -	station 510+00



Begin Section No. 1	- - - - -	station	510+00
Begin section for measurements joint No. 1	-----	station	510+25
	joint No. 10	-----	station 512+05
	joint No. 13	-----	station 513+45
Temperature well 7 feet right of C. L.	-----	station	517+54
	joint No. 53	-----	station 521+43
	joint No. 56	-----	station 556+00
End section for measurements joint No. 66	-----	station	558+00
End Section No. 1	- - - - -	station	560+00
Begin Standard Section	- - - - -	station	560+00
Begin subsections for measurements joint No. 1	--	station	567+61
Temperature well 7 feet right of C. L.	--	station	573+77
End subsections for measurements joint No. 41	--	station	579+62
End Standard Section	- - - - -	station	630+00
Begin Section No. 2	- - - - -	station	630+00
End Section No. 2	- - - - -	station	655+00
Begin Section No. 3	- - - - -	station	655+00
End Section No. 3	- - - - -	station	680+00
Begin Section No. 4	- - - - -	station	680+00
End Section No. 4	- - - - -	station	695+00
Begin Section No. 5	- - - - -	station	695+00
End Section No. 5	- - - - -	station	710+00
Begin Section No. 6	- - - - -	station	710+00
End Section No. 6	- - - - -	station	725+00
Begin Section No. 7	- - - - -	station	725+00
End Section No. 7	- - - - -	station	737+00



XI. ILLUSTRATIONS





Fig. 1.- Batching equipment, Owensboro, Ky.





Fig. 2.- Batching equipment, Owensboro, Ky.





Fig. 3.-Five tooth scarifier pulled by Caterpillar and Allis-Chalmers diesel tractors operating at station 404+00.





Fig. 4.- Austin-Western No. 10 grader operating at  
station 410+00.





Fig. 5.- Cleveland Form grader operating at  
station 532+00.





Fig. 6.- R. B. Power Finegrader operating at station 660+00.





Fig. 7.- Huber Roller (5 tons) operating at  
station 663+00.





Fig. 8.- Completed Subgrade, Stations 664+00 to 669+00.





Fig. 9.- Completed subgrade, stations 530+00 to 540+00.





Fig. 10.- Equipment train, paver operating at station 708+00.





Fig. 11.- Koehring 27-E Paver operating at  
station 668+60.





Fig. 12.- Equipment train, paver operating at station 663+00.





Fig. 13.- Equipment train, paver operating at station 662+00.





Fig. 14.- Completed subgrade, stations 539+00 to 534+00.



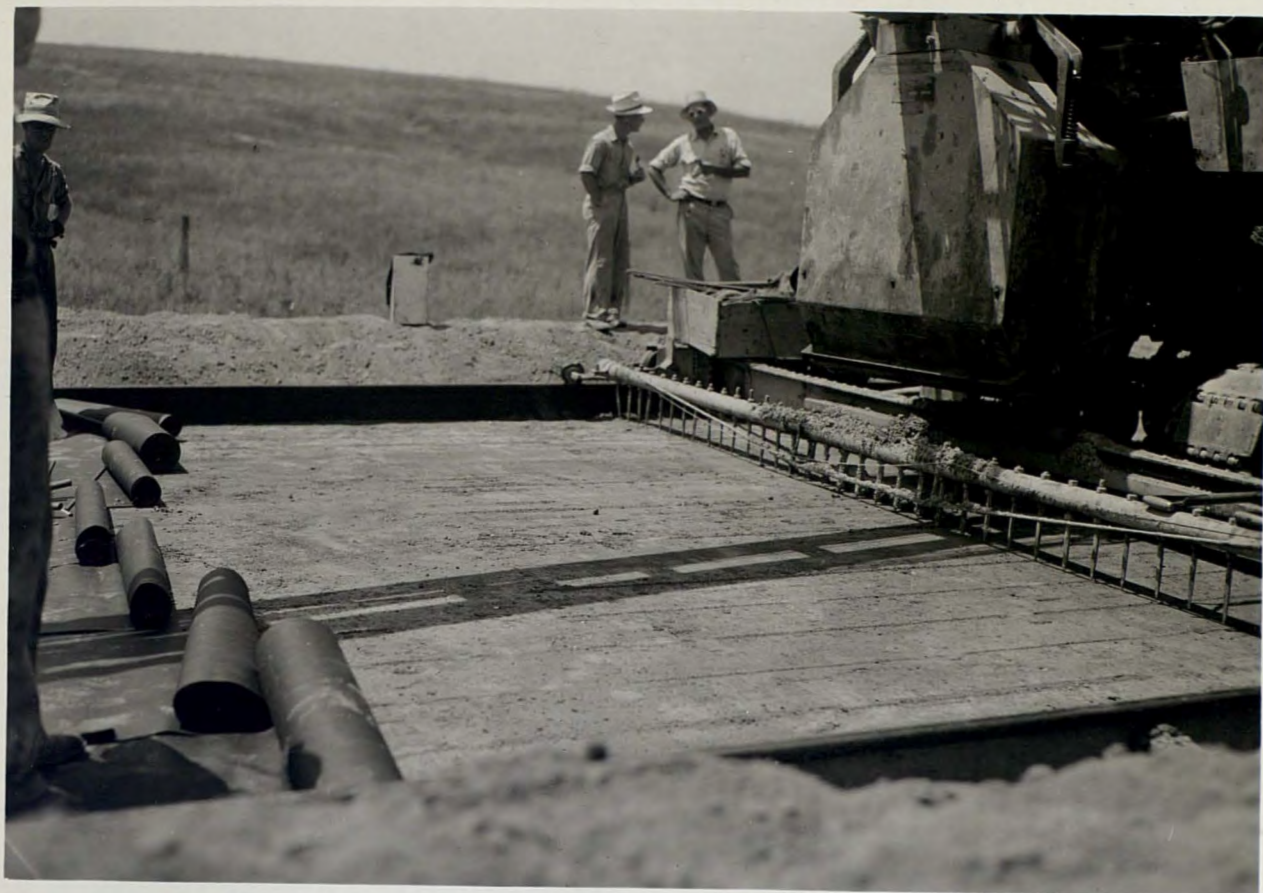


Fig. 15.- Completed subgrade before placing subgrade paper, station 539+50.





Fig. 16.—Completed installation of Laclede Welded Dowel Spacer and dowels at contraction joint, station 436+81.





Fig. 17.-Completed installation of Laclede Welded Dowel Spacer, dowels, and premoulded fiber joint filler at expansion joint, station 668+80.





Fig. 18.- Placing of concrete by hand around dowel bars  
at expansion joint, station 668+80.





Fig. 19.- Placing of concrete by hand around dowel bars  
at expansion joint, station 668+80.





Fig. 20.- Spreading concrete by hand in front of finishing machine, and vibrator operating alongside form, station 540+00.





Fig. 21.- Spreading concrete by hand in front of finishing machine, station 663+00.





Fig. 22.- Concrete roll on front screed second pass of finishing machine. Front screed flat, rear screed not operating, removing crown from pavement on superelevated curve, station 711+15.





Fig. 23.- Mortar roll on rear screed of finishing machine,  
station 668+00.





Fig. 24.- Mortar roll on rear screed of finishing machine,  
station 667+50.





Fig. 25.- Cutting contraction joint with steel T beam cutter, station 470+40.





Fig. 26.- Installing premoulded fiber contraction joint filler, station 470+40.

This method is used on contraction joints only, stations 397+42.4 to 450+01.





Fig. 27: - Forming weakened plane contraction joint station 443+81 by inserting two steel strips ( $1\frac{1}{2}$  in. x  $\frac{1}{2}$  in. x 10 ft.)  $\frac{1}{4}$  in. below surface. Joint is then edged and steel removed. No pre-moulded fiber used, joint poured with OA-2 crack and joint filler throughout entire depth. This method used on contraction joints only, stations 397+49.4 to 450+21.





Fig. 28.- Contraction joint after insertion of steel strips, station 438+21.





Fig. 29.- Koehring longitudinal finishing machine  
operating at station 666+00.





Fig. 30.- Pavement poured during a.m. covered with burlap and being kept wet by sprinkling, stations 662+00 to 667+19.6. Previous days pour in background covered with Sisalkraft curing paper.





Fig. 31.- Testing surface for irregularities with 10 ft. metal straightedges, station 663+00.



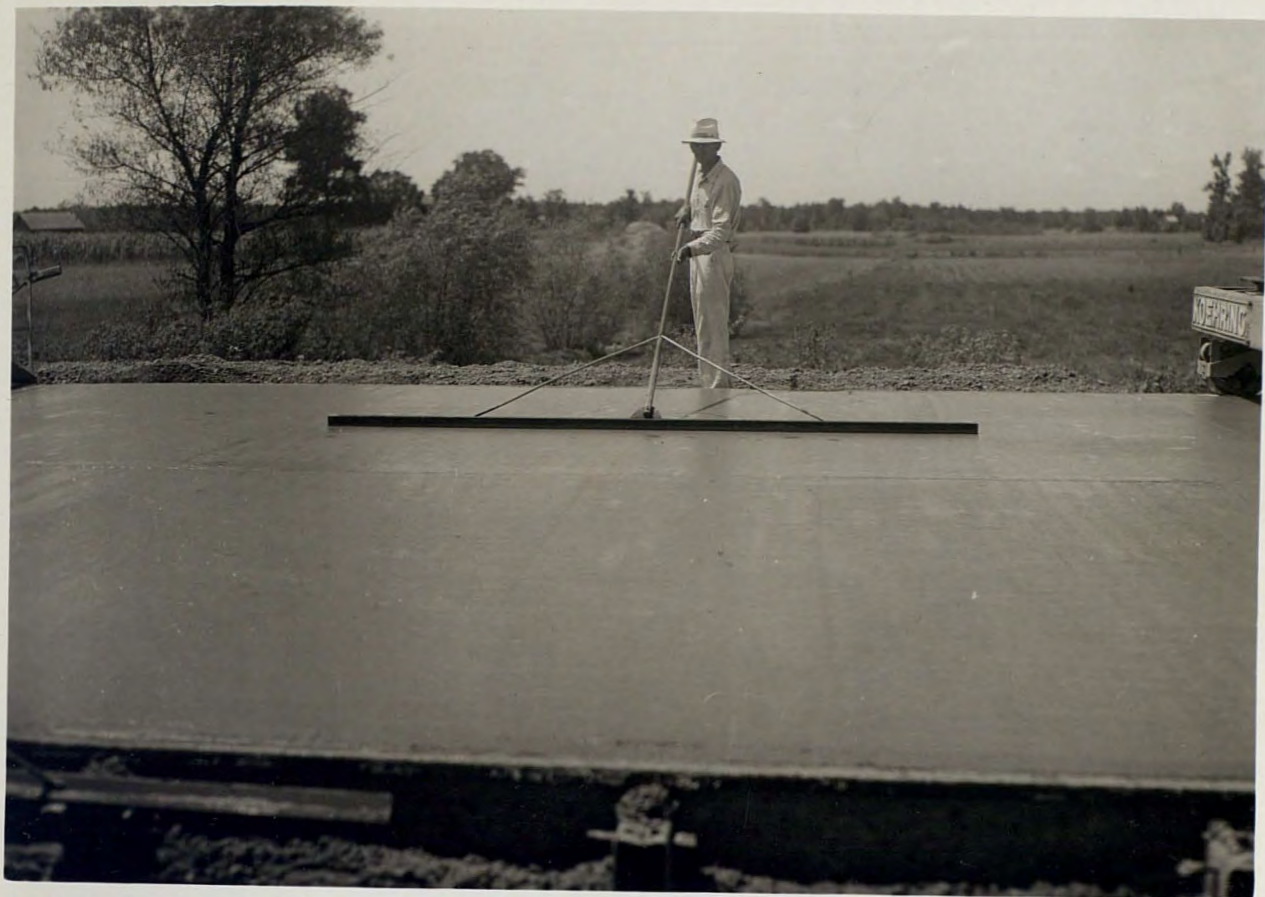


Fig. 32.- Testing surface for irregularities with 10 ft.  
metal straightedge, station 516+00.





Fig. 33.- Final belting of surface with bowstring rubber belt (width 8 in.), station 446+00.





Fig. 34.- Completed contraction joint (width  $\frac{3}{4}$  in.),  
station 666+00.



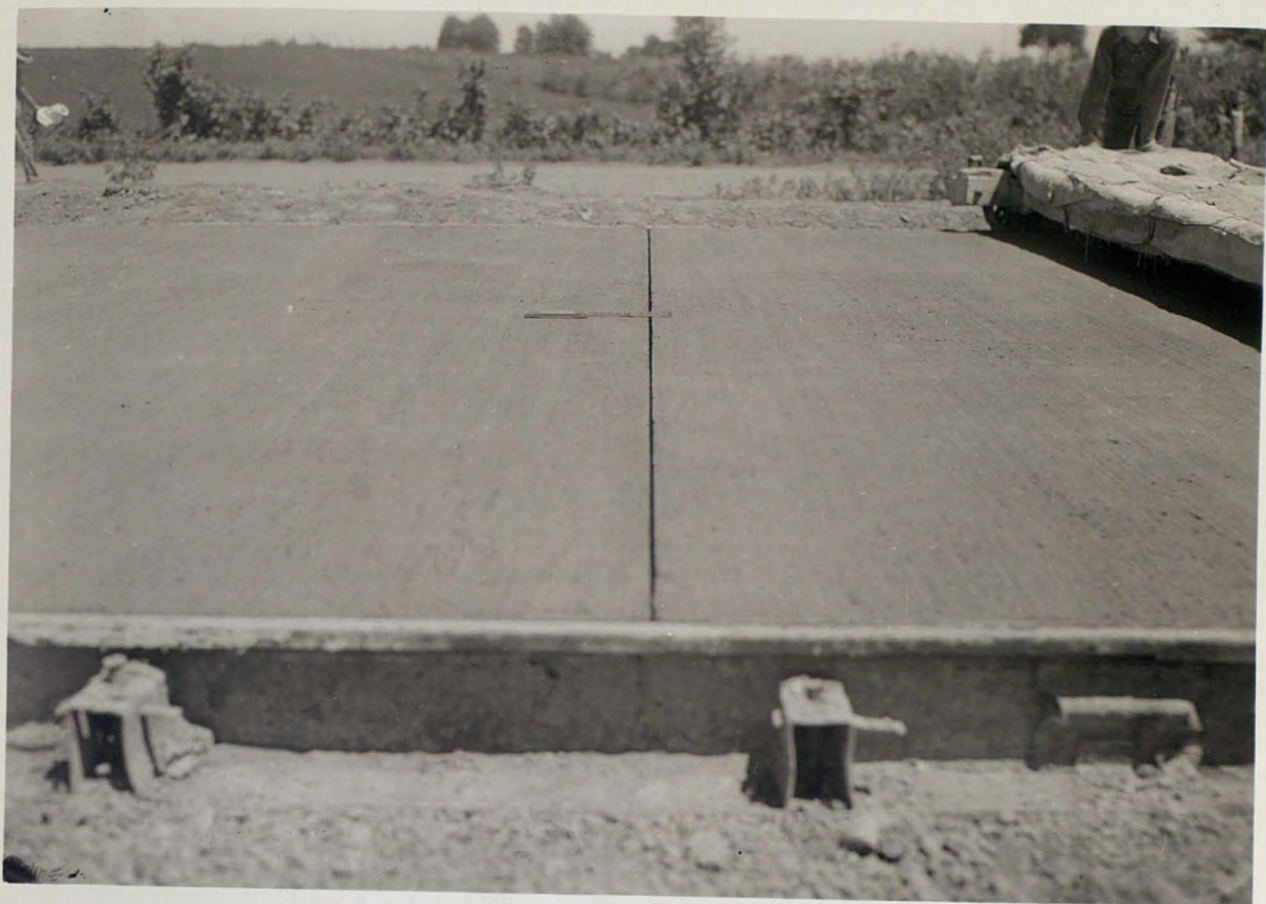


Fig. 35.- Completed contraction joint (width  $1/2$  in.),  
station 433+01.





Fig. 36.- Brooming of surface, station 512+50.





Fig. 37.- Pavement poured during run covered with burlap  
and kept wet by sprinkling, stations 513+00  
to 521+24.





Fig. 38.- Completed expansion joint, station 432+41.



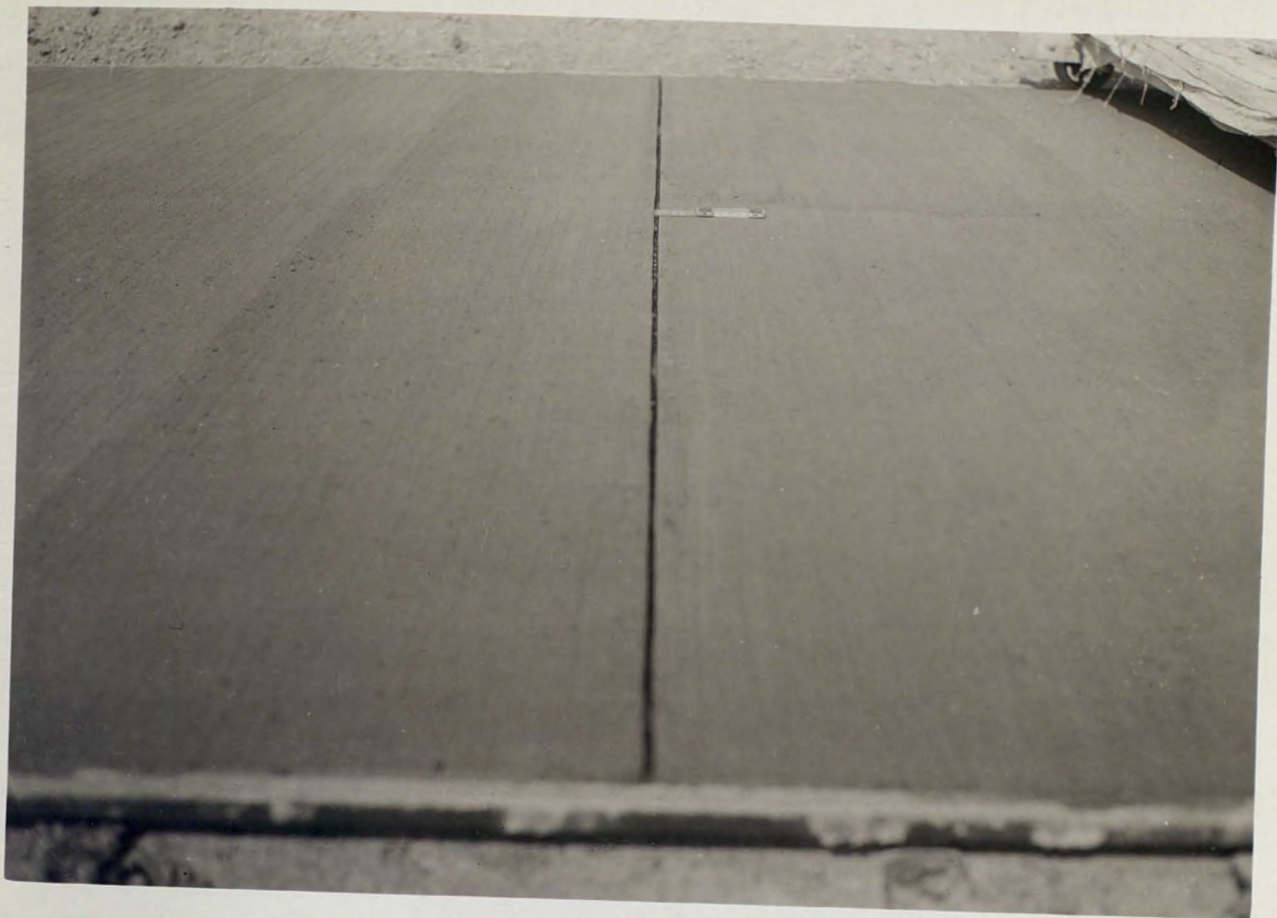


Fig. 39.- Completed contraction joint (width  $3/4$  in.),  
station 514+05.





Fig. 40.- Testing completed pavement for surface irregularities at construction joint, station 667+19.6.

Note: Workman on right thoroughly wetting surface before application of curing paper.





Fig. 41.- Placing Sisalkraft curing paper 8:20 a.m. of the day following the placing of the concrete, station 667+50.  
Note: Workman on right thoroughly wetting surface before application of curing paper.





Fig. 42.- Placing Sisalkraft curing paper 7:45 a.m. of the day following the placing of the concrete, station 669+75.





Fig. 43.- Removing curing paper, station 657+00.





Fig. 44.- Removing curing paper, station 655+00.





Fig. 45.- Completed pavement, stations 483+00 to 420+00.





Fig. 46.- Completed pavement, stations 544+00 to 490+00.





Fig. 47.- Completed pavement, stations 635+00 to 556+00.





Fig. 48.- Completed pavement, stations 653+00 to 638+00.





Fig. 49. - Completed pavement, stations 709+00 to 705+00.





Campbell

Hailey

Fig. 50.- Measuring the change in width of the joint,  
station 572+42.



(Distance in inches of premoulded joint filler below surface of pavement.)



Sta.	Type	Lt.	C.L.	Rt.	Sta.	Type	Lt.	C.L.	Rt.
397+61	Ex.	5/16	0	1/2	403+41	C	2-1/4	2-7/16	2-1/8
397+81	C	1-15/16	2	1-15/16	403+61	Ex.	15/16	1"	13/16
398+01	C	2	1-7/8	1-15/16	403+81	C	1-15/16	2"	2"
398+21	C	1-13/16	2-1/16	1-3/4	404+01	C	2-1/16	2-1/8	2-1/16
398+41	C	1-3/4	2-1/8	1-13/16	404+21	C	1-15/16	1-3/4	1-7/8
398+61	C	1-3/4	2-3/16	1-7/8	404+41	C	1-7/8	1-15/16	2-1/16
398+81	Ex.	3/8	0	3/8	404+61	C	2-1/4	2-3/16	1-7/8
399+01	C	1-5/8	2-1/16	2	404+81	Ex.	1"	1-3/8	7/8
399+21	C	1-15/16	2-1/4	1-3/4	405+01	C	2-3/16	1-7/8	2"
399+41	C	1-3/4	2-1/16	2-1/8	405+21	C	2-1/16	2"	2-1/16
399+61	C	2	2-1/4	1-7/8	405+41	C	2"	2-1/16	2"
399+81	C	1-3/4	2-1/8	1-7/8	405+61	C	1-7/8	2-1/8	2"
400+01	Ex.	7/8	3/4	5/8	405+81	C	1-3/4	2-3/16	2"
400+21	C	1-15/16	1-7/8	2	406+01	Ex.	3/4	1/2	5/8
400+41	C	1-3/4	2-1/16	1-3/4	406+21	C	1-15/16	2-1/16	2-3/16
400+61	C	1-7/8	2-1/8	2-1/4	406+41	C	2"	1-7/8	2"
400+81	C	1-15/16	2	1-7/8	406+61	C	1-15/16	2-1/8	2-9/16
401+01	C	1-3/4	1-15/16	2-1/4	406+81.4	Const. Jt.			
401+21	Ex.	1-3/16	7/8	3/4	407+01	C	2"	2-1/16	2-1/8
401+41	C	1-3/4	2"	1-3/4	407+21	Ex.	5/8	3/4	13/16
401+61	C	1-7/8	2"	1-13/16	407+41	C	2-1/8	2-1/16	2"
401+81	C	1-7/8	2"	2-3/16	407+61	C	2-1/16	2"	2-3/16
402+01	C	1-3/4	2-1/2	1-1/2	407+81	C	2-1/16	2-3/16	2-1/16
402+21	C	2-1/16	2-1/8	2-1/4	408+01	C	1-15/16	1-7/8	1-15/16
402+41	Ex.	7/8	7/8	3/4	408+21	C	1-3/4	1-15/16	2-1/8
402+61	C	1-13/16	2"	1-15/16	408+41	Ex.	3/4	1/2	1/2
402+81	C	2"	2"	1-7/8	408+61	C	2"	2-3/4	2-1/8
403+01	C	2-1/8	2-1/8	2"	408+81	C	1-7/8	2-1/16	1-15/16
403+21	C	1-15/16	2-1/8	2"	409+01	C	1-3/4	1-15/16	2"



Sta.	Type	Lt.	C.L.	Rt.	Sta.	Type	Lt.	C.L.	Rt.
409+21	C	1-15/16	2-1/8	2-1/8	425+21	Ex.	15/16	1/2	7/16
409+41	C	2-1/16	2"	1-7/8	425+41	C	1-15/16	2"	2-1/16
409+61	Ex.	3/4	1/2	9-16	425+61	C	1-7/8	1-3/4	1-3/4
409+81	C	1-15/16	1-7/8	1-15/16	425+81	C	2-3/16	1-15/16	2-1/16
410+01	C	2-1/16	2-1/8	2-1/2	426+01	C	1-15/16	2"	1-7/8
410+21	C	1-3/4	1-15/16	2-1/8	426+21	C	1-7/8	1-7/8	2-1/16
410+81	Ex.	3/4	5/8	5/8	426+41	Ex.	3/4	1/2	5/8
411+41	C	1-13/16	1-7/8	1-7/8	426+61	C	1-15/16	1-15/16	1-7/8
412+01	Ex.	13/16	1/2	1/2	426+81	C	1-7/8	2-1/16	1-15/16
412+61	C	1-3/4	1-7/8	1-7/8	427+01	C	2-1/4	2"	1-7/8
413+21	Ex.	7/8	13/16	3/4	427+21	C	1-7/8	2-1/16	1-7/8
413+81	C	2"	1-13/16	2-1/16	427+41	C	2"	1-7/8	2-1/8
414+41	Ex.	1/2	5/8	1/2	427+61	Ex.	3/4	9/16	3/8
415+01	C	1-7/8	2"	1-7/8	427+81	C.	1-7/8	1-3/4	1-3/4
415+61	Ex.	5/8	1/2	3/8	428+01	C	1-15/16	2"	1-7/8
416+21	C	2"	1-7/8	1-3/4	428+21	C	2-1/2	2"	1-7/8
416+81	Ex.	1/2	1/2	7/16	428+41	C	1-7/8	2"	2"
417+41	C	1-7/8	1-7/8	1-13/16	428+61	C	1-15/16	1-7/8	1-13/16
418+01	Ex.	3/4	7/16	3/8	428+81	Ex.	3/4	9/16	1/2
418+61	C	1-7/8	2"	1-3/4	429+01	C	1-13/16	1-3/4	1-7/8
419+21	Ex.	1/2	5/8	5/8	429+21	Const. Jt.			
419+81	Const. Jt.				429+41	C	2-1/16	2"	1-7/8
420+41	Ex.	1/2	3/8	3/8	429+61	C	1-15/16	2"	1-11/16
421+01	C	1-7/8	2-1/4	2"	429+81	C	1-3/4	1-3/4	1-15/16
421+61	Ex.	5/8	13/16	5/8	430+01	Ex.	11/16	7/16	9/16
422+21	C	1-7/8	1-13/16	1-7/8	430+21	C	1-15/16	1-7/8	2"
422+81	Ex.	13/16	5/8	1/2	430+41	C	1-7/8	1-15/16	2-1/16
423+41	C	2-3/16	1-7/8	2-1/2	430+61	C	2-1/8	2-1/8	1-13/16
424+01	Ex.	3/4	1/4	9/16	430+81	C	2-1/16	1-3/4	1-7/8
424+61	C	1-7/8	2-1/16	1-7/8	431+01	C	1-7/8	1-3/4	1-7/8
					431+21	Ex.	15/16	5/8	1/2
					431+41	C	1-13/16	1-3/4	1-13/16
					431+61	C	1-5/8	1-3/4	1-3/4



Sta.	Type	Lt.	C.L.	Rt.	Sta.	Type	Lt.	C.L.	Rt.
431+81	C	1-3/4	1-13/16	1-7/8	439+01	C	1-3/4	1-7/8	1-7/8
432+01	C	1-7/8	1-15/16	1-7/8	439+21	C	1-13/16	1-15/16	1-13/16
432+21	C	2-1/16	1-7/8	1-13/16	439+41	C	1-3/4	1-3/4	2-1/8
432+41	Ex.	3/4	1/2	5/8	439+61	Ex.	7/8	9/16	5/8
432+61	C	1-15/16	1-3/4	1-3/4	439+81	C	1-7/8	1-7/8	2-3/16
432+81	C	2"	2"	1-13/16	440+01	C	1-13/16	1-7/8	1-3/4
433+01	C	2"	1-15/16	2-1/16	440+21	C	1-7/8	1-15/16	2-1/4
433+21	C	1-7/8	1-3/4	1-7/8	440+41	C	1-5/8	1-15/16	1-9/16
433+41	C	1-3/4	1-5/8	1-3/4	440+61	C	1-3/4	1-3/4	1-15/16
433+61	Ex.	1/2	1/2	7/8	440+81	Ex.	3/4	3/8	1/2
433+82.5	Const. Jt.				441+01	C	1-11/16	1-7/8	2"
434+01	C	1-7/8	1-7/8	1-3/4	441+21	C	1-3/4	1-3/4	2"
434+21	C	1-3/4	2"	2-1/16	441+41	C	2-1/8	1-7/8	2-3/16
434+41	C	1-3/4	1-7/8	1-5/8	441+61	C	1-5/8	1-7/8	1-5/8
434+61	C	1-7/8	1-15/16	1-15/16	441+81	C	1-13/16	1-7/8	1-13/16
434+81	Ex.	5/8	9/16	3/4	442+01	Ex.	11/16	1/2	5/8
435+01	C	1-15/16	1-7/8	1-15/16	442+21	C	1-7/8	2-1/8	1-15/16
435+21	C	1-3/4	1-13/16	1-7/8	442+41	C	2"	2"	2-1/16
435+41	C	1-5/8	2"	1-15/16	442+61	C	1-7/8	2"	1-7/8
435+61	C	1-7/8	1-15/16	1-7/8	442+81	C	2"	1-7/8	1-3/4
435+81	C	1-7/8	1-13/16	2"	443+01	C	1-3/4	2-3/16	1-3/4
436+01	Ex.	3/4	3/8	3/4	443+21	Ex.	5/8	3/8	1/2
436+21	C	1-3/4	1-15/16	2"	443+41	C	1-7/8	2"	1-3/4
436+41	C	2-1/8	1-3/4	2-1/4	443+61	C	1-13/16	2"	1-7/8
436+61	C	1-15/16	2-1/16	2"	443+81	C	2"	2"	1-7/8
436+81	C	1-3/4	2-1/16	1-13/16	444+01	C	2-1/16	1-7/8	1-15/16
437+01	C	1-3/4	1-7/8	1-5/8	444+21	C	2"	1-3/4	1-3/4
437+21	Ex.	7/8	1/2	3/4	444+41	Ex.	1/2	9/16	1/2
437+41	C	1-3/4	1-13/16	1-1/2	444+61	C	1-7/8	1-15/16	2"
437+61	C	1-7/8	1-15/16	2"					
437+81	C	1-13/16	1-13/16	1-3/4					
438+01	C	1-3/4	1-3/4	1-15/16					
438+21	C	1-7/8	1-7/8	2"					
438+41	Ex.	5/8	7/16	9-1/6					
438+61	C	1-3/4	1-13/16	1-3/4					
438+81	C	1-7/8	1-3/4	1-13/16					



Sta.	Type	Lt.	C.L.	Rt.	Sta.	Type	Lt.	C.L.	Rt.
444+81	C	2"	1-15/16	1-7/8	450+42	Ex.	5/8	1/2	9/16
445+01	C	2-1/8	2"	1-13/16	450+62	C	1/2	3/8	7/16
445+21	C	2"	2"	1-15/16	450+82	C	5/8	3/8	1/2
445+41	C	1-7/8	2-3/16	2-1/16	451+02	C	9/16	7/16	1/2
445+61	Ex.	11/16	9/16	5/16	451+22	C	9/16	1/2	9/16
445+81	C	2"	2"	2"	451+42	C	5/8	11/16	9/16
446+01	C	2"	2"	1-15/16	451+62	Ex.	7/8	3/8	1/2
446+21	C	2-1/8	2"	2"	451+82	C.	7/16	9/16	11/16
446+41	C	1-7/8	1-15/16	1-13/16	452+02	C	9/16	1/2	9/16
446+61	C	1-15/16	2-1/8	1-7/8	452+22	C	13/16	15/16	3/4
446+81	Ex.	7/8	1"	5/8	452+42	C	11/16	5/8	9/16
447+01	C	2"	1-3/4	1-7/8	452+62	C	7/16	5/8	5/8
447+22	C	2-1/8	2"	1-7/8	452+82	Ex.	5/8	5/16	3/8
447+42	C	1-7/8	2-1/16	2"	453+02	C	3/4	11/16	9/16
447+62	C	2"	1-15/16	1-15/16	453+22	C	1/2	1"	3/4
447+82	C	2"	1-7/8	2"	453+42	C	15/16	7/8	13/16
447+90.5	Const. Joint				453+62	C	3/4	11/16	15/16
448+02	Ex.	13/16	7/16	11/16	453+82	C	9/16	13/16	3/4
448+22	C	1-7/8	2"	1-7/8	454+02	Ex.	5/8	5/8	15/16
448+42	C	1-5/8	2-5/16	1-15/16	454+22	C	5/8	13/16	13/16
448+62	C	2-1/4	2"	2"	454+42	C	3/4	13/16	7/8
448+82	C	1-13/16	1-7/8	1-3/4	454+62	C	7/8	13/16	7/8
449+02	C	1-7/8	2"	1-5/8	454+82	C	7/16	3/4	7/8
449+22	Ex.	13/16	1/2	9/16	455+02	C	7/16	1/2	3/4
449+42	C	2"	2"	1-13/16	455+22	C	5/8	15/16	3/4
449+62	C	1-11/16	2-1/8	2"	455+42	C	13/16	9/16	13/16
449+82	C	2"	1-15/16	1-15/16	455+62	C	3/4	3/4	13/16
450+02	C	1-3/4	1-3/4	2"	455+82	C	7/16	13/16	13/16
450+22	C	1-7/8	1-7/8	1-5/8	456+02	C	9/16	5/8	3/4



Sta.	Type	Lt.	C.L.	Rt.	Sta.	Type	Lt.	C.L.	Rt.
456+22	C	13/16	7/8	3/4	461+80	C	5/8	3/4	3/4
456+42	C	7/8	11/16	7/8	462+00	Ex.	7/16	3/8	7/16
456+62	C	13/16	3/4	11/16	462+20	C	3/4	11/16	13/16
456+82	C	11/16	9/16	9/16	462+40	C	9/16	9/16	11/16
457+02	C	1/2	7/16	3/4	462+60	C	13/16	11/16	3/4
457+22	C	7/8	1"	13/16	462+80	C	11/16	3/4	7/8
457+42	C	3/4	13/16	3/4	463+00	C	3/4	3/4	3/4
457+62	C	13/16	1"	11/16	463+20	C	7/16	3/4	13/16
457+82	C	11/16	5/8	7/8	463+40	C	3/4	5/8	1/2
458+02	Ex.	3/8	5/16	5/16	463+60	C	7/16	5/8	3/4
458+22	C	7/8	15/16	1"	463+80	C	13/16	7/8	13/16
458+42	C	7/8	15/16	7/8	464+00	C	5/8	3/4	7/8
458+62	C	11/16	13/16	7/8	464+20	C	1/2	7/8	3/4
458+82	C	13/16	7/8	1"	464+40	C	13/16	15/16	7/8
459+02	C	7/8	3/4	11/16	464+60	C	9/16	1/2	3/4
459+20	C	11/16	3/4	3/4	464+80	C	13/16	7/8	1"
459+31.0	Const. Jt.				465+00	C	13/16	7/8	7/8
459+40	C	5/8	3/4	3/4	465+20	C	5/8	5/8	11/16
459+60	C	1/2	1/2	9/16	465+40	C	3/4	11/16	11/16
459+80	C	11/16	1/2	9/16	465+60	C	13/16	7/8	7/8
460+00	C	11/16	3/4	3/4	465+80	C	3/4	7/8	3/4
460+20	C	7/8	3/4	7/8	466+00	Ex.	9/16	1/2	1/2
460+40	C	1"	7/8	3/4	466+20	C	13/16	11/16	7/16
460+60	C	1/2	9/16	7/8	466+40	C	7/8	13/16	13/16
460+80	C	11/16	7/8	7/8	466+60	C	13/16	7/8	15/16
461+00	C	3/4	1"	7/8	466+80	C	13/16	13/16	13/16
461+20	C	15/16	3/4	13/16	467+00	C	3/4	15/16	15/16
461+40	C	7/8	11/16	15/16	467+20	C	11/16	13/16	7/8
461+60	C	5/8	11/16	13/16	467+40	C	7/8	3/4	7/8



Sta.	Type	Lt.	C.L.	Rt.	Sta.	Type	Lt.	C.L.	Rt.
467+60	C	13/16	7/8	3/4	473+60	C	1/2	7/8	11/16
467+80	C	7/8	3/4	7/8	473+80	C	1/2	3/4	7/8
468+00	C	15/16	15/16	15/16	474+00	Ex.	3/8	1/4	3/8
468+20	C	13/16	15/16	15/16	474+20	C	7/8	7/8	3/4
468+40	C	7/8	1/2	1"	474+40	C	7/8	3/4	3/4
468+60	C	11/16	7/16	7/8	474+60	C	3/4	15/16	15/16
468+80	C	11/16	7/8	7/8	474+80	C	13/16	13/16	5/8
469+00	C	3/4	3/4	11/16	475+00	C	11/16	9/16	5/8
469+21.4	Const. Jt.				475+20	C	3/4	5/8	3/4
469+40	C	11/16	9/16	13/16	475+40	C	3/4	15/16	15/16
469+60	C	7/16	11/16	9/16	475+60	C	7/8	3/4	3/4
469+80	C	13/16	13/16	1/2	475+80	C	13/16	5/8	15/16
470+00	Ex.	11/16	1/4	5/16	476+00	C	15/16	13/16	1"
470+20	C	11/16	3/4	11/16	476+20	C	11/16	3/4	1"
470+40	C	1"	5/8	7/8	476+40	C	5/8	15/16	13/16
470+60	C	3/4	13/16	3/4	476+60	C	15/16	1"	1-1/8
470+80	C	3/4	7/8	3/4	476+80	C	3/4	1-5/16	15/16
471+00	C	3/4	3/4	5/8	477+00	C	15/16	3/4	3/4
471+20	C	13/16	3/4	3/4	477+20	C	13/16	1/2	7/8
471+40	C	13/16	3/4	9/16	477+40	C	15/16	1"	7/8
471+60	C	1/2	11/16	5/8	477+60	C	5/8	1"	7/8
471+80	C	13/16	5/8	13/16	477+80	C	13/16	13/16	11/16
472+00	C	3/4	7/8	5/8	478+00	Ex.	1/2	3/8	7/16
472+20	C	1/2	11/16	11/16	478+20	C	7/8	1"	1"
472+40	C	3/4	3/4	5/8	478+40	C	7/8	1"	1"
472+60	C	5/8	13/16	5/8	478+60	C	15/16	7/8	5/8
472+80	C	7/8	1/2	7/8	478+80	C	3/4	1"	13/16
473+00	C	7/8	1"	3/4	479+00	C	7/8	7/8	3/4
473+20	C	7/8	3/4	7/8	479+20	C	1"	1"	3/4
473+40	C	5/8	7/8	3/4					



Sta.	Type	Lt.	C.L.	Rt.	Sta.	Type	Lt.	C.L.	Rt.
479+40	C	13/16	1-3/16	1"	485+00	C	1/2	11/16	3/4
479+60	C	15/16	15/16	13/16	485+20	C	13/16	13/16	13/16
479+80	C	1"	1"	1"	485+40	C	3/4	13/16	1"
480+00	C	5/8	1"	3/4	485+60	C	1/2	11/16	5/8
480+20	C	5/8	7/8	3/4	485+80	C	5/8	7/8	5/8
480+40	C	7/8	7/8	13/16	486+00	Ex.	9/16	7/16	1/2
480+60	C	5/8	3/4	3/4	486+20	C	3/4	3/4	13/16
480+80	C	5/8	3/4	1/2	486+40	C	11/16	11/16	13/16
481+00	C	9/16	1"	1"	486+60	C	3/4	3/4	5/8
481+20	C	3/4	5/8	3/4	486+80	C	5/8	9/16	9/16
481+40	C	7/8	1"	1"	487+00	C	3/4	11/16	3/4
481+60	C	13/16	1"	1"	487+20	C	5/8	7/8	1"
481+80	C	7/8	1"	5/8	487+40	C	9/16	11/16	11/16
482+00	C	5/8	3/4	5/8	487+60	C	5/8	3/4	3/4
482+20	C	9/16	3/4	5/8	487+80	C	3/4	3/4	5/8
482+32.3	Const. Jt.				488+00	C	7/16	1/4	5/8
482+40	C	3/4	3/4	7/8	488+20	C	7/16	3/4	7/8
482+60	C	11/16	3/4	9/16	488+40	C	5/8	7/8	3/4
482+80	C	13/16	1"	3/4	488+60	C	1/2	5/8	9/16
483+00	C	9/16	3/4	3/4	488+80	C	5/8	11/16	13/16
483+20	C	3/4	3/4	13/16	489+00	C	1/2	11/16	3/4
483+40	C	11/16	13/16	7/8	489+20	C	1/2	9/16	5/8
483+60	C	3/4	3/4	3/4	489+40	C	3/4	5/8	13/16
483+80	C	11/16	3/4	7/8	489+60	C	3/4	3/4	3/4
484+00	C	11/16	3/4	7/8					
484+20	C	13/16	7/8	5/8					
484+40	C	13/16	7/8	15/16					
484+60	C	13/16	1"	3/4					
484+80	C	9/16	11/16	3/4					



Sta.	Type	Lt.	C.L.	Rt.	Sta.	Type	Lt.	C.L.	Rt.
489+80	C	5/8	5/8	5/8	495+60	C	3/4	7/8	7/8
490+00	C	1/2	3/4	11/16	495+80	C	11/16	15/16	13/16
490+20	C	7/16	1"	11/16	496+00	C	3/4	15/16	7/8
490+40	C	1/2	1"	13/16	496+20	C	7/8	7/8	7/8
490+60	C	3/4	1/2	1"	496+40	C	3/4	1"	3/4
490+80	C	13/16	15/16	7/8	496+60	C	15/16	7/8	13/16
491+00	C	1/2	5/8	3/4	496+80	C	3/4	1"	15/16
491+20	C	9/16	13/16	3/4	497+00	Const. Jt.			
491+40	C	7/8	1"	7/8	497+20	C	3/8	9/16	11/16
491+60	C	13/16	1"	11/16	497+40	C	7/16	1/2	3/4
491+80	C	7/8	15/16	3/4	497+60	C	3/4	5/8	5/8
492+00	C	11/16	1/2	13/16	497+80	C	1/2	7/16	3/4
492+20	C	5/16	7/8	7/8	498+00	C	5/8	5/8	7/8
492+40	C	3/4	7/8	7/8	498+20	C	5/8	11/16	11/16
492+60	C	15/16	1"	13/16	498+40	C	11/16	5/8	1/2
492+80	C	3/4	1"	13/16	498+60	C	1"	13/16	13/16
493+00	C	3/4	1"	1"	498+80	C	3/4	11/16	3/4
493+20	C	7/8	7/8	7/8	499+00	C	13/16	13/16	11/16
493+40	C	11/16	3/4	3/4	499+20	C	1/2	3/4	5/8
493+60	C	3/4	1"	13/16	499+40	C	3/4	13/16	13/16
493+80	C	11/16	7/8	3/4	499+60	C	7/16	7/16	3/4
494+00	Ex.	9/16	1/4	9/16	499+80	C	15/16	9/16	11/16
494+20	C	3/4	13/16	3/4	500+00	C	3/4	11/16	7/8
494+40	C	3/4	1"	7/8	500+20	C	3/4	7/16	11/16
494+60	C	13/16	7/8	13/16	500+40	C	9/16	7/16	13/16
494+80	C	15/16	1-1/8"	1"	500+60	C	7/16	3/4	3/4
495+00	C	13/16	1"	11/16	500+80	C	9/16	3/4	13/16
495+20	C	7/8	1"	3/4	501+00	C	13/16	7/8	5/8
495+40	C	5/8	13/16	13/16	501+20	C	11/16	3/4	3/4



Sta.	Type	Lt.	C.L.	Rt.	Sta.	Type	Lt.	C.L.	Rt.
501+40	C	9/16	5/8	1"	507+20	C	7/8	15/16	7/8
501+60	C	15/16	13/16	13/16	507+40	C	11/16	7/8	13/16
501+80	C	13/16	15/16	7/8	507+60	C	7/8	7/8	11-1/16
502+00	Ex.	5/16	3/16	3/8	507+80	C	7/8	15/16	1-1/16
502+20	C	13/16	11/16	13/16	508+00	C	1"	1-1/8	7/8
502+40	C	13/16	11/16	3/4	508+20	C	1-1/8	1"	1-1/16
502+60	C	5/8	5/8	11/16	508+40	C	3/4	1	13/16
502+80	C	9/16	13/16	11/16	508+60	C	13/16	1-1/16	7/8
503+00	C	1/2	7/8	13/16	508+80.0	Const. Jt.			
503+20	C	7/16	11/16	5/8	509+00	C	5/8	13/16	5/8
503+40	C	1/2	5/8	11/16	509+20	C	5/8	1/2	5/8
503+60	C	7/8	11/16	13/16	509+40	C	5/8	3/4	9/16
503+80	C	7/8	3/4	3/4	509+60	C	5/8	15/16	3/4
504+00	C	7/16	1/2	13/16	509+80	C	11/16	11/16	1/2
504+20	C	3/4	9/16	3/4	510+00	Ex.	11/16	1/8	3/16
504+40	C	3/4	9/16	7/8	510+25	C	7/16	5/8	9/16
504+60	C	3/4	3/4	1"	510+45	C	5/8	7/8	5/8
504+80	C	15/16	3/4	15/16	510+65	C	3/4	15/16	1/2
505+00	C	15/16	15/16	1-1/16	510+85	C	11/16	3/4	5/8
505+20	C	7/8	7/8	13/16	511+05	C	13/16	5/8	5/8
505+40	C	3/4	7/8	7/8	511+25	C	9/16	3/4	3/4
505+60	C	7/8	3/4	1-1/16	511+45	C	3/4	3/4	11/16
505+80	C	11/16	15/16	1"	511+65	C	9/16	9/16	11/16
506+00	C	7/8	7/8	3/4	511+85	C	1-1/16	7/8	11/16
506+20	C	3/4	15/16	11/16	512+05	C	5/16	9/16	9/16
506+40	C	5/8	7/8	11/16	512+25	C	5/8	1/2	3/4
506+60	C	3/4	13/16	15/16	512+45	C	1-3/16	1-3/16	9/16
506+80	C	7/8	3/4	13/16	512+65	C	3/4	3/4	9/16
507+00	C	5/8	7/8	13/16	512+85	C	7/16	3/8	11/16



Sta.	Type	Lt.	C.L.	Rt.	Sta.	Type	Lt.	C.L.	Rt.
513+05	C	1-1/8	15/16	9/16	518+84	C	7/8	1"	1-1/16
513+25	C	13/16	7/16	3/4	519+04	C	7/8	1-3/8	1-1/16
513+45	C	1/2	7/16	3/4	519+24	C	3/4	1-1/8	3/4
513+65	C	7/16	1/2	9/16	519+44	C	3/4	11/16	7/8
513+85	C	11/16	9/16	13/16	519+64	C	13/16	3/4	15/16
514+05	C	1/2	5/8	5/8	519+84	C	5/8	7/8	7/8
514+25	C	1/2	5/8	3/4	520+04	C	13/16	13/16	3/4
514+45	C	1/2	7/16	5/8	520+24	C	13/16	1"	7/8
514+65	C	3/4	13/16	3/4	520+44	C	13/16	1-1/16	3/4
514+85	C	7/16	9/16	5/8	520+64	C	1"	1-1/16	1"
515+05	C	3/4	13/16	3/8	520+84	C	3/4	7/8	13/16
515+24	C	9/16	7/8	3/4	521+04	C	3/4	3/4	7/8
515+44	C	3/4	1-1/8	11/16	521+24.0 Const. Jt.				
515+64	C	5/8	15/16	7/8	521+43	C	1/2	9/16	5/8
515+84	C	11/16	13/16	3/4	521+63	C	7/16	13/16	5/8
516+04	C	1/2	1-1/8	5/8	521+83	C	3/4	3/4	11/16
516+24	C	5/8	1-3/16	3/4	522+03	C	5/8	5/8	11/16
516+44	C	7/8	7/8	13/16	522+23	C	11/16	7/16	5/8
516+64	C	3/4	1-1/16	13/16	522+43	C	5/16	1/2	1/2
516+84	C	7/8	15/16	13/16	522+63	C	11/16	13/16	3/4
517+04	C	5/8	3/4	9/16	522+83	C	11/16	13/16	11/16
517+24	C	13/16	5/8	13/16	523+03	C	3/4	5/8	9/16
517+44	C	3/4	1-1/16	1-1/8	523+23	C	1/4	3/4	13/16
517+64	C	7/8	13/16	7/8	523+43	C	13/16	13/16	5/8
517+84	C	13/16	7/8	1"	523+63	C	13/16	9/16	3/4
518+04	C	3/4	13/16	3/4	523+83	C	3/4	13/16	5/8
518+24	C	7/8	1-3/16	1-1/16	524+03	C	9/16	5/8	3/8
518+44	C	1-1/16	1-1/4	7/8	524+23	C	11/16	11/16	5/8
518+64	C	15/16	7/8	3/4	524+43	C	1/2	7/8	7/8



Sta.	Type	Lt.	C.L.	Rt.	Sta.	Type	Lt.	C.L.	Rt.
524+63	C	5/8	11/16	11/16	530+63	C	13/16	13/16	7/8
524+83	C	11/16	7/16	5/8	530+83	C	7/8	9/16	11/16
525+03	C	3/4	7/8	13/16	531+03	C	15/16	1-1/8	15/16
525+23	C	7/8	11/16	15/16	531+23	C	11/16	7/8	7/8
525+43	C	3/4	5/8	11/16	531+43	C	7/8	1-1/8	7/8
525+63	C	5/8	5/8	3/4	531+63	C	13/16	3/8	7/8
525+83	C	1/8	11/16	5/8	531+83	C	1-1/16	7/8	5/8
526+03	C	1/2	9/16	1/2	532+03	C	13/16	13/16	3/4
526+23	C	1/2	11/16	5/8	532+23	C	7/8	1"	7/8
526+43	C	3/4	13/16	9/16	532+43	C	3/4	15/16	7/8
526+63	C	1/2	9/16	1/2	532+63	C	15/16	3/8	15/16
526+83	C	9/16	9/16	11/16	532+83	C	13/16	1/2	13/16
527+03	C	7/16	1/2	1/2	533+03	C	3/4	7/8	9/16
527+23	C	9/16	1/2	5/8	533+23	C	11/16	1"	7/8
527+43	C	7/16	11/16	5/8	533+43	C	9/16	3/8	13/16
527+63	C	3/8	5/8	9/16	533+63	C	7/8	9/16	11/16
527+83	C	1/2	9/16	1/2	533+83	C	11/16	1-1/16	13/16
528+03	C	3/4	13/16	3/4	534+03	C	15/16	13/16	3/4
528+23	C	7/8	3/4	9/16	534+23	C	5/8	3/4	3/4
528+43	C	11/16	7/8	7/8	534+44.0	Const. Jt.			
528+63	C	13/16	1-1/16	13/16	534+63	C	11/16	5/8	3/4
528+83	C	7/8	15/16	7/8	534+83	C	5/8	1/2	3/4
529+03	C	11/16	7/8	7/8	535+03	C	11/16	5/8	9/16
529+23	C	7/8	3/4	15/16	535+23	C	9/16	3/4	5/16
529+43	C	15/16	13/16	11/16	535+43	C	7/16	1/2	11/16
529+63	C	3/4	7/8	3/4	535+63	C	7/16	9/16	3/4
529+83	C	13/16	3/4	3/4	535+83	C	9/16	7/16	3/4
530+03	C	3/4	1-1/16	13/16	536+03	C	1/2	5/8	1/2
530+23	C	1"	15/16	13/16	536+23	C	5/16	13/16	11/16
530+43	C	7/8	1-3/16	7/8					



Sta.	Type	Lt.	C.L.	Rt.	Sta.	Type	Lt.	C.L.	Rt.
536+43	C	7/16	7/8	13/16	542+23	C	3/4	3/4	7/8
536+63	C	7/16	7/16	5/8	542+43	C	3/4	7/8	7/8
536+83	C	1/2	5/8	11/16	542+63	C	9/16	1/2	5/8
537+03	C	7/16	1/2	13/16	542+83	C	3/4	1-1/16	1-1/16
537+23	C	1/2	7/16	1/2	543+03	C	7/16	5/8	7/8
537+43	C	5/8	9/16	5/8	543+23	C	1"	7/8	1"
537+63	C	5/8	1/2	5/8	543+43	C	7/8	7/8	7/8
537+83	C	9/16	7/16	1/2	543+63	C	1"	5/8	3/4
538+03	C	5/8	3/4	5/8	543+83	C	7/8	15/16	1-1/8
538+23	C	1/2	3/4	5/8	544+03	C	1-1/4	13/16	7/8
538+43	C	9/16	1/2	13/16	544+22	C	1"	7/8	15/16
538+63	C	3/4	11/16	1/2	544+42	C	1"	13/16	13/16
538+83	C	7/16	1/2	3/4	544+62	C	1"	11/16	13/16
539+03	C	1/2	5/8	3/4	544+82	C	3/4	13/16	3/4
539+23	C	5/8	7/8	3/4	545+02	C	11/16	3/4	11/16
539+43	C	1/2	11/16	11/16	545+22	C	13/16	3/4	1"
539+63	C	3/4	3/4	9/16	545+42	C	7/8	13/16	15/16
539+83	C	5/8	5/8	1"	545+62	C	13/16	7/8	7/8
540+03	C	5/8	5/8	5/8	545+82	C	15/16	5/8	15/16
540+23	C	1/2	9/16	1/2	546+02	C	3/4	1/2	7/8
540+43	C	5/8	11/16	7/16	546+22	C	3/4	15/16	3/4
540+63	C	3/8	5/8	5/8	546+31.8 Const. Jt.				
540+83	C	3/4	7/8	7/8	546+42	C	7/16	5/8	7/8
541+03	C	3/4	13/16	3/4	546+62	C	1"	5/8	7/8
541+23	C	7/8	7/8	7/8	546+82	C	13/16	7/8	13/16
541+43	C	1"	15/16	15/16	547+02	C	1"	7/8	7/8
541+63	C	3/4	7/8	15/16	547+22	C	15/16	1"	3/4
541+83	C	7/8	7/8	3/4	547+42	C	3/4	5/8	1"
542+03	C	5/8	5/8	3/4	547+62	C	13/16	5/8	3/4



Sta.	Type	Lt.	C.L.	Rt.	Sta.	Type	Lt.	C.L.	Rt.
547+82	C	7/8	11/16	7/16	553+42	C	5/8	5/8	3/4
548+02	C	1/2	3/8	1/2	553+62	C	5/8	5/8	1"
548+22	C	7/8	1"	13/16	553+82	C	13/16	3/4	11/16
548+42	C	3/4	3/4	11/16	554+02	C	13/16	11/16	13/16
548+62	C	13/16	1/2	5/8	554+22	C	3/4	7/8	5/8
548+82	C	3/4	3/4	9/16	554+42	C	15/16	1"	13/16
549+02	C	7/8	5/8	11/16	554+62	C	11/16	3/4	7/8
549+22	C	1/16	3/4	11/16	554+82	C	3/4	11/16	3/4
549+42	C	13/16	11/16	15/16	555+02	C	3/4	5/8	3/4
549+62	C	7/8	13/16	15/16	555+20	C	3/4	5/8	3/4
549+82	C	5/8	3/4	15/16	555+40	C	1/2	11/16	13/16
550+02	C	5/8	3/4	11/16	555+60	C	11/16	1/2	11/16
550+22	C	1/2	3/4	9/16	555+80	C	1/2	1/2	3/4
550+42	C	13/16	7/8	3/4	556+00	C	11/16	11/16	13/16
550+62	C	3/4	15/16	7/8	556+20	C	3/4	15/16	13/16
550+82	C	5/8	13/16	13/16	556+40	C	11/16	3/4	13/16
551+02	C	1/2	5/8	3/4	556+60	C	3/4	11/16	1"
551+22	C	3/4	1"	3/4	556+80	C	3/4	7/8	7/8
551+42	C	1/2	5/8	5/8	557+00	C	15/16	3/4	3/4
551+62	C	5/8	1/2	3/4	557+20	C	9/16	3/4	3/4
551+82	C	3/4	3/8	11/16	557+40	C	7/16	11/16	1/2
552+02	C	5/8	3/4	13/16	557+60.3 Const. Jt.				
552+22	C	3/4	7/8	13/16	557+80	C	11/16	3/4	13/16
552+42	C	3/4	5/8	1"	558+00	C	5/8	3/8	3/8
552+62	C	7/8	5/8	11/16	558+20	C	3/4	3/4	1/2
552+82	C	1-1/16	11/16	13/16	558+40	C	1/2	9/16	3/4
553+02	C	3/4	1/2	13/16	558+60	C	5/8	7/8	13/16
553+22	C	13/16	13/16	13/16	558+80	C	5/8	11/16	1"



Sta.	Type	Lt.	C.L.	Rt.	Sta.	Type	Lt.	C.L.	Rt.
559+00	C	7/16	3/4	3/8	567+01	C	7/16	5/8	7/16
559+20	C	1"	5/8	1/2	567+31	C	5/8	1/2	1/2
559+40	C	7/8	5/8	3/4	567+61	Ex.	3/8	7/16	7/16
559+60	C	3/4	5/8	3/4	567+91	C	5/8	7/16	7/16
559+80	C	15/16	11/16	11/16	568+00.5	Const. Jt.			
560+00	C	5/8	9/16	11/16	568+21	C	1/2	3/8	7/16
560+21	C	9/16	9/16	1/2	568+51	C	1/4	7/16	5/16
560+41	Ex.	3/8	9/16	9/16	568+81	Ex.	3/8	3/8	3/8
560+71	C	5/16	9/16	7/16	569+11	C	3/8	3/8	1/2
561+01	C	7/16	1/2	7/16	569+41	C	1/2	5/16	3/8
561+31	C	1/2	1/2	1/2	569+71	C	1/4	7/16	1/2
561+61	Ex.	5/16	5/16	1/2	570+01	Ex.	3/8	7/16	3/8
561+91	C	3/8	7/16	5/8	570+32	C	1/8	1/8	9/16
562+21	C	1/2	7/16	1/2	570+62	C	3/8	9/16	7/16
562+51	C	3/8	3/8	3/8	570+92	C	5/16	5/16	5/16
562+81	Ex.	3/8	5/16	5/16	571+22	Ex.	1/4	1/4	9/16
563+11	C	1/4	1/2	3/8	571+52	C	3/8	0	7/16
563+41	C	1/2	7/16	5/8	571+82	C	7/16	3/8	5/8
563+71	C	1/2	3/4	3/8	572+12	C	3/8	1/4	6/16
564+01	Ex.	5/8	5/16	3/8	572+42	Ex.	3/4	7/16	7/16
564+31	C	1/2	1/2	9/16	572+72	C	1/4	3/16	7/16
564+61	C	3/8	1/2	1/2	573+02	C	3/8	3/8	1/2
564+91	C	9/16	3/4	1/2	573+32	C	11/16	5/8	1/2
565+21	Ex.	1/4	5/16	3/8	573+62	Ex.	1/2	3/16	1/2
565+51	C	5/8	7/16	7/16	573+92	C	11/16	5/16	3/8
565+81	C	3/8	1/2	9/16	574+22	C	11/16	3/8	1/2
566+11	C	1/2	1/2	9/16	574+52	C	3/8	5/8	5/8
566+41	Ex.	1/2	3/8	1/4	574+82	Ex.	11/16	5/8	1/2
566+71	C	7/16	1/2	3/8	575+12	C	5/8	7/16	9/16



Sta.	Type	Lt.	C.L.	Rt.	Sta.	Type	Lt.	C.L.	Rt.
575+42	C	1/2	9/16	9/16	585+21.3	Ex.	3/4	5/16	1/2
575+72	C	3/4	1/2	11/16	585+51.3	C	3/4	1/2	9/16
576+02	Ex.	9/16	0	3/8	585+81.0	Const. Jt.			
576+32	C	1/2	5/8	13/16	586+11.3	C	5/16	1/2	5/8
576+62	C	7/16	7/16	1/2	586+40.7	Ex.	1/2	15/16	1"
576+92	C	3/8	5/16	13/16	586+61.0	Bridge Begin			
577+22	Ex.	3/4	13/16	3/8	588+26.0	Bridge End			
577+52	C	9/16	1/2	1/2	588+47.4	Ex.	9/16	1-3/16	3/8
577+82	C	1/2	9/16	11/16	588+76	C	5/16	7/16	3/8
578+12	C	11/16	1/2	3/4	589+08.5	C	1/2	7/16	1/2
578+42	Ex.	7/16	1/8	5/16	589+41	C	7/16	1/2	1/2
578+72	C	1/2	7/16	9/16	589+71	C	1/2	5/16	1/2
579+02.0	C	7/16	7/16	1/8	590+01	Ex.	1/2	1/2	1/2
579+32	C	1/8	3/8	3/8	590+31	C	7/16	5/16	3/8
579+62	Ex.	5/16	3/16	3/8	590+61	C	9/16	3/8	7/16
579+92	C	7/16	3/8	5/8	590+91	C	7/16	3/8	1/2
580+22	C	5/8	3/8	1/2	591+21	Ex.	1/2	1/2	7/16
580+52	C	5/8	3/8	1/2	591+51	C	3/4	13/16	5/8
580+81	Ex.	1/2	1-3/16	7/8	591+81	C	3/4	1/2	1/2
581+02.0	Bridge Begin				592+11	C	9/16	9/16	3/4
582+67.0	Bridge End				592+41	Ex.	3/4	1/2	1/2
582+89.7	Ex.	7/8	1/2	1"	592+71	C	5/8	5/8	5/8
583+18.7	C	1"	3/4	1-1/8	593+01	C	1/2	3/8	7/8
583+42.4	C	1/2	1/2	5/8	593+31	C	5/8	1/2	5/8
583+72.5	C	9/16	1/2	1/2	593+61	Ex.	1/2	1/2	1/2
584+00.7	Ex.	5/8	3/16	3/16	593+91	C	3/4	3/4	3/4
584+30.7	C	5/8	1/2	7/16	594+21	C	3/4	9/16	9/16
584+61.3	C	1/2	1/2	9/16	594+50.8	C	3/16	1/4	3/8
584+91.3	C	1/2	1/2	9/16	594+79.8	Ex.	1-1/2	1-1/2	1-3/4



Sta.	Type	Lt.	C.L.	Rt.	Sta.	Type	Lt.	C.L.	Rt.
595+01.0	Bridge Begin				605+80	C	1/4	1/4	1/2
596+66.0	Bridge End				606+08.7	C	3/8	9/16	7/16
596+87.4	Ex.	15/16	1-3/4	5/8	606+37.5	C	5/8	11/16	9/16
597+16	C	9/16	1/2	1/2	606+66	Ex.	5/16	1/8	1/2
597+40	C	5/8	3/8	1/2	606+95	C	3/8	1/2	1/2
597+65	Ex.	9/16	5/16	1/2	607+23.6	C	1/2	1/2	1/2
597+95	C	3/4	5/8	1/2	607+52.4	C	11/16	5/8	3/4
598+25	C	5/8	1/2	5/8	607+81.0	Ex.	4/16	3/16	3/8
598+55	Ex.	3/4	7/16	9/16	608+10.0	C	3/4	11/16	3/4
598+85	C	5/8	1/2	9/16	608+38.6	C	11/16	13/16	5/8
599+15	C	3/4	5/16	5/8	608+66.2	C	7/8	1"	3/4
599+45	C	9/16	1/2	3/8	608+96	Ex.	1/2	7/8	3/8
599+75	Ex.	3/4	7/16	1/2	609+16.6	Bridge Begin			
600+05	C	1/2	3/8	7/16	610+82.0	Bridge End			
600+35	C	9/16	3/8	9/16	611+02.6	Ex.	11/16	1-1/16	1"
600+68	C	5/16	3/8	5/8	611+32.2	C	9/16	1/2	5/8
600+95	Ex.	1-1/2	1-1/2	1"	611+57.1	C	3/4	1/4	1/2
601+14.5	Bridge Begin Skew				611+84.4	C	3/8	7/16	7/16
602+99.5	Bridge End Skew				612+10	Ex.	5/16	1/4	7/16
603+20.2	Ex.	1/2	1-11/16	1"	612+37.5	C	3/4	1/2	5/8
603+49	C	5/8	9/16	3/8	612+65	C	1/2	9/16	11/16
603+78.7	C	1/2	1/4	11/16	612+90	C	9/16	5/16	11/16
604+07.3	C	3/4	1/2	1/2	613+20	Ex.	7/16	3/8	3/8
604+36	Ex.	7/16	5/16	1/2	613+50	C	5/8	3/8	3/4
604+65.0	C	9/16	3/8	5/8	613+80	C	3/16	1/2	5/8
604+73.0	Const. Jt.				614+10	C	5/8	7/16	7/8
604+93.7	C	1/2	7/16	9/16	614+40	Ex.	9/16	7/16	1/2
605+22.3	C	5/8	3/8	7/16	614+70	C	9/16	1/2	11/16
605+51	Ex.	1/4	1/8	1/4	615+00	C	3/4	9/16	11/16



Sta.	Type	Lt.	C.L.	Rt.
615+30	C	5/8	11/16	11/16
615+60	Ex.	9/16	3/8	3/8
615+90	C	1/2	1/2	9/16
616+20	C	11/16	1/2	5/8
616+50	C	3/8	9/16	3/4
616+80	Ex.	1/2	7/16	9/16
617+10	C	11/16	1/2	7/8
617+40	C	5/8	1/2	1/2
617+70	C	1/2	9/16	5/8
618+00	Ex.	3/8	5/16	1/2
618+30	C	5/8	1/2	11/16
618+60	C	1/2	9/16	1/2
618+90	C	9/16	3/8	3/8
619+20	Ex.	1/2	3/8	7/16
619+50	C	3/8	9/16	9/16
619+80	C	1/2	9/16	11/16
620+10.0	Const. Jt.			
620+40	Ex.	3/8	7/16	1/2
620+70	C	1/2	1/2	1/2
621+00	C	1/2	3/8	9/16
621+30	C	5/16	1/4	5/8
621+60	Ex.	5/16	3/8	5/8
621+90	C	5/8	3/8	9/16
622+20	C	3/4	11/16	5/8
622+50	C	5/8	1/4	9/16
622+80	Ex.	5/16	5/16	7/16
623+10	C	1/2	3/8	9/16
623+40	C	9/16	1/2	5/8
623+70	C	3/4	1/2	11/16



Sta.	Type	Lt.	C.L.	Rt.	Sta.	Type	Lt.	C.L.	Rt.
624+00	Ex.	7/16	3/16	9/16	631+60	C	15/16	3/4	3/4
624+30	C	1/2	3/8	9/16	631+80	C	1/2	7/8	13/16
624+60	C	1/2	1/2	5/8	632+00	C	11/16	13/16	13/16
624+90	C	1/2	7/16	1/2	632+20	C	5/8	3/4	3/4
625+20	Ex.	7/16	1/4	7/16	632+40	C	5/8	5/8	11/16
625+50	C	5/8	1/2	5/8	632+60	C	3/4	5/8	5/8
625+80	C	1/2	3/8	3/4	632+80	Ex.	9/16	1/2	5/8
626+10	C	1/2	3/8	9/16	633+00	C	13/16	3/4	7/8
626+40	Ex.	1/2	1/2	11/16	633+20	C	7/8	1-1/16	15/16
626+70	C	1/2	7/16	5/8	633+40	C	11/16	1"	15/16
627+00	C	5/8	5/8	9/16	633+60	C	9/16	7/8	3/4
627+30	C	5/8	5/16	9/16	633+80	C	9/16	3/4	13/16
627+60	Ex.	9/16	1/2	1/2	634+00	C	3/4	3/4	15/16
627+90	C	7/8	5/8	5/8	634+20	C	15/16	11/16	13/16
628+20	C	3/4	1/2	3/4	634+40	C	9/16	11/16	7/8
628+50	C	1/2	5/16	9/16	634+60	C	11/16	15/16	3/4
628+80	Ex.	1/2	1/2	3/4	634+80	C	5/8	11/16	5/8
629+10	C	11/16	5/8	3/4	635+00	C	3/4	3/4	13/16
629+29.6	Const. Jt.				635+20	C	1"	13/16	7/16
629+40	C	7/16	1/2	1/2	635+40	C	9/16	5/8	11/16
629+70	C	9/16	3/4	9/16	635+60	C	1/2	1/2	9/16
630+00	Ex.	5/16	13/16	1/2	635+80	C	7/16	1/4	11/16
630+20	C	3/4	13/16	11/16	636+00	C	11/16	13/16	9/16
630+40	C	13/16	13/16	11/16	636+20	C	1/2	5/8	1/2
630+60	C	11/16	11/16	7/8	636+40	C	11/16	13/16	1/2
630+80	C	5/8	9/16	9/16	636+60	C	11/16	5/8	9/16
631+00	C	5/8	1/2	5/8	636+80	C	11/16	3/4	5/8
631+20	C	5/8	5/8	3/4	637+00	C	11/16	9/16	9/16
631+40	C	13/16	9/16	3/4	637+20	C	11/16	9/16	11/16
					637+40	C	9/16	13/16	5/8



Sta.	Type	Lt.	C.L.	Rt.	Sta.	Type	Lt.	C.L.	Rt.
637+60	C	1/2	1/2	5/8	643+40	C	9/16	3/4	3/4
637+80	C	9/16	3/4	11/16	643+60	C	7/8	13/16	15/16
638+00	C	7/16	9/16	9/16	643+80	C	9/16	1/2	3/4
638+20	C	9/16	11/16	11/16	644+00	C	1/2	13/16	9/16
638+40	C	3/4	7/8	1/2	644+20	C	3/4	5/8	13/16
638+60	C	3/4	3/4	1/2	644+40	C	11/16	1"	11/16
638+80	C	1/2	11/16	3/4	644+60	C	1/2	3/4	3/4
639+00	C	7/16	5/8	11/16	644+80	C	11/16	9/16	9/16
639+20	C	5/8	9/16	11/16	645+00	C	5/16	1/2	5/8
639+40	C	13/16	5/8	3/4	645+20	C	7/16	3/4	5/8
639+60	C	13/16	3/4	3/4	645+40	C	1/2	3/4	9/16
639+80	C	5/8	7/8	9/16	645+60	C	11/16	1/2	3/4
640+00	C	5/8	5/8	13/16	645+80	C	5/8	13/16	3/4
640+20	C	13/16	15/16	1"	646+00	C	7/16	7/16	5/8
640+40	C	7/8	11/16	10/16	646+20	C	11/16	13/16	13/16
640+60	C	13/16	7/8	7/8	646+40	C	11/16	7/8	1"
640+80	Ex.	7/16	11/16	13/16	646+60	C	3/4	1"	15/16
640+99.7	Const. Jt.				646+80	C	3/4	15/16	15/16
641+20	C	11/16	5/8	3/4	647+00	C	7/8	15/16	15/16
641+40	C	3/4	11/16	15/16	647+20	C	5/8	7/8	7/8
641+60	C	3/4	9/16	3/4	647+40	C	1/2	7/8	7/8
641+80	C	13/16	13/16	1-1/16	647+60	C	3/8	1/2	1/2
642+00	C	3/4	15/16	13/16	647+80	C	1/2	9/16	5/8
642+20	C	1/2	3/8	9/16	648+00	C	5/8	13/16	11/16
642+40	C	11/16	15/16	7/8	648+20	C	11/16	5/8	5/8
642+60	C	1"	7/8	1"	648+40	C	5/8	9/16	7/8
642+80	C	3/4	5/8	11/16	648+60	C	11/16	9/16	9/16
643+00	C	5/8	9/16	1/2	648+80	Ex.	1/4	5/16	1/2
643+20	C	5/8	13/16	11/16	649+00	C	11/16	9/16	9/16



Sta.	Type	Lt.	C.L.	Rt.	Sta.	Type	Lt.	C.L.	Rt.
649+20	C	5/8	13/16	3/4	655+00	C	5/8	7/8	7/8
649+40	C	11/16	11/16	9/16	655+20	C	1/2	5/8	3/4
649+60	C	3/8	9/16	3/4	655+40	C	5/8	9/16	11/16
649+80	C	9/16	3/4	5/8	655+60	C	9/16	13/16	7/8
650+00	C	5/8	5/8	3/4	655+80	C	3/4	7/8	7/8
650+20	C	5/8	13/16	5/8	656+00	C	1/2	3/4	3/4
650+40	C	5/8	11/16	5/8	656+20	C	11/16	5/8	7/8
650+60	C	1/2	9/16	11/16	656+40	C	11/16	3/4	3/4
650+80	C	9/16	5/8	9/16	656+60	C	3/4	1/2	3/4
651+00	C	1/2	5/8	5/8	656+80	Ex.	7/16	7/16	3/4
651+20	C	9/16	5/8	1/2	657+00	C	5/8	3/4	11/16
651+40	C	11/16	10/16	9/16	657+20	C	11/16	9/16	1"
651+60	C	7/16	9/16	3/4	657+40	C	3/4	3/4	7/8
651+80	C	5/8	9/16	3/4	657+60	C	3/4	11/16	13/16
652+00	C	7/16	9/16	11/16	657+80	C	1/2	7/8	3/4
652+20	C	9/16	11/16	11/16	658+00	C	1/2	11/16	7/8
652+40	C	11/16	11/16	1/2	658+20	C	1/2	3/4	5/8
652+60	C	9/16	5/8	9/16	658+40	C	5/8	1"	1"
652+80	C	7/16	1/2	7/16	658+60	C	1/2	9/16	3/4
653+00	C	3/8	7/16	9/16	658+80	C	1/2	5/8	13/16
653+20	C	9/16	7/16	1/2	659+00	C	5/8	3/4	3/4
653+40	C	1/2	9/16	1/2	659+20	C	3/4	5/8	5/8
653+60	C	9/16	9/16	11/16	659+40	C	11/16	13/16	5/8
653+80	C	1/2	5/8	5/8	659+60	C	1/2	7/8	13/16
654+00	O Const. Jt.				659+80	C	9/16	3/4	3/4
654+20	C	7/16	9/16	9/16	660+00	C	7/16	11/16	13/16
654+40	C	9/16	5/8	11/16	660+20	C	5/8	5/8	7/8
654+60	C	1/2	13/16	3/4	660+40	C	7/8	7/8	1/2
654+80	C	11/16	13/16	7/8	660+60	C	1/2	5/8	5/8



Sta.	Type	Lt.	C.L.	Rt.	Sta.	Type	Lt.	C.L.	Rt.
660+80	Ex.	7/16	7/16	7/16	666+60	C	3/4	5/8	3/4
661+00	C	7/16	3/4	7/8	666+80	C	1/2	9/16	3/4
661+20	C	9/16	1/2	11/16	667+00	C	3/8	1/8	9/16
661+40	C	5/8	1/2	9/16	667+19.6	Const. Jt.			
661+60	C	1/2	9/16	1/2	667+40	C	3/4	3/4	5/8
661+80	C	7/16	5/8	9/16	667+60	C	3/8	1/2	11/16
662+00	C	7/16	9/16	7/16	667+80	C	11/16	11/16	9/16
662+20	C	7/16	9/16	5/8	668+00	C	3/4	3/4	3/4
662+40	C	5/8	5/8	11/16	668+20	C	9/16	1/2	3/4
662+60	C	5/8	11/16	7/16	668+40	C	3/4	3/4	3/4
662+80	C	3/4	5/8	5/8	668+60	C	5/8	9/16	7/8
663+00	C	5/8	5/8	3/4	668+80	Ex.	1/4	7/16	9/16
663+20	C	1/2	7/16	11/16	669+00	C	5/8	11/16	15/16
663+40	C	1/2	7/16	9/16	669+20	C	13/16	1/2	15/16
663+60	C	7/16	7/16	5/8	669+40	C	1/2	3/4	3/4
663+80	C	9/16	5/8	9/16	669+60	C	1/2	1/4	3/4
664+00	C	1/2	9/16	7/16	669+80	C	5/8	5/8	1/2
664+20	C	5/8	9/16	7/16	670+00	C	3/4	3/4	3/4
664+40	C	1/2	1/2	1/2	670+20	C	3/4	5/8	5/8
664+60	C	11/16	5/8	11/16	670+40	C	1/2	9/16	7/8
664+80	Ex.	7/16	5/16	5/16	670+60	C	5/8	9/16	3/4
665+00	C	5/8	1/2	7/16	670+80	C	11/16	3/4	11/16
665+20	C	1/2	7/16	5/8	671+00	C	11/16	3/4	7/8
665+40	C	7/16	7/16	9/16	671+20	C	1/2	1/2	3/4
665+60	C	9/16	7/16	5/8	671+40	C	5/8	3/8	5/8
665+80	C	5/8	5/8	7/16	671+60	C	3/4	3/4	1/2
666+00	C	5/8	11/16	1/2	671+80	C	3/4	3/4	5/8
666+20	C	1/2	1/2	11/16	672+00	C	11/16	5/16	3/4
666+40	C	9/16	3/4	3/8	672+20	C	9/16	1/4	1/2



Sta.	Type	Lt.	C.L.	Rt.	Sta.	Type	Lt.	C.L.	Rt.
672+40	C	7/16	3/8	7/16	678+20	C	3/8	1/2	1/2
672+60	C	7/16	5/16	5/8	678+40	C	1/2	1/2	1/2
672+80	Ex.	1/8	1/4	3/8	678+60	C	5/8	1/2	5/8
673+00	C	5/8	9/16	5/8	678+80	C	11/16	1/2	5/8
673+20	C	11/16	5/8	3/4	679+00	C	3/4	5/8	5/8
673+40	C	1/2	3/4	5/8	679+20	C	9/16	3/8	5/8
673+60	C	5/8	3/8	1/2	679+40	C	9/16	1/2	9/16
673+80	C	9/16	1/2	3/8	679+60	C	11/16	5/8	5/8
674+00	C	7/16	1/2	5/16	679+80	C	3/4	1/2	1/2
674+20	C	1/4	3/8	3/8	680+00	C	1/2	1/4	3/8
674+40	C	5/8	1/2	1/2	680+20	C	11/16	5/8	3/4
674+60	C	9/16	11/16	1/2	680+40	C	5/8	1/2	5/8
674+80	C	1/2	5/16	5/8	680+60	C	9/16	1/2	5/8
675+00	C	1/4	3/8	3/4	680+80	Ex.	3/4	1/2	9/16
675+20	C	3/16	1/2	1/2	681+00.6	Const. Jt.			
675+40	C	9/16	1/2	1/2	681+20	C	3/4	9/16	7/8
675+60	C	11/16	11/16	1/2	681+40	C	3/4	3/4	5/8
675+80	C	7/16	3/8	1/2	681+60	C	5/8	1/2	5/8
676+00	C	11/16	3/8	3/8	681+80	Ex.	3/8	1/2	3/8
676+20	C	9/16	3/8	1/2	682+00	C	1/2	9/16	5/8
676+39.6	Const. Jt.				682+20	C	1/2	9/16	5/8
676+60	C	3/4	3/4	3/4	682+40	C	3/4	7/8	3/4
676+80	Ex.	1/4	0	1/4	682+60	C	9/16	3/4	11/16
677+00	C	1/2	1/2	1/2	682+80	C	3/4	9/16	3/4
677+20	C	5/8	5/8	3/8	683+00	Ex.	1/4	3/4	3/8
677+40	C	11/16	1/4	3/8	683+20	C	11/16	9/16	3/4
677+60	C	9/16	5/16	1/2	683+40	C	9/16	9/16	3/4
677+80	C	1/2	1/4	1/2	683+60	C	3/4	13/16	5/8
678+00	C	1/2	3/4	5/8	683+80	C	3/4	3/4	3/4



Sta.	Type	Lt.	C.L.	Rt.	Sta.	Type	Lt.	C.L.	Rt.
684+00	C	15/16	1"	1"	689+80	C	3/4	11/16	3/4
684+20	Ex.	1/4	1/2	1/2	690+00	C	1/2	3/4	3/4
684+40	C	3/4	7/16	1"	690+20	Ex.	7/16	1/2	1/2
684+60	C	9/16	3/4	3/4	690+40	C	3/4	5/8	7/16
684+80	C	7/16	5/8	3/4	690+60	C	5/8	9/16	9/16
685+00	C	3/4	5/8	3/4	690+80	C	7/16	9/16	7/16
685+20	C	9/16	3/4	3/4	691+00	C	7/16	1/2	5/8
685+40	C	9/16	3/8	3/4	691+20	C	7/8	15/16	1"
685+60	C	7/8	1/2	3/4	691+40	Ex.	9/16	7/8	1/2
685+80	Ex.	1/4	1/2	11/16	691+60	C	7/8	3/4	1/2
686+00	C	7/8	5/8	1"	691+80	C	7/8	5/8	3/4
686+20	C	3/4	11/16	3/4	692+00	C	3/4	1/2	3/4
686+40	C	5/8	5/8	3/4	692+20	C	3/4	1/2	13/16
686+60	Ex.	7/16	9/16	3/8	692+40	C	7/8	3/4	3/4
686+80	C	5/8	3/8	1"	692+60	Ex.	5/8	3/4	1/2
687+00	C	5/8	1/2	3/4	692+80	C	7/8	9/16	3/4
687+20	C	3/4	3/4	1"	693+00	C	7/8	1/4	3/4
687+40	C	1"	11/16	11/16	693+29.5	Const. Jt.			
687+60	C	3/4	1/2	3/4	693+40	C	5/8	5/8	3/4
687+80	Ex.	7/16	11/16	1/2	693+60	C	3/4	3/4	13/16
688+00	C	3/4	3/8	11/16	693+80	Ex.	9/16	3/4	1/2
688+20	C	9/16	1/2	11/16	694+00	C	9/16	1/2	11/16
688+40	C	9/16	1/2	5/8	694+20	C	1/2	1/2	3/4
688+60	C	1/2	1/2	1/2	694+40	C	9/16	5/8	7/16
688+80	C	3/4	3/8	11/16	694+60	C	7/16	9/16	5/8
689+00	Ex.	7/16	3/4	1/2	694+80	C	7/16	9/16	7/16
689+20	C	3/4	7/16	5/8	695+00	Ex.	7/16	15/16	3/4
689+40	C	3/4	5/8	5/8	695+20	C	7/16	3/8	1/2
689+60	C	9/16	11/16	7/8	695+40	C	7/16	3/8	3/8



Sta.	Type	Lt.	C.L.	Rt.	Sta.	Type	Lt.	C.L.	Rt.
695+60	C	9/16	1/2	5/8	701+60	C	7/16	5/16	1/2
695+80	C	5/8	1/2	3/4	701+80	C	1/4	1/2	9/16
696+00	C	1/2	3/8	1/2	702+00	C	7/16	1/2	1/2
696+20	Ex.	9/16	9/16	9/16	702+20	Ex.	1/4	1/4	1/2
696+40	C	9/16	3/8	5/8	702+40	C	5/8	7/16	3/8
696+60	C	7/16	9/16	5/8	702+60	C	5/8	5/8	5/8
696+80	C	3/4	1/2	11/16	702+80	C	9/16	1/2	9/16
697+00	C	5/8	1/2	1/2	703+00	C	9/16	5/8	1/2
697+20	C	3/4	1/2	5/8	703+20	C	5/8	1/2	1/2
697+40	Ex.	3/4	3/8	5/8	703+40.0	Ex. 1-1/16	5/8	3/4	
697+60	C	5/8	1/2	3/4	Const. Jt.				
697+80	C	5/8	5/8	5/8	703+60	C	1"	5/8	15/16
698+00	C	5/8	1/2	5/8	703+80	C	7/8	1/2	3/4
698+20	C	15/16	1/2	5/8	704+00	C	1/2	1/4	3/8
698+40	C	7/8	9/16	13/16	704+20	C	3/4	3/8	1/2
698+60	Ex.	1/8	1/8	7/16	704+40	C	5/8	1/2	5/8
698+80	C	9/16	9/16	1/2	704+60	Ex.	9/16	5/8	1/2
699+00	C	1/2	7/16	9/16	704+80	C	5/8	9/16	3/4
699+20	C	3/4	7/16	7/16	705+00	C	15/16	3/8	5/8
699+40	C	7/16	1/2	7/16	705+20	C	1-1/8	1/2	1/2
699+60	C	3/4	3/8	3/8	705+40.0	Const. Jt.			
699+80	Ex.	3/8	7/16	5/8	705+60	C	3/4	1/2	7/16
700+00	C	3/4	3/8	3/8	705+80	Ex.	7/16	1/2	9/16
700+20	C	7/8	1/4	1/2	706+00	C	7/16	1/2	9/16
700+40	C	5/8	5/16	7/16	706+20	C	1/4	3/4	3/4
700+60	C	7/16	1/4	3/8	706+40	C	9/16	5/8	5/8
700+80	C	5/8	1/4	1/2	706+60	C	3/4	1/2	3/4
701+00	Ex.	1/8	5/16	3/8	706+80	C	7/8	1/4	7/8
701+20	C	9/16	3/8	3/8	707+00	Ex.	1/2	1/2	7/8
701+40	C	9/16	1/4	9/16	707+20	C	7/16	1/4	3/4



Sta.	Type	Lt.	C.L.	Rt.	Sta.	Type	Lt.	C.L.	Rt.
707+40	C	7/8	9/16	7/8	719+60	C	3/4	1/2	15/16
707+60	C	5/8	3/8	3/16	720+20	Ex.	1/8	3/16	1/8
707+80	C	9/16	1/2	5/8	720+80	C	3/8	1/8	1/2
708+00	C	1-1/8	1/2	1-3/8	721+40	Ex.	1/16	1/16	1/8
708+20	C	3/4	9/16	5/8	722+00	C	9/16	1/2	3/8
708+40	Ex.	1/2	1/4	15/16	722+60	Ex.	3/16	1/8	1/8
708+60	C	3/4	5/8	13/16	723+20	C	3/4	9/16	1/2
708+80	C	3/4	1/2	1/2	723+80	Ex.	3/8	3/8	1/4
709+00	C	5/8	3/8	5/8	724+40	C	9/16	3/8	1/2
709+20	C	3/4	1/2	3/4	725+00	Ex.	3/8	1/4	1/2
709+40	Ex.	1/8	5/16	1/2	725+20	C	1/2	9/16	1/4
709+60	C	3/4	7/16	3/4	725+40.0	Const. Jt.			
709+80	C	3/4	1/4	7/16	725+60	C	5/16	7/16	3/8
710+00	C	5/8	1/8	1/2	725+80	C	5/8	7/16	9/16
710+60	Ex.	9/16	1/2	1/2	726+00	C	9/16	9/16	5/8
711+20	C	3/4	1/8	3/4	726+20	Ex.	1/2	7/16	7/16
711+80	Ex.	3/4	9/16	3/8	726+40	C	9/16	9/16	5/8
712+40	C	9/16	9/16	1/4	726+60	C	9/16	3/4	3/4
713+00	Ex.	1/2	9/16	1-3/16	726+80	C	9/16	3/4	11/16
713+60	C	7/16	7/16	9/16	727+00	C	7/16	1/4	9/16
714+20	Ex.	3/4	11/16	9/16	727+20	C	1/2	9/16	5/16
714+80	C	9/16	3/4	3/4	727+40	Ex.	1/2	7/16	7/16
715+40	Ex.	5/8	9/16	7/8	727+60	C	1/2	7/16	1/2
716+00.0	Const. Jt.				727+80	C	1/2	9/16	7/16
716+60	Ex.	1/2	9/16	1-1/8	728+00	C	1/2	7/16	7/16
717+20	C	9/16	1/2	3/4	728+20	C	9/16	9/16	7/16
717+80	Ex.	3/4	1-3/8	1-1/8	728+40	C	3/8	5/8	13/16
718+40	C	1/2	5/16	1/2	728+60	Ex.	1/2	11/16	7/16
719+00	Ex.	1/8	1/8	1/4	728+80	C	3/4	13/16	1/2



Sta.	Type	Lt.	C.L.	Rt.	Sta.	Type	Lt.	C.L.	Rt.
729+00	C	3/8	1/2	11/16	734+60	Ex.	3/4	1/2	3/16
729+20	C	1/2	3/4	5/8	734+80	C	1/4	3/8	1/2
729+40	C	3/4	11/16	3/4	735+00	C	11/16	3/4	1/2
729+60	C	5/8	1/2	5/8	735+20	C	3/4	1/2	7/16
729+80	Ex.	1/4	1/4	3/8	735+40	C	5/8	5/16	5/16
730+00	C	3/4	1/2	5/8	735+60	C	9/16	3/8	5/16
730+20	C	1/2	1/4	1/2	735+80	Ex.	1/4	5/16	3/16
730+40	C	5/8	1/4	1/2	736+00	C	11/16	5/8	5/8
730+60	C	11/16	1/2	7/16	736+20	C	9/16	3/8	7/16
730+80	C	9/16	1/2	9/16	736+40	C	1/2	7/8	1/2
731+00	Ex.	3/16	1/2	7/16	736+60	C	3/4	5/8	5/8
731+09.5	Const. Jt.				736+80	C	1/4	3/4	5/8
731+20	C	3/8	5/16	7/16					
731+40	C	5/16	3/8	11/16					
731+60	C	9/16	9/16	3/8					
731+80	C	5/8	1/2	1-1/8					
732+00	C	3/4	7/16	1/2					
732+20	Ex.	3/16	7/16	5/8					
732+40	C	11/16	1/2	7/16					
732+60	C	9/16	3/8	1/2					
732+80	C	3/4	3/4	13/16					
733+00	C	9/16	3/8	15/16					
733+20	C	9/16	5/16	9/16					
733+40	Ex.	5/16	3/8	1/2					
733+60	C	9/16	1/4	15/16					
733+80	C	5/8	1/4	3/4					
734+00	C	7/16	7/16	3/4					
734+20	C	3/4	13/16	3/4					
734+40	C	3/4	9/16	1/4					



Section No. 1

Sept. 11, 1940

Standard B.M. No. 1 - Elevation 308.540 - 35 ft. left of sta. 513+50

182A 402.625	23A 402.625	30A 402.645
182B 514+457	23B 402.630	30B 402.650
183 402.625	234 402.630	304 402.650
183 402.630	23B 402.625	30B 402.635
184 402.630	23A 402.650	30A 402.635
192 402.620	30A 402.630	40A 402.635
20A 402.630	30B 402.635	40B 402.635
202 402.635	30B 402.635	40B 402.635
21A 402.635	31A 402.640	41A 402.640
21B 402.635	31B 402.640	41B 402.640
22A 402.620	32A 402.635	42A 402.620
22B 402.620	32B 402.640	42B 402.610
23A 402.630	33A 402.640	43A 402.615

### XIII. SECTION LEVEL MEASUREMENTS

24A 402.630	34A 402.640	44A 402.610
24B 402.630	34B 402.640	44B 402.600
24C 402.630	34A 402.640	44A 402.610
25A 402.630	35B 402.640	45B 402.610
25B 402.625	35C 402.630	45A 402.640
26A 402.650	36A 402.650	46B 402.640
26B 402.650	36B 402.650	46A 402.650
27A 402.630	37A 402.640	47B 402.650
27B 402.630	37B 402.640	47C 402.650
		48A 402.610
		48B 402.610
		48C 402.610



Section No. 1

Sept. 11, 1940

Standard B.M. No. 1 - Elevation 398.840 - 38 ft. left of sta. 517+50

(18A 402.625  
Sta. 514+45)

18B 402.625

18C 402.630

19A 402.620

19B 402.620

20A 402.630

20B 402.635

21A 402.635

21B 402.635

22A 402.620

22B 402.620

23A 402.630

23B 402.630

24A 402.630

24B 402.630

24C 402.630

25A 402.630

25B 402.625

26A 402.650

26B 402.650

27A 402.630

27B 402.630

28A 402.635

28B 402.630

29A 402.630

29B 402.625

30A 402.650

30B 402.650

30C 402.655

31A 402.660

31B 402.660

32A 402.635

32B 402.640

33A 402.645

33B 402.650

34A 402.640

34B 402.640

35A 402.640

35B 402.640

35C 402.650

36A 402.650

36B 402.650

37A 402.640

37B 402.640

38A 402.645

38B 402.640

39A 402.630

39B 402.635

40A 402.630

40B 402.625

41A 402.625

41B 402.625

41C 402.610

42A 402.610

42B 402.610

43A 402.615

43B 402.620

44A 402.610

44B 402.600

45A 402.610

45B 402.610

46A 402.640

46B 402.640

47A 402.660

47B 402.660

47C 402.680

48A 402.710

(48B 402.710  
Sta. 520+44)



Section No. 2

Sept. 11, 1940

Standard B.M. No. 2 - Elevation 407.470 - 38 ft. right of sta. 506+40

(1A 414.270 Sta. 502+00)	13A 410.565	25A 407.020	37B 403.600
1B 414.260	13B 410.555	25B 407.015	38A 403.380
1C 414.110	14A 410.265	26A 406.720	38B 403.380
2A 413.960	14B 410.255	26B 406.715	39A 403.230
2B 413.950	15A 409.970	27A 406.420	39B 403.230
3A 413.625	15B 409.965	27B 406.415	40A 403.080
3B 413.620	16A 409.685	28A 406.125	40B 403.075
4A 413.300	16B 409.680	28B 406.120	40C 403.010
4B 413.295	17A 409.380	29A 405.815	41A 402.960
5A 413.000	17B 409.375	29B 405.810	(41B 402.960 Sta. 510+00)
5B 412.990	17C 409.240	30A 405.530	
6A 412.690	18A 409.080	30B 405.520	
6B 412.680	18B 409.080	31A 405.215	
7A 412.365	19A 408.800	31B 405.210	
7B 412.360	19B 408.795	32A 404.900	
8A 412.050	20A 408.500	32B 404.895	
8B 412.050	20B 408.495	32C 404.750	
9A 411.745	21A 408.200	33A 404.620	
9B 411.740	21B 408.190	33B 404.620	
9C 411.585	22A 407.900	34A 404.330	
10A 411.445	22B 407.900	34B 404.330	
10B 411.440	23A 407.605	35A 404.070	
11A 411.145	23B 407.600	35B 404.070	
11B 411.135	24A 407.320	36A 403.820	
12A 410.840	24B 407.325	36B 403.820	
12B 410.835	24C 407.165	37A 403.600	



Section No. 3

Sept. 11, 1940

Standard B.M. No. 3 - Elevation 423.615 - 38 ft. left of sta. 466+40

(1A 423.315 Sta. 462+00)	14A 423.835	26B 424.335	39B 424.865
1B 423.320	14B 423.835	27A 424.365	40A 424.895
1C 423.335	15A 423.885	27B 424.365	40B 424.900
2A 423.365	15B 423.885	28A 424.405	40C 424.925
2B 423.365	16A 423.935	28B 424.405	41A 424.945
3A 423.415	16B 423.935	29A 424.450	(41B 424.950 Sta. 470+00)
3B 423.415	17A 423.985	29B 424.445	
4A 423.450	17B 423.985	30A 424.495	
4B 423.455	17C 424.010	30B 424.500	
5A 423.500	18A 424.025	31A 424.525	
5B 423.505	18B 424.025	31B 424.535	
6A 423.520	19A 424.055	32A 424.570	
6B 423.525	19B 424.065	32B 424.575	
7A 423.560	20A 424.105	32C 424.595	
7B 423.565	20B 424.105	33A 424.615	
8A 423.590	21A 424.145	33B 424.615	
8B 423.595	21B 424.155	34A 424.655	
9A 423.630	22A 424.190	34B 424.660	
9B 423.625 9C 423.645	22B 424.195	35A 424.715	
10A 423.665	23A 424.225	35B 424.710	
10B 423.670	23B 424.230	36A 424.740	
11A 423.705	24A 424.260	36B 424.740	
11B 423.715	24B 424.265	37A 424.785	
12A 423.755	24C 424.285	37B 424.790	
12B 423.755	25A 424.295	38A 424.830	
13A 423.795	25B 424.295	38B 424.835	
13B 423.800	26A 424.340	39A 424.865	



Section No. 4

Sept. 10, 1940

Standard B.M. No. 4 - Elevation 417.900 - 38 ft. right of sta. 452+25.

(1A 420.410 Sta. 448+02)	13A 420.890	22B 421.280
1B 420.415	13B 420.890	23A 421.310
2A 420.445	13C 420.925	23B 421.310
2B 420.450	14A 420.940	24A 421.360
3A 420.490	14B 420.940	24B 421.365
3B 420.490	14C 420.965	25A 421.400
4A 420.540	15A 420.980	25B 421.400
4B 420.540	15B 420.980	26A 421.440
5A 420.570	15C 421.000	26B 421.445
5B 420.570	16A 421.040	27A 421.470
6A 420.610	16B 421.045	27B 421.475
6B 420.615	16C 421.065	28A 421.530
7A 420.640	17A 421.095	28B 421.530
7B 420.630	17B 421.100	29A 421.580
8A 420.675	17C 421.120	29B 421.580
8B 420.680	18A 421.120	30A 421.620
9A 420.720	18B 421.120	30B 421.620
9B 420.725	18C 421.140	31A 421.670
10A 420.770	19A 421.160	(31B 421.665 Sta. 454+02)
10B 420.770	19B 421.160	
11A 420.810	20A 421.195	
11B 420.800	20B 421.195	
12A 420.840	21A 421.225	
12B 420.845	21B 421.240	
	22A 421.280	

420.640  
420.675  
1015  
420.680  
420.690  
810  
1025



Section No. 5

Sept. 10, 1940

Standard B.M. No. 5 - Elevation 424.540 - 38 ft. right of sta. 436+40

(1A 426.370 Sta. 433+61)	13A 426.125	22A 424.015
1B 426.375	13B 426.120	22B 424.010
2A 426.470	13C 426.070	23A 423.705
2B 426.475	14A 425.980	23B 423.685
3A 426.540	14B 425.975	24A 423.395
3B 426.545	14C 425.880	24B 423.390
4A 426.570	15A 425.790	25A 423.100
4B 426.575	15B 425.795	25B 423.095
5A 426.590	15C 425.695	26A 422.775
5B 426.595	16A 425.575	26B 422.775
6A 426.600	16B 425.565	27A 422.515
6B 426.605	16C 425.475	27B 422.510
7A 426.600	17A 425.370	28A 422.220
7B 426.600	17B 425.360	28B 422.215
8A 426.575	17C 425.275	29A 421.925
8B 426.570	18A 425.145	29B 421.915
9A 426.500	18B 425.145	30A 421.635
9B 426.500	18C 425.020	30B 421.625
10A 426.440	19A 424.880	31A 421.335
10B 426.440	19B 424.875	(31B 421.320 Sta. 439+61)
11A 426.350	20A 424.605	
11B 426.350	20B 424.595	
12A 426.250	21A 424.315	
12B 426.250	21B 424.305	



Section No. 6

Sept. 10, 1940

Standard B.M. No. 6 - Elevation 444.330 - 38 ft. left of sta. 413+00.

(1A	439.350	9C	441.225
Sta. 410+81)			
1B	439.350	10A	441.010
1C	439.500	10B	441.010
2A	439.650	10C	440.740
2B	439.655	11A	440.400
2C	439.810	(11B	440.390
3A	439.970	Sta. 416+81)	
3B	439.970		
3C	440.130		
4A	440.300		
4B	440.300		
4C	440.460		
5A	440.600		
5B	440.605		
5C	440.770		
6A	440.890		
6B	440.890		
6C	441.050		
7A	441.195		
7B	441.200		
7C	441.320		
8A	441.420		
8B	441.420		
8C	441.420		
9A	441.360		
9B	441.360		



Section No. 7

Sept. 10, 1940

Standard B.M. No. 7 - Elevation 435.290 - 38 ft. right of sta. 406+40

(1A 439.545 Sta. 403+61)	12A 438.275	20A 438.010
1B 439.535	12B 438.270	20B 438.010
2A 439.375	13A 438.210	21A 438.020
2B 439.375	13B 438.205	21B 438.025
3A 439.215	13C 438.185	22A 438.040
3B 439.215	14A 438.145	22B 438.040
4A 439.065	14B 438.145	23A 438.080
4B 439.055	14C 438.135	23B 438.080
5A 438.925	15A 438.105	24A 438.120
5B 438.920	15B 438.105	24B 438.120
6A 438.805	15C 438.105	25A 438.160
6B 438.805	16A 438.050	25B 438.165
7A 438.695	16B 438.050	26A 438.230
7B 438.690	16C 438.010	26B 438.235
8A 438.610	17A 438.035	27A 438.310
8B 438.605	17B 438.030	27B 438.315
9A 438.515	17C 438.015	28A 438.415
9B 438.515	18A 438.015	28B 438.415
10A 438.415	18B 438.015	29A 438.505
10B 438.415	18C 438.015	29B 438.500
11A 438.315	19A 437.990	30A 438.615
11B 438.310	19B 437.990	30B 438.615
		31A 438.710
		(31B 438.710 Sta. 409+61)



## Section Standard

Sept. 11, 1940

Standard B.M. No. 8 - Elevation 405.000 - 38 ft. left of sta. 574+00.

(1A 407.605 Sta. 567+61)	13A 405.445	25B 403.250	38A 400.870
1B 407.605	13B 405.445	26A 403.060	38B 400.865
1C 407.505	14A 405.265	26B 403.055	39A 400.700
2A 407.415	14B 405.260	27A 402.875	39B 400.700
2B 407.415	15A 405.080	27B 402.875	40A 400.540
3A 407.235	15B 405.075	28A 402.680	40B 400.540
3B 407.235	16A 404.875	28B 402.680	40C 400.485
4A 407.055	16B 404.875	29A 402.520	41A 400.430
4B 407.055	17A 404.705	29B 402.510	(41B 400.430 Sta. 579+62)
5A 406.855	17B 404.700	30A 402.320	
5B 406.850	17C 404.615	30B 402.320	
6A 406.680	18A 404.520	31A 402.145	
6B 406.675	18B 404.515	31B 402.145	
7A 406.500	19A 404.355	32A 401.960	
7B 406.495	19B 404.350	32B 401.955	
8A 406.330	20A 404.170	32C 401.860	
8B 406.335	20B 404.170	33A 401.775	
9A 406.150	21A 403.980	33B 401.770	
9B 406.155	21B 403.985	34A 401.595	
9C 406.055	22A 403.780	34B 401.590	
10A 405.975	22B 403.785	35A 401.400	
10B 405.975	23A 403.595	35B 401.395	
11A 405.820	23B 403.595	36A 401.230	
11B 405.820	24A 403.440	36B 401.230	
12A 405.625	24B 403.435	37A 401.080	
12B 405.625	24C 403.340	37B 401.070	
	25A 403.250		



# PRELIMINARY DATA

The changes in widths of the joints which were caused by the daily temperature cycle of November 28, 1940, are as follows:

## Section No. 1

Time 7:00 a.m. 2:00 p.m.  
T. Concrete F. 34 35  
T. Air F. 35 35

St. No.	Type	Width	Width	Width
1	C	1.000	1.000	1.000
2	C	1.000	1.000	1.000
3	C	1.000	1.000	1.000
4	C	1.000	1.000	1.000
5	C	1.000	1.000	1.000
6	C	1.000	1.000	1.000
7	C	1.000	1.000	1.000
8	C	1.000	1.000	1.000
9	C	1.000	1.000	1.000
10	C	1.000	1.000	1.000

## Section No. 2

Time 7:00 a.m. 2:00 p.m.  
T. Concrete F. 34 35  
T. Air F. 35 35

St. No.	Type	Width	Width	Width
1	C	1.000	1.000	1.000
2	C	1.000	1.000	1.000
3	C	1.000	1.000	1.000
4	C	1.000	1.000	1.000
5	C	1.000	1.000	1.000
6	C	1.000	1.000	1.000
7	C	1.000	1.000	1.000
8	C	1.000	1.000	1.000
9	C	1.000	1.000	1.000
10	C	1.000	1.000	1.000

## XIV. DAILY CHANGES IN JOINT WIDTH MEASUREMENTS NOV. 28, 1940



# PRELIMINARY DATA

The changes in widths of the joints which were caused by the daily temperature cycle of November 28, 1940, are as follows:

## Section No. 1

Time	7:50 a.m.	2:50 p.m.
T. Concrete F.	34	45
T. Air F.	30	40

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
1	C	5.072	5.048	-.024
5	C	5.044	5.025	-.019
10	C	5.028	5.012	-.016
29	C	4.964	4.948	-.016
33	C	5.000	4.983	-.017
56	C	4.910	4.896	-.014
61	C	5.132	5.118	-.014
65	C	5.107	5.091	-.016

## Section No. 2

Time	7:40 a.m.	2:40 p.m.
T. Concrete F.	34	45
T. Air F.	30	40

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
1	Exp.	5.084	5.066	-.018
2	C	5.104	5.089	-.015
6	C	5.154	5.143	-.011
11	C	5.074	5.058	-.016
20	C	5.048	5.035	-.013
22	C	5.129	5.110	-.019
31	C	5.100	5.086	-.014
36	C	5.153	5.130	-.023
40	C	5.147	5.125	-.022
41	Exp.	6.000	5.989	-.011

Note: Measurements of the daily change in widths of the joints in Section 4 is not available.



Section No. 3

Time  
T. Concrete F. 7:30 a.m.; 2:30 p.m.  
T. Air F. 34 45  
30 40

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
1	Exp.	6.171	6.161	-.010
2	C	5.189	5.168	-.021
6	C	5.116	5.100	-.016
11	C	5.139	5.122	-.017
16	C	5.228	5.208	-.020
20	C	5.132	5.113	-.019
21	Exp.	5.016	5.004	-.012

Section No. 5

Time  
T. Concrete F. 7:20 a.m.; 2:20 p.m.  
T. Air F. 34 46  
30 42

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
7	Exp.	6.184	6.157	-.027
8	C	5.113	5.098	-.015
9	C	5.044	5.026	-.018
10	C	5.091	5.070	-.021
11	C	5.064	5.050	-.014
12	C	5.045	5.032	-.013
13	Exp.	5.170	5.140	-.030

Note: Measurement of the daily change in widths  
of the joints in Section 4 is not scheduled.



Section No. 6

Time 7:10 a.m. 2:10 p.m.  
T. Concrete F. 33 45  
T. Air F. 29 41

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
3	Exp.	5.268	5.223	-.045
4	C	5.584	5.536	-.048
5	Exp.	5.475	5.430	-.045
6	C	5.195	5.151	-.044
7	Exp.	5.223	5.170	-.053

Section No. 7

Time 7:00 a.m. 2:00 p.m.  
T. Concrete F. 33 45  
T. Air F. 28 39

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
7	Exp.	6.028	6.020	-.008
8	C	5.069	5.051	-.018
9	C	5.346	5.325	-.021
10	C	5.199	5.179	-.020
11	C	4.922	4.903	-.019
12	C	5.123	5.113	-.010
13	Exp.	5.942	5.927	-.015



# SUMMARY OF THE DAILY CHANGES IN WIDTHS OF THE JOINTS NOV. 22, 1940.

Section No. 1. Design - contraction joints only, spaced 30 feet apart. For an increase in pavement temperature of 11 F., the average decrease in width of the joints was .017 inches.

## Section Standard

Section No. 2. Design - expansion joints spaced 120 feet apart and intermediate contraction joints spaced 30 feet apart. For an increase in pavement temperature of 11 F., the average decrease in width of the expansion joints was .017 inches, and the average decrease in width of the contraction joints was .017 inches.

Time 8:05 a.m. 3:10 p.m.  
T. Concrete F. 37 46  
T. Air F. 34 40

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
17	Exp.	5.545	5.525	-.020
18	C	5.196	5.177	-.019
19	C	5.119	5.102	-.017
20	C	5.217	5.196	-.021
21	Exp.	5.527	5.507	-.020
22	C	5.110	5.091	-.019
23	C	5.164	5.134	-.030
24	C	5.020	5.013	-.007
25	Exp.	5.169	5.139	-.030

Average decrease in width of the contraction joints was .016 inches.

Section No. 7. Design - expansion joints spaced 120 feet apart and intermediate contraction joints spaced 30 feet apart. For an increase in pavement temperature of 12 F., the average decrease in width of the expansion joints was .018 inches, and the average decrease in width of the contraction joints was .015 inches.

Section Standard Design - expansion joints spaced 120 feet apart and intermediate contraction joints spaced 30 feet apart. For an increase in pavement temperature of 9 F., the average decrease in width of the expansion joints was .023 inches, and the average decrease in width of the contraction joints was .019 inches.



SUMMARY OF THE DAILY CHANGES IN WIDTHS OF THE JOINTS NOV. 28, 1940.

- Section No. 1. Design - contraction joints only, spaced 20 feet apart. For an increase in pavement temperature of 11 F., the average decrease in width of the joints was .017 inches.
- Section No. 2. Design - expansion joints spaced 800 feet apart and intermediate contraction joints spaced 20 feet apart. For an increase in pavement temperature of 11 F., the average decrease in width of the expansion joints was .015 inches, and the average decrease in width of the contraction joints was .017 inches.
- Section No. 3. Design - expansion joints spaced 400 feet apart and intermediate contraction joints spaced 20 feet apart. For an increase in pavement temperature of 11 F., the average decrease in width of the expansion joints was .011 inches, and the average decrease in width of the contraction joints was .019 inches.
- Section No. 5. Design - expansion joints spaced 120 feet apart and intermediate contraction joints spaced 20 feet apart. For an increase in pavement temperature of 12 F., the average decrease in width of the expansion joints was .029 inches, and the average decrease in width of the contraction joints was .016 inches.
- Section No. 6. Design - alternate expansion and contraction joints spaced 60 feet apart. For an increase in pavement temperature of 12 F., the average decrease in width of the expansion joints was .048 inches, and the average decrease in width of the contraction joints was .046 inches.
- Section No. 7. Design - expansion joints spaced 120 feet apart and intermediate contraction joints spaced 20 feet apart. For an increase in pavement temperature of 12 F., the average decrease in width of the expansion joints was .012 inches, and the average decrease in width of the contraction joints was .018 inches.
- Section Standard Design - expansion joints spaced 120 feet apart and intermediate contraction joints spaced 30 feet apart. For an increase in pavement temperature of 9 F., the average decrease in width of the expansion joints was .023 inches, and the average decrease in width of the contraction joints was .019 inches.



The changes in widths of the joints which were caused by the daily temperature cycle of February 25, 1941, are as follows:

Section No. 1

Time	7:55 A.M.	2:45 P.M.		
T. Concrete F.	38	42		
T. Air F.	37	47		
Jt. No.	Type	Temp	Width	Width Change
1	0	38.0	1.000	0.000
2	0	38.0	1.000	0.000
3	0	38.0	1.000	0.000
4	0	38.0	1.000	0.000
5	0	38.0	1.000	0.000
6	0	38.0	1.000	0.000
7	0	38.0	1.000	0.000
8	0	38.0	1.000	0.000
9	0	38.0	1.000	0.000
10	0	38.0	1.000	0.000
11	0	38.0	1.000	0.000
12	0	38.0	1.000	0.000
13	0	38.0	1.000	0.000
14	0	38.0	1.000	0.000
15	0	38.0	1.000	0.000
16	0	38.0	1.000	0.000
17	0	38.0	1.000	0.000
18	0	38.0	1.000	0.000
19	0	38.0	1.000	0.000
20	0	38.0	1.000	0.000
21	0	38.0	1.000	0.000
22	0	38.0	1.000	0.000
23	0	38.0	1.000	0.000
24	0	38.0	1.000	0.000
25	0	38.0	1.000	0.000
26	0	38.0	1.000	0.000
27	0	38.0	1.000	0.000
28	0	38.0	1.000	0.000
29	0	38.0	1.000	0.000
30	0	38.0	1.000	0.000
31	0	38.0	1.000	0.000
32	0	38.0	1.000	0.000
33	0	38.0	1.000	0.000
34	0	38.0	1.000	0.000
35	0	38.0	1.000	0.000
36	0	38.0	1.000	0.000
37	0	38.0	1.000	0.000
38	0	38.0	1.000	0.000
39	0	38.0	1.000	0.000
40	0	38.0	1.000	0.000
41	0	38.0	1.000	0.000
42	0	38.0	1.000	0.000
43	0	38.0	1.000	0.000
44	0	38.0	1.000	0.000
45	0	38.0	1.000	0.000
46	0	38.0	1.000	0.000
47	0	38.0	1.000	0.000
48	0	38.0	1.000	0.000
49	0	38.0	1.000	0.000
50	0	38.0	1.000	0.000
51	0	38.0	1.000	0.000
52	0	38.0	1.000	0.000
53	0	38.0	1.000	0.000
54	0	38.0	1.000	0.000
55	0	38.0	1.000	0.000
56	0	38.0	1.000	0.000
57	0	38.0	1.000	0.000
58	0	38.0	1.000	0.000
59	0	38.0	1.000	0.000
60	0	38.0	1.000	0.000
61	0	38.0	1.000	0.000
62	0	38.0	1.000	0.000
63	0	38.0	1.000	0.000
64	0	38.0	1.000	0.000
65	0	38.0	1.000	0.000
66	0	38.0	1.000	0.000
67	0	38.0	1.000	0.000
68	0	38.0	1.000	0.000
69	0	38.0	1.000	0.000
70	0	38.0	1.000	0.000
71	0	38.0	1.000	0.000
72	0	38.0	1.000	0.000
73	0	38.0	1.000	0.000
74	0	38.0	1.000	0.000
75	0	38.0	1.000	0.000
76	0	38.0	1.000	0.000
77	0	38.0	1.000	0.000
78	0	38.0	1.000	0.000
79	0	38.0	1.000	0.000
80	0	38.0	1.000	0.000
81	0	38.0	1.000	0.000
82	0	38.0	1.000	0.000
83	0	38.0	1.000	0.000
84	0	38.0	1.000	0.000
85	0	38.0	1.000	0.000
86	0	38.0	1.000	0.000
87	0	38.0	1.000	0.000
88	0	38.0	1.000	0.000
89	0	38.0	1.000	0.000
90	0	38.0	1.000	0.000
91	0	38.0	1.000	0.000
92	0	38.0	1.000	0.000
93	0	38.0	1.000	0.000
94	0	38.0	1.000	0.000
95	0	38.0	1.000	0.000
96	0	38.0	1.000	0.000
97	0	38.0	1.000	0.000
98	0	38.0	1.000	0.000
99	0	38.0	1.000	0.000
100	0	38.0	1.000	0.000

XV. DAILY CHANGES IN JOINT WIDTH MEASUREMENTS FEB. 25, 1941

Section No. 1

Time	7:55 A.M.	2:45 P.M.
T. Concrete F.	38	52
T. Air F.	35	47

Jt. No.	Type	Temp	Width	Width Change
1	0	38.0	1.000	0.000
2	0	38.0	1.000	0.000
3	0	38.0	1.000	0.000
4	0	38.0	1.000	0.000
5	0	38.0	1.000	0.000
6	0	38.0	1.000	0.000
7	0	38.0	1.000	0.000
8	0	38.0	1.000	0.000
9	0	38.0	1.000	0.000
10	0	38.0	1.000	0.000
11	0	38.0	1.000	0.000
12	0	38.0	1.000	0.000
13	0	38.0	1.000	0.000
14	0	38.0	1.000	0.000
15	0	38.0	1.000	0.000
16	0	38.0	1.000	0.000
17	0	38.0	1.000	0.000
18	0	38.0	1.000	0.000
19	0	38.0	1.000	0.000
20	0	38.0	1.000	0.000
21	0	38.0	1.000	0.000
22	0	38.0	1.000	0.000
23	0	38.0	1.000	0.000
24	0	38.0	1.000	0.000
25	0	38.0	1.000	0.000
26	0	38.0	1.000	0.000
27	0	38.0	1.000	0.000
28	0	38.0	1.000	0.000
29	0	38.0	1.000	0.000
30	0	38.0	1.000	0.000
31	0	38.0	1.000	0.000
32	0	38.0	1.000	0.000
33	0	38.0	1.000	0.000
34	0	38.0	1.000	0.000
35	0	38.0	1.000	0.000
36	0	38.0	1.000	0.000
37	0	38.0	1.000	0.000
38	0	38.0	1.000	0.000
39	0	38.0	1.000	0.000
40	0	38.0	1.000	0.000
41	0	38.0	1.000	0.000
42	0	38.0	1.000	0.000
43	0	38.0	1.000	0.000
44	0	38.0	1.000	0.000
45	0	38.0	1.000	0.000
46	0	38.0	1.000	0.000
47	0	38.0	1.000	0.000
48	0	38.0	1.000	0.000
49	0	38.0	1.000	0.000
50	0	38.0	1.000	0.000
51	0	38.0	1.000	0.000
52	0	38.0	1.000	0.000
53	0	38.0	1.000	0.000
54	0	38.0	1.000	0.000
55	0	38.0	1.000	0.000
56	0	38.0	1.000	0.000
57	0	38.0	1.000	0.000
58	0	38.0	1.000	0.000
59	0	38.0	1.000	0.000
60	0	38.0	1.000	0.000
61	0	38.0	1.000	0.000
62	0	38.0	1.000	0.000
63	0	38.0	1.000	0.000
64	0	38.0	1.000	0.000
65	0	38.0	1.000	0.000
66	0	38.0	1.000	0.000
67	0	38.0	1.000	0.000
68	0	38.0	1.000	0.000
69	0	38.0	1.000	0.000
70	0	38.0	1.000	0.000
71	0	38.0	1.000	0.000
72	0	38.0	1.000	0.000
73	0	38.0	1.000	0.000
74	0	38.0	1.000	0.000
75	0	38.0	1.000	0.000
76	0	38.0	1.000	0.000
77	0	38.0	1.000	0.000
78	0	38.0	1.000	0.000
79	0	38.0	1.000	0.000
80	0	38.0	1.000	0.000
81	0	38.0	1.000	0.000
82	0	38.0	1.000	0.000
83	0	38.0	1.000	0.000
84	0	38.0	1.000	0.000
85	0	38.0	1.000	0.000
86	0	38.0	1.000	0.000
87	0	38.0	1.000	0.000
88	0	38.0	1.000	0.000
89	0	38.0	1.000	0.000
90	0	38.0	1.000	0.000
91	0	38.0	1.000	0.000
92	0	38.0	1.000	0.000
93	0	38.0	1.000	0.000
94	0	38.0	1.000	0.000
95	0	38.0	1.000	0.000
96	0	38.0	1.000	0.000
97	0	38.0	1.000	0.000
98	0	38.0	1.000	0.000
99	0	38.0	1.000	0.000
100	0	38.0	1.000	0.000



The changes in widths of the joints which were caused by the daily temperature cycle of February 25, 1941, are as follows:

### Section No. 1

Time	7:55 a.m.	2:50 p.m.
T. Concrete F.	38	52
T. Air F.	37	47

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
1	C	5.060	5.035	-.025
5	C	5.029	5.008	-.021
10	C	5.009	4.987	-.022
29	C	4.957	4.940	-.017
33	C	4.988	4.967	-.021
56	C	4.899	4.884	-.015
61	C	5.117	5.098	-.019
65	C	5.087	5.068	-.019

### Section No. 2

Time	7:40 a.m.	2:40 p.m.
T. Concrete F.	38	52
T. Air F.	36	47

Jt. No.	Type	Gage Inches	Gage inches	Jt. Width Change inches
1	Exp.	5.064	5.048	-.016
2	C	5.108	5.088	-.020
6	C	5.135	5.113	-.022
11	C	5.059	5.038	-.021
20	C	5.045	5.026	-.019
22	C	5.114	5.090	-.024
31	C	5.088	5.066	-.022
36	C	5.132	5.101	-.031
40	C	5.145	5.115	-.030
41	Exp.	5.970	5.958	-.012



### Section No. 3

Time	7:30 a.m.	2:30 p.m.
T. Concrete F.	38	50
T. Air F.	36	46

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
1	Exp.	6.137	6.126	-.011
2	C	5.192	5.168	-.024
6	C	5.103	5.085	-.018
11	C	5.131	5.110	-.021
16	C	5.204	5.181	-.023
20	C	5.138	5.108	-.030
21	Exp.	4.992	4.978	-.014

### Section No. 5

Time	7:20 a.m.	2:20 p.m.
T. Concrete F.	38	51
T. Air F.	36	46

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
7	Exp.	6.134	6.110	-.024
8	C	5.099	5.084	-.015
9	C	5.028	5.002	-.026
10	C	5.072	5.046	-.026
11	C	5.065	5.046	-.019
12	C	5.044	5.030	-.014
13	Exp.	5.147	5.119	-.028

Note: Measurement of the daily change in widths of the joints in Section No. 4 is not scheduled.



# Section No. 6

Time	7:10 a.m.	2:10 p.m.
T. Concrete F.	38	51
T. Air F.	35	46

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
3	Exp.	5.248	5.190	-.058
4	C	5.574	5.520	-.054
5	Exp.	5.432	5.376	-.056
6	C	5.190	5.137	-.053
7	Exp.	5.188	5.128	-.060

# Section No. 7

Time	7:00 a.m.	2:00 p.m.
T. Concrete F.	38	51
T. Air F.	35	46

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
7	Exp.	5.976	5.955	-.021
8	C	5.083	5.052	-.031
9	C	5.344	5.320	-.024
10	C	5.188	5.168	-.020
11	C	4.922	4.900	-.022
12	C	5.133	5.105	-.028
13	Exp.	5.890	5.870	-.020



# Section Standard

Time 8:15 a.m. 3:05 p.m.  
T. Concrete F. 40 51  
T. Air F. 38 47

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
17	Exp.	5.516	5.491	-.025
18	C	5.181	5.157	-.024
19	C	5.104	5.081	-.023
20	C	5.215	5.189	-.026
21	Exp.	5.502	5.478	-.024
22	C	5.092	5.069	-.023
23	C	5.143	5.115	-.028
24	C	5.018	5.000	-.018
25	Exp.	5.155	5.124	-.031



SUMMARY OF THE DAILY CHANGES IN WIDTHS OF THE JOINTS FEB. 25, 1941.

- Section No. 1. Design - contraction joints only, spaced 20 feet apart. For an increase in pavement temperature of 14 F., the average decrease in width of the joints was .020 inches.
- Section No. 2. Design - expansion joints spaced 800 feet apart and intermediate contraction joints spaced 20 feet apart. For an increase in pavement temperature of 14 F., the average decrease in width of the expansion joints was .014 inches, and the average decrease in width of the contraction joints was .024 inches.
- Section No. 3. Design - expansion joints spaced 400 feet apart and intermediate contraction joints spaced 20 feet apart. For an increase in pavement temperature of 12 F., the average decrease in width of the expansion joints was .013 inches, and the average decrease in width of the contraction joints was .023 inches.
- Section No. 5. Design - expansion joints spaced 120 feet apart and intermediate contraction joints spaced 20 feet apart. For an increase in pavement temperature of 13 F., the average decrease in width of the expansion joints was .026 inches, and the average decrease in width of the contraction joints was .020 inches.
- Section No. 6. Design - alternate expansion and contraction joints spaced 60 feet apart. For an increase in pavement temperature of 13 F., the average decrease in width of the expansion joints was .058 inches, and the average decrease in width of the contraction joints was .054 inches.
- Section No. 7. Design - expansion joints spaced 120 feet apart and intermediate contraction joints spaced 20 feet apart. For an increase in pavement temperature of 13 F., the average decrease in width of the expansion joints was .021 inches, and the average decrease in width of the contraction joints was .025 inches.
- Section Standard Design - expansion joints spaced 120 feet apart and intermediate contraction joints spaced 30 feet apart. For an increase in pavement temperature of 11 F., the average decrease in width of the expansion joints was .027 inches, and the average decrease in width of the contraction joints was .024 inches.



PRELIMINARY DATA

The seasonal changes in width of the joints between November 27, 1940 and February 24, 1941 are as follows:

Section No. 1

Date	11-27-40	2-24-41
Time	3:00 p.m.	2:15 p.m.
T. Concrete T.	40	43
T. Air T.	34	33

No.	Type	Base	Top	St. Width (inches)
-----	------	------	-----	--------------------

XVI. SEASONAL CHANGES IN JOINT WIDTH MEASUREMENTS  
NOV. 27, 1940 and FEB. 24, 1941



# PRELIMINARY DATA

The seasonal changes in width of the joints between November 27, 1940 and February 24, 1941 are as follows:

## Section No. 1

Date	11-27-40	2-24-41
Time	3:00 p.m.	3:00 p.m.
T. Concrete F.	40	43
T. Air F.	34	42

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
1	C	5.060	5.049	-.011
3	C	5.212	5.200	-.012
5	C	5.032	5.019	-.013
7	C	5.132	5.128	-.004
9	C	5.046	5.039	-.007
13	C	5.052	5.040	-.012
17	C	5.076	5.056	-.020
21	C	5.009	4.999	-.010
25	C	5.079	5.075	-.004
29	C	4.963	4.949	-.014
33	C	4.986	4.980	-.006
37	C	5.014	4.998	-.016
41	C	5.104	5.092	-.012
45	C	4.756	4.746	-.010
49	C	4.994	4.988	-.006
53	C	5.046	5.045	-.001
57	C	5.045	5.040	-.005
59	C	5.020	5.005	-.015
61	C	5.121	5.109	-.012
63	C	5.123	5.135	+.012
65	C	5.098	5.084	-.014



Section No. 2

Date	11-27-40	2-24-41
Time	2:30 p.m.	2:30 p.m.
T. Concrete F.	40	42
T. Air F.	34	42

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
1	Exp.	5.072	5.055	-.017
2	C	5.080	5.100	+.020
4	C	5.125	5.111	-.014
6	C	5.145	5.127	-.018
8	C	5.072	5.065	-.007
10	C	5.116	5.108	-.008
12	C	5.035	5.030	-.005
14	C	5.069	5.064	-.005
16	C	5.047	5.035	-.012
18	C	5.146	5.152	+.006
20	C	5.042	5.040	-.002
22	C	5.119	5.104	-.015
24	C	5.068	5.064	-.004
26	C	5.064	5.056	-.008
28	C	5.046	5.037	-.009
30	C	5.062	5.050	-.012
32	C	5.064	5.060	-.004
34	C	5.103	5.092	-.011
36	C	5.135	5.124	-.011
38	C	5.051	5.038	-.013
40	C	5.137	5.130	-.007
41	Exp.	5.992	6.099	+.107



### Section No. 3

Date	11-27-40	2-24-41
Time	2:00 p.m.	2:00 p.m.
T. Concrete F.	40	42
T. Air F.	34	41

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
1	Exp.	6.167	6.137	-.030
2	C	5.180	5.181	+.001
4	C	5.012	5.010	-.002
6	C	5.114	5.098	-.016
8	C	5.156	5.144	-.012
10	C	5.168	5.170	+.002
12	C	5.052	5.037	-.015
14	C	5.285	5.274	-.011
16	C	5.218	5.197	-.021
18	C	5.027	5.018	-.009
20	C	5.124	5.123	-.001
21	Exp.	5.008	4.990	-.018
41	Exp.	5.971	5.948	-.023

### Section No. 4

Date	11-27-40	2-24-41
Time	1:30 p.m.	1:30 p.m.
T. Concrete F.	40	42
T. Air F.	34	42

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
7	Exp.	5.888	5.856	-.032
8	C	5.077	5.084	+.007
9	C	5.149	5.140	-.009
10	C	5.069	5.055	-.014
11	C	5.128	5.131	+.003
12	C	5.038	5.056	+.018
13	Exp.	5.025	4.992	-.033
19	Exp.	6.052	6.026	-.026
20	C	5.118	5.116	-.002
21	C	5.055	5.054	-.001
22	C	5.045	5.048	+.003
23	C	5.040	5.039	-.001
24	C	5.176	5.173	-.003
25	Exp.	4.954	4.930	-.024



Section No. 5

Date	11-27-40	2-24-41
Time	1:00 p.m.	1:00 p.m.
T. Concrete F.	40	42
T. Air F.	34	42

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
7	Exp.	6.164	6.124	-.040
8	C	5.098	5.100	+.002
9	C	5.032	5.020	-.012
10	C	5.079	5.063	-.016
11	C	5.052	5.059	+.007
12	C	5.039	5.043	+.004
13	Exp.	5.148	5.137	-.011
19	Exp.	6.113	6.085	-.028
20	C	5.028	5.029	+.001
21	C	5.104	5.097	-.007
22	C	5.122	5.107	-.015
23	C	5.104	5.098	-.006
24	C	5.197	5.199	+.002
25	Exp.	5.181	5.167	-.014

Section No. 6

Date	11-27-40	2-24-41
Time	12:30 p.m.	12:30 p.m.
T. Concrete F.	40	42
T. Air F.	32	41

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
1	Exp.	5.588	5.562	-.026
2	C	5.032	5.020	-.012
3	Exp.	5.248	5.230	-.018
4	C	5.560	5.560	.000
5	Exp.	5.449	5.418	-.031
6	C	5.173	5.177	+.004
7	Exp.	5.191	5.169	-.022
8	C	5.264	5.261	-.003
9	Exp.	5.561	5.546	-.015
10	C	5.170	5.164	-.006
11	Exp.	5.999	5.990	-.009



Section No. 7

Date	11-27-40	2-24-41
Time	12:00 m.	12:00 m.
T. Concrete F.	40	42
T. Air F.	32	41

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
7	Exp.	6.024	5.969	-.055
8	C	5.061	5.072	+.011
9	C	5.345	5.339	-.006
10	C	5.185	5.184	-.001
11	C	4.914	4.915	+.001
12	C	5.123	5.128	+.005
13	Exp.	5.930	5.884	-.046
19	Exp.	5.425	5.374	-.051
20	C	5.032	5.032	..000
21	C	5.092	5.107	+.015
22	C	5.642	5.617	-.025
23	C	4.922	4.930	+.008
24	C	5.163	5.178	+.015
25	Exp.	5.521	5.484	-.037



# Section Standard

Date	11-27-40	2-24-41
Time	3:30 p.m.	3:30 p.m.
T. Concrete F.	42	43
T. Air F.	34	43

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
1	Exp.	5.225	5.204	-.021
2	C	4.956	4.955	-.001
4	C	5.129	5.139	+.010
6	C	4.986	4.987	+.001
8	C	5.096	5.104	+.008
10	C	5.064	5.057	-.007
11	C	5.012	5.018	+.006
12	C	5.156	5.144	-.012
14	C	5.060	5.058	-.002
16	C	4.998	4.997	-.001
17	Exp.	5.530	5.513	-.017
18	C	5.184	5.179	-.005
19	C	5.110	5.099	-.011
20	C	5.200	5.208	+.008
21	Exp.	5.516	5.502	-.014
22	C	5.096	5.088	-.008
23	C	5.144	5.136	-.008
24	C	5.016	5.020	+.004
25	Exp.	5.149	5.145	-.004
26	C	5.188	5.183	-.005
28	C	5.092	5.085	-.007
30	C	5.211	5.210	-.001
31	C	5.112	5.100	-.012
32	C	5.140	5.139	-.001
34	C	5.204	5.208	+.004
36	C	5.084	5.078	-.006
38	C	5.053	5.048	-.005
40	C	5.070	5.072	+.002
41	Exp.	5.280	5.255	-.025



The changes in widths of the joints which were caused by the daily temperature cycle of May 28, 1941, are as follows:

Section No. 1

Time 5:45 a.m. 3:40 p.m.  
 T. Concrete F. 75 106  
 T. Air F. 75 94

Jt. No.	Type	5:45 a.m.	3:40 p.m.	Jt. Width Change
1	C	1.025	1.025	0.000
2	C	1.025	1.025	0.000
3	C	1.025	1.025	0.000
4	C	1.025	1.025	0.000
5	C	1.025	1.025	0.000
6	C	1.025	1.025	0.000
7	C	1.025	1.025	0.000
8	C	1.025	1.025	0.000
9	C	1.025	1.025	0.000
10	C	1.025	1.025	0.000
11	C	1.025	1.025	0.000
12	C	1.025	1.025	0.000
13	C	1.025	1.025	0.000
14	C	1.025	1.025	0.000
15	C	1.025	1.025	0.000
16	C	1.025	1.025	0.000
17	C	1.025	1.025	0.000
18	C	1.025	1.025	0.000
19	C	1.025	1.025	0.000
20	C	1.025	1.025	0.000
21	C	1.025	1.025	0.000
22	C	1.025	1.025	0.000
23	C	1.025	1.025	0.000
24	C	1.025	1.025	0.000
25	C	1.025	1.025	0.000
26	C	1.025	1.025	0.000
27	C	1.025	1.025	0.000
28	C	1.025	1.025	0.000
29	C	1.025	1.025	0.000
30	C	1.025	1.025	0.000
31	C	1.025	1.025	0.000
32	C	1.025	1.025	0.000
33	C	1.025	1.025	0.000
34	C	1.025	1.025	0.000
35	C	1.025	1.025	0.000
36	C	1.025	1.025	0.000
37	C	1.025	1.025	0.000
38	C	1.025	1.025	0.000
39	C	1.025	1.025	0.000
40	C	1.025	1.025	0.000
41	C	1.025	1.025	0.000
42	C	1.025	1.025	0.000
43	C	1.025	1.025	0.000
44	C	1.025	1.025	0.000
45	C	1.025	1.025	0.000
46	C	1.025	1.025	0.000
47	C	1.025	1.025	0.000
48	C	1.025	1.025	0.000
49	C	1.025	1.025	0.000
50	C	1.025	1.025	0.000
51	C	1.025	1.025	0.000
52	C	1.025	1.025	0.000
53	C	1.025	1.025	0.000
54	C	1.025	1.025	0.000
55	C	1.025	1.025	0.000
56	C	1.025	1.025	0.000
57	C	1.025	1.025	0.000
58	C	1.025	1.025	0.000
59	C	1.025	1.025	0.000
60	C	1.025	1.025	0.000
61	C	1.025	1.025	0.000
62	C	1.025	1.025	0.000
63	C	1.025	1.025	0.000
64	C	1.025	1.025	0.000
65	C	1.025	1.025	0.000
66	C	1.025	1.025	0.000
67	C	1.025	1.025	0.000
68	C	1.025	1.025	0.000
69	C	1.025	1.025	0.000
70	C	1.025	1.025	0.000
71	C	1.025	1.025	0.000
72	C	1.025	1.025	0.000
73	C	1.025	1.025	0.000
74	C	1.025	1.025	0.000
75	C	1.025	1.025	0.000
76	C	1.025	1.025	0.000
77	C	1.025	1.025	0.000
78	C	1.025	1.025	0.000
79	C	1.025	1.025	0.000
80	C	1.025	1.025	0.000
81	C	1.025	1.025	0.000
82	C	1.025	1.025	0.000
83	C	1.025	1.025	0.000
84	C	1.025	1.025	0.000
85	C	1.025	1.025	0.000
86	C	1.025	1.025	0.000
87	C	1.025	1.025	0.000
88	C	1.025	1.025	0.000
89	C	1.025	1.025	0.000
90	C	1.025	1.025	0.000
91	C	1.025	1.025	0.000
92	C	1.025	1.025	0.000
93	C	1.025	1.025	0.000
94	C	1.025	1.025	0.000
95	C	1.025	1.025	0.000
96	C	1.025	1.025	0.000
97	C	1.025	1.025	0.000
98	C	1.025	1.025	0.000
99	C	1.025	1.025	0.000
100	C	1.025	1.025	0.000

Section No. 2

Time 5:45 a.m. 2:50 p.m.  
 T. Concrete F. 75 106  
 T. Air F. 75 94

XVII. DAILY CHANGES IN JOINT WIDTH MEASUREMENTS MAY 28, 1941

1	C	1.025	1.025	0.000
2	C	1.025	1.025	0.000
3	C	1.025	1.025	0.000
4	C	1.025	1.025	0.000
5	C	1.025	1.025	0.000
6	C	1.025	1.025	0.000
7	C	1.025	1.025	0.000
8	C	1.025	1.025	0.000
9	C	1.025	1.025	0.000
10	C	1.025	1.025	0.000
11	C	1.025	1.025	0.000
12	C	1.025	1.025	0.000
13	C	1.025	1.025	0.000
14	C	1.025	1.025	0.000
15	C	1.025	1.025	0.000
16	C	1.025	1.025	0.000
17	C	1.025	1.025	0.000
18	C	1.025	1.025	0.000
19	C	1.025	1.025	0.000
20	C	1.025	1.025	0.000
21	C	1.025	1.025	0.000
22	C	1.025	1.025	0.000
23	C	1.025	1.025	0.000
24	C	1.025	1.025	0.000
25	C	1.025	1.025	0.000
26	C	1.025	1.025	0.000
27	C	1.025	1.025	0.000
28	C	1.025	1.025	0.000
29	C	1.025	1.025	0.000
30	C	1.025	1.025	0.000
31	C	1.025	1.025	0.000
32	C	1.025	1.025	0.000
33	C	1.025	1.025	0.000
34	C	1.025	1.025	0.000
35	C	1.025	1.025	0.000
36	C	1.025	1.025	0.000
37	C	1.025	1.025	0.000
38	C	1.025	1.025	0.000
39	C	1.025	1.025	0.000
40	C	1.025	1.025	0.000
41	C	1.025	1.025	0.000
42	C	1.025	1.025	0.000
43	C	1.025	1.025	0.000
44	C	1.025	1.025	0.000
45	C	1.025	1.025	0.000
46	C	1.025	1.025	0.000
47	C	1.025	1.025	0.000
48	C	1.025	1.025	0.000
49	C	1.025	1.025	0.000
50	C	1.025	1.025	0.000
51	C	1.025	1.025	0.000
52	C	1.025	1.025	0.000
53	C	1.025	1.025	0.000
54	C	1.025	1.025	0.000
55	C	1.025	1.025	0.000
56	C	1.025	1.025	0.000
57	C	1.025	1.025	0.000
58	C	1.025	1.025	0.000
59	C	1.025	1.025	0.000
60	C	1.025	1.025	0.000
61	C	1.025	1.025	0.000
62	C	1.025	1.025	0.000
63	C	1.025	1.025	0.000
64	C	1.025	1.025	0.000
65	C	1.025	1.025	0.000
66	C	1.025	1.025	0.000
67	C	1.025	1.025	0.000
68	C	1.025	1.025	0.000
69	C	1.025	1.025	0.000
70	C	1.025	1.025	0.000
71	C	1.025	1.025	0.000
72	C	1.025	1.025	0.000
73	C	1.025	1.025	0.000
74	C	1.025	1.025	0.000
75	C	1.025	1.025	0.000
76	C	1.025	1.025	0.000
77	C	1.025	1.025	0.000
78	C	1.025	1.025	0.000
79	C	1.025	1.025	0.000
80	C	1.025	1.025	0.000
81	C	1.025	1.025	0.000
82	C	1.025	1.025	0.000
83	C	1.025	1.025	0.000
84	C	1.025	1.025	0.000
85	C	1.025	1.025	0.000
86	C	1.025	1.025	0.000
87	C	1.025	1.025	0.000
88	C	1.025	1.025	0.000
89	C	1.025	1.025	0.000
90	C	1.025	1.025	0.000
91	C	1.025	1.025	0.000
92	C	1.025	1.025	0.000
93	C	1.025	1.025	0.000
94	C	1.025	1.025	0.000
95	C	1.025	1.025	0.000
96	C	1.025	1.025	0.000
97	C	1.025	1.025	0.000
98	C	1.025	1.025	0.000
99	C	1.025	1.025	0.000
100	C	1.025	1.025	0.000



The changes in widths of the joints which were caused by the daily temperature cycle of May 28, 1941, are as follows:

### Section No. 1

Time	5:45 a.m.	3:10 p.m.
T. Concrete F.	79	106
T. Air F.	72	94

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
1	C	5.024	4.970	-.054
5	C	5.000	4.960	-.040
10	C	4.980	4.953	-.027
29	C	4.918	4.887	-.031
33	C	4.946	4.904	-.042
56	C	4.870	4.838	-.032
61	C	5.081	5.045	-.036
65	C	5.060	5.025	-.035

### Section No. 2

Time	5:15 a.m.	2:50 p.m.
T. Concrete F.	79	106
T. Air F.	68	94

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
1	Exp.	4.688	4.636	-.052
2	C	5.067	5.030	-.037
6	C	5.102	5.073	-.029
11	C	5.050	5.017	-.033
20	C	5.014	4.985	-.029
22	C	5.089	5.056	-.033
31	C	5.064	5.032	-.032
36	C	5.092	5.048	-.044
40	C	5.115	5.067	-.048
41	Exp.	5.480	5.432	-.048



### Section No. 3

Time	5:00 a.m.	2:40 p.m.
T. Concrete F.	80	106
T. Air F.	68	93

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
1	Exp.	5.649	5.611	-.038
2	C	5.172	5.121	-.051
6	C	5.095	5.055	-.040
11	C	5.108	5.081	-.027
16	C	5.173	5.135	-.038
20	C	5.110	5.059	-.051
21	Exp.	4.498	4.441	-.057

### Section No. 5

Time	4:45 a.m.	2:30 p.m.
T. Concrete F.	80	106
T. Air F.	68	93

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
7	Exp.	5.811	5.750	-.061
8	C	5.136	5.095	-.041
9	C	5.042	5.000	-.042
10	C	5.068	5.028	-.040
11	C	5.085	5.045	-.040
12	C	5.070	5.029	-.041
13	Exp.	4.815	4.734	-.081

Note: Measurement of the daily change in widths of the joints in Section No. 4 is not scheduled.



# Section No. 6

Time	4:30 a.m.	2:15 p.m.
T. Concrete F.	81	106
T. Air F.	68	92

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
3	Exp.	4.950	4.793	-.157
4	C	5.560	5.485	-.075
5	Exp.	5.185	5.044	-.141
6	C	5.185	5.108	-.077
7	Exp.	4.875	4.716	-.159

# Section No. 7

Time	4:15 a.m.	2:00 p.m.
T. Concrete F.	81	104
T. Air F.	68	92

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
7	Exp.	5.653	5.580	-.073
8	C	5.106	5.056	-.050
9	C	5.366	5.320	-.046
10	C	5.199	5.155	-.044
11	C	4.930	4.885	-.045
12	C	5.153	5.100	-.053
13	Exp.	5.575	5.500	-.075



# SUMMARY OF THE DAILY CHANGES IN WIDTHS OF THE JOINTS MAY 23, 1941

## Section No. 1. Design Section Standard

Time	6:00 a.m.	3:30 p.m.
T. Concrete F.	78	104
T. Air F.	75	92

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
17	Exp.	5.269	5.168	-.101
18	C	5.182	5.123	-.059
19	C	5.088	5.048	-.040
20	C	5.222	5.165	-.057
21	Exp.	5.226	5.140	-.086
22	C	5.118	5.066	-.052
23	C	5.128	5.073	-.055
24	C	5.028	4.997	-.031
25	Exp.	4.881	4.772	-.109

Section No. 5. Design - expansion joints spaced 120 feet apart and intermediate contraction joints spaced 30 feet apart. For an increase in pavement temperature of 25 F., the average decrease in width of the expansion joints was .071 inches, and the average decrease in width of the contraction joints was .041 inches.

Section No. 6. Design - alternate expansion and contraction joints spaced 60 feet apart. For an increase in pavement temperature of 25 F., the average decrease in width of the expansion joints was .132 inches, and the average decrease in width of the contraction joints was .076 inches.

Section No. 7. Design - expansion joints spaced 120 feet apart and intermediate contraction joints spaced 30 feet apart. For an increase in pavement temperature of 25 F., the average decrease in width of the expansion joints was .074 inches, and the average decrease in width of the contraction joints was .042 inches.

Section Standard Design - expansion joints spaced 120 feet apart and intermediate contraction joints spaced 30 feet apart. For an increase in pavement temperature of 25 F., the average decrease in width of the expansion joints was .074 inches, and the average decrease in width of the contraction joints was .042 inches.



SUMMARY OF THE DAILY CHANGES IN WIDTHS OF THE JOINTS MAY 28, 1941

- Section No. 1. Design - contraction joints only, spaced 20 feet apart. For an increase in pavement temperature of 27 F., the average decrease in width of the joints was .037 inches.
- Section No. 2. Design - expansion joints spaced 800 feet apart and intermediate contraction joints spaced 20 feet apart. For an increase in pavement temperature of 27 F., the average decrease in width of the expansion joints was .050 inches, and the average decrease in width of the contraction joints was .036 inches.
- Section No. 3. Design - expansion joints spaced 400 feet apart and intermediate contraction joints spaced 20 feet apart. For an increase in pavement temperature of 26 F., the average decrease in width of the expansion joints was .048 inches, and the average decrease in width of the contraction joints was .041 inches.
- Section No. 5. Design - expansion joints spaced 120 feet apart and intermediate contraction joints spaced 20 feet apart. For an increase in pavement temperature of 26 F., the average decrease in width of the expansion joints was .071 inches, and the average decrease in width of the contraction joints was .041 inches.
- Section No. 6. Design - alternate expansion and contraction joints spaced 60 feet apart. For an increase in pavement temperature of 25 F., the average decrease in width of the expansion joints was .152 inches, and the average decrease in width of the contraction joints was .076 inches.
- Section No. 7. Design - expansion joints spaced 120 feet apart and intermediate contraction joints spaced 20 feet apart. For an increase in pavement temperature of 23 F., the average decrease in width of the expansion joints was .074 inches, and the average decrease in width of the contraction joints was .048 inches.
- Section Standard Design - expansion joints spaced 120 feet apart and intermediate contraction joints spaced 30 feet apart. For an increase in pavement temperature of 26 F., the average decrease in width of the expansion joints was .099 inches, and the average decrease in width of the contraction joints was .049 inches.



The seasonal changes in width of the joints between February 24, 1941 and May 27, 1941 are as follows:

Section No. 1

Date	2-24-41	5-27-41
Time	3:00 p.m.	2:30 p.m.
Concrete F.	43	104
Air F.	42	32

St. No.	Time	Temp	Temp	St. Width
		inches	inches	inches
1	0	0.02	0.02	0.02
2	0	0.02	0.02	0.02
3	0	0.02	0.02	0.02
4	0	0.02	0.02	0.02
5	0	0.02	0.02	0.02
6	0	0.02	0.02	0.02
7	0	0.02	0.02	0.02
8	0	0.02	0.02	0.02
9	0	0.02	0.02	0.02
10	0	0.02	0.02	0.02
11	0	0.02	0.02	0.02
12	0	0.02	0.02	0.02
13	0	0.02	0.02	0.02
14	0	0.02	0.02	0.02
15	0	0.02	0.02	0.02
16	0	0.02	0.02	0.02
17	0	0.02	0.02	0.02
18	0	0.02	0.02	0.02
19	0	0.02	0.02	0.02
20	0	0.02	0.02	0.02
21	0	0.02	0.02	0.02
22	0	0.02	0.02	0.02
23	0	0.02	0.02	0.02
24	0	0.02	0.02	0.02
25	0	0.02	0.02	0.02
26	0	0.02	0.02	0.02
27	0	0.02	0.02	0.02
28	0	0.02	0.02	0.02
29	0	0.02	0.02	0.02
30	0	0.02	0.02	0.02
31	0	0.02	0.02	0.02
32	0	0.02	0.02	0.02
33	0	0.02	0.02	0.02
34	0	0.02	0.02	0.02
35	0	0.02	0.02	0.02
36	0	0.02	0.02	0.02
37	0	0.02	0.02	0.02
38	0	0.02	0.02	0.02
39	0	0.02	0.02	0.02
40	0	0.02	0.02	0.02
41	0	0.02	0.02	0.02
42	0	0.02	0.02	0.02
43	0	0.02	0.02	0.02
44	0	0.02	0.02	0.02
45	0	0.02	0.02	0.02
46	0	0.02	0.02	0.02
47	0	0.02	0.02	0.02
48	0	0.02	0.02	0.02
49	0	0.02	0.02	0.02
50	0	0.02	0.02	0.02
51	0	0.02	0.02	0.02
52	0	0.02	0.02	0.02
53	0	0.02	0.02	0.02
54	0	0.02	0.02	0.02
55	0	0.02	0.02	0.02
56	0	0.02	0.02	0.02
57	0	0.02	0.02	0.02
58	0	0.02	0.02	0.02
59	0	0.02	0.02	0.02
60	0	0.02	0.02	0.02
61	0	0.02	0.02	0.02
62	0	0.02	0.02	0.02
63	0	0.02	0.02	0.02
64	0	0.02	0.02	0.02
65	0	0.02	0.02	0.02
66	0	0.02	0.02	0.02
67	0	0.02	0.02	0.02
68	0	0.02	0.02	0.02
69	0	0.02	0.02	0.02
70	0	0.02	0.02	0.02
71	0	0.02	0.02	0.02
72	0	0.02	0.02	0.02
73	0	0.02	0.02	0.02
74	0	0.02	0.02	0.02
75	0	0.02	0.02	0.02
76	0	0.02	0.02	0.02
77	0	0.02	0.02	0.02
78	0	0.02	0.02	0.02
79	0	0.02	0.02	0.02
80	0	0.02	0.02	0.02
81	0	0.02	0.02	0.02
82	0	0.02	0.02	0.02
83	0	0.02	0.02	0.02
84	0	0.02	0.02	0.02
85	0	0.02	0.02	0.02
86	0	0.02	0.02	0.02
87	0	0.02	0.02	0.02
88	0	0.02	0.02	0.02
89	0	0.02	0.02	0.02
90	0	0.02	0.02	0.02
91	0	0.02	0.02	0.02
92	0	0.02	0.02	0.02
93	0	0.02	0.02	0.02
94	0	0.02	0.02	0.02
95	0	0.02	0.02	0.02
96	0	0.02	0.02	0.02
97	0	0.02	0.02	0.02
98	0	0.02	0.02	0.02
99	0	0.02	0.02	0.02
100	0	0.02	0.02	0.02

XVIII. SEASONAL CHANGES IN JOINT WIDTH MEASUREMENTS  
FEB. 24, 1941 and MAY 27, 1941



The seasonal changes in width of the joints between February 24, 1941 and May 27, 1941 are as follows:

Section No. 1

Date	2-24-41	5-27-41
Time	3:00 p.m.	2:30 p.m.
T. Concrete F.	43	104
T. Air F.	42	92

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
1	C	5.049	4.972	-.077
3	C	5.200	5.150	-.050
5	C	5.019	4.960	-.059
7	C	5.128	5.071	-.057
9	C	5.039	4.979	-.060
13	C	5.040	5.000	-.040
17	C	5.056	4.995	-.061
21	C	4.999	4.944	-.055
25	C	5.075	5.006	-.069
29	C	4.949	4.888	-.061
33	C	4.980	4.904	-.076
37	C	4.998	4.940	-.058
41	C	5.092	5.024	-.068
45	C	4.746	4.688	-.058
49	C	4.988	4.915	-.073
53	C	5.045	4.980	-.065
57	C	5.040	4.990	-.050
59	C	5.005	4.945	-.060
61	C	5.109	5.046	-.063
63	C	5.135	5.072	-.063
65	C	5.084	5.022	-.062



Section No. 2

Date	2-24-41	5-27-41
Time	2:30 p.m.	2:00 p.m.
T. Concrete F.	42	102
T. Air F.	42	92

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
1	Exp.	5.055	4.645	-.410
2	C	5.100	5.033	-.067
4	C	5.111	5.052	-.059
6	C	5.127	5.072	-.055
8	C	5.065	5.015	-.050
10	C	5.108	5.060	-.048
12	C	5.030	4.985	-.045
14	C	5.064	5.019	-.045
16	C	5.035	4.987	-.048
18	C	5.152	5.093	-.059
20	C	5.040	4.983	-.057
22	C	5.104	5.056	-.048
24	C	5.064	5.010	-.054
26	C	5.056	5.000	-.056
28	C	5.037	4.984	-.053
30	C	5.050	4.980	-.070
32	C	5.060	5.003	-.057
34	C	5.092	5.032	-.060
36	C	5.124	5.046	-.078
38	C	5.038	4.972	-.066
40	C	5.130	5.064	-.066
41	Exp.	6.099	5.441	-.658



## Section No. 3

Date	2-24-41	5-27-41
Time	2:00 p.m.	1:45 p.m.
T. Concrete F.	42	100
T. Air F.	41	90

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
1	Exp.	6.137	5.622	-.515
2	C	5.181	5.124	-.057
4	C	5.010	4.960	-.050
6	C	5.098	5.055	-.043
8	C	5.144	5.100	-.044
10	C	5.170	5.116	-.054
12	C	5.037	4.977	-.060
14	C	5.274	5.225	-.049
16	C	5.197	5.139	-.058
18	C	5.018	4.963	-.055
20	C	5.123	5.060	-.063
21	Exp.	4.990	4.463	-.527
41	Exp.	5.948	5.420	-.528

## Section No. 4

Date	2-24-41	5-27-41
Time	1:30 p.m.	1:20 p.m.
T. Concrete F.	42	100
T. Air F.	42	90

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
7	Exp.	5.856	5.576	-.280
8	C	5.084	5.060	-.024
9	C	5.140	5.108	-.032
10	C	5.055	5.020	-.035
11	C	5.131	5.098	-.033
12	C	5.056	5.010	-.046
13	Exp.	4.992	4.755	-.237
19	Exp.	6.026	5.783	-.243
20	C	5.116	5.068	-.048
21	C	5.054	5.008	-.046
22	C	5.048	4.975	-.073
23	C	5.039	4.998	-.041
24	C	5.173	5.152	-.021
25	Exp.	4.930	4.599	-.331



Section No. 5

Date	2-24-41	5-27-41
Time	1:00 p.m.	1:00 p.m.
T. Concrete F.	42	100
T. Air F.	42	88

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
7	Exp.	6.124	5.774	-.350
8	C	5.100	5.094	-.006
9	C	5.020	5.003	-.017
10	C	5.063	5.032	-.031
11	C	5.059	5.046	-.013
12	C	5.043	5.032	-.011
13	Exp.	5.137	4.765	-.372
19	Exp.	6.085	5.728	-.357
20	C	5.029	5.019	-.010
21	C	5.097	5.082	-.015
22	C	5.107	5.060	-.047
23	C	5.098	5.072	-.026
24	C	5.199	5.194	-.005
25	Exp.	5.167	4.821	-.346

Section No. 6

Date	2-24-41	5-27-41
Time	12:30 p.m.	12:15 p.m.
T. Concrete F.	42	99
T. Air F.	41	90

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
1	Exp.	5.562	5.182	-.380
2	C	5.020	4.960	-.060
3	Exp.	5.230	4.853	-.377
4	C	5.560	5.490	-.070
5	Exp.	5.418	5.082	-.336
6	C	5.177	5.110	-.067
7	Exp.	5.169	4.775	-.394
8	C	5.261	5.187	-.074
9	Exp.	5.546	5.185	-.361
10	C	5.164	5.114	-.050
11	Exp.	5.990	5.590	-.400



# Section No. 7

Date	2-24-41	5-27-41
Time	12:00 m.	12:00 m.
T. Concrete F.	42	98
T. Air F.	41	88

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
7	Exp.	5.969	5.618	-.351
8	C	5.072	5.060	-.012
9	C	5.339	5.321	-.018
10	C	5.184	5.162	-.022
11	C	4.915	4.890	-.025
12	C	5.128	5.100	-.028
13	Exp.	5.884	5.532	-.352
19	Exp.	5.374	5.022	-.352
20	C	5.032	5.039	+.007
21	C	5.107	5.089	-.018
22	C	5.617	5.573	-.044
23	C	4.930	4.907	-.023
24	C	5.178	5.148	-.030
25	Exp.	5.484	5.175	-.309



# Section Standard

Date	2-24-41	5-27-41
Time	3:30 p.m.	2:45 p.m.
T. Concrete F.	43	102
T. Air F.	43	93

Jt. No.	Type	Gage inches	Gage inches	Jt. Width Change inches
1	Exp.	5.204	4.830	-.374
2	C	4.955	4.950	-.005
4	C	5.139	5.124	-.015
6	C	4.987	4.967	-.020
8	C	5.104	5.065	-.039
10	C	5.057	5.034	-.023
11	C	5.018	4.954	-.064
12	C	5.144	5.114	-.030
14	C	5.058	5.021	-.037
16	C	4.997	4.962	-.035
17	Exp.	5.513	5.178	-.335
18	C	5.179	5.124	-.055
19	C	5.099	5.042	-.057
20	C	5.208	5.164	-.044
21	Exp.	5.502	5.145	-.357
22	C	5.088	5.060	-.028
23	C	5.136	5.070	-.066
24	C	5.020	4.993	-.027
25	Exp.	5.145	4.782	-.363
26	C	5.183	5.145	-.038
28	C	5.085	5.053	-.032
30	C	5.210	5.176	-.034
31	C	5.100	5.040	-.060
32	C	5.139	5.100	-.039
34	C	5.208	5.175	-.033
36	C	5.078	5.050	-.028
38	C	5.048	5.020	-.028
40	C	5.072	5.055	-.017
41	Exp.	5.255	4.884	-.371



# EXPERIMENTAL INVESTIGATION OF THE EFFECTS OF TEMPERATURE ON THE

Observations

July 1, 1940

July 1, 1940

July 1, 1940

July 1, 1940

July 1, 1940

July 1, 1940

July 1, 1940

July 1, 1940

July 1, 1940

July 1, 1940

July 1, 1940

July 1, 1940

July 1, 1940

July 1, 1940

July 1, 1940

July 1, 1940

July 1, 1940

July 1, 1940

July 1, 1940

July 1, 1940

July 1, 1940

July 1, 1940

July 1, 1940

July 1, 1940

July 1, 1940

July 1, 1940

July 1, 1940

## XIX. CONSTRUCTION DIARY

July 1, 1940

July 1, 1940

July 1, 1940

July 1, 1940



# COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Daviess County Kentucky

Owensboro-Hartford FA-125-F(2)S

Daily Observations

Date July 8, 1940

## 1. Weather

Temp. 9:00 a.m. 72°F. Cloudy  
12:00 m. 80°F. "  
3:00 p.m. 79°F. "  
 Slight wind from South.

## 12. Edging of Joints

No extra water or mortar required.  
 Joints edging O.K.

2. Station Start 737+00.0 at 10:00 a.m.  
 Station Stop 731+09.5 at 6:15 p.m.  
 Lin. Ft. 590.5

## 13. Curing

- One thickness burlap thoroughly wet during pour 7-8
- Begin burlap removal 737+00 at 6:00 a.m. 7-9
- Burlap removed 731+09.5 at 8:30 a.m. 7-9
- Pav. thoro. wet 731+09.5 at 8:30 a.m. 7-9
- Paper in place 733+00 at 8:30 a.m. 7-9
- Pav. thoro. wet all paper in place 9:30 a.m. 7-9
- Curing complete all paper 9:00 a.m.)  
 removed 11:00 a.m.) 7-12

3. See Daily Report

4. Temp. Conc. Final Finish (Broom)

## 14. Report on Construction Equipment.

No delays

5.  
 Time \_\_\_\_\_  
 Placing \_\_\_\_\_  
 Screeds \_\_\_\_\_  
 B-Float \_\_\_\_\_  
 Belt \_\_\_\_\_  
 Broom \_\_\_\_\_  
 B'lap \_\_\_\_\_  
 W-B'lap \_\_\_\_\_

## 6. Condition of Subgrade

Subgrade firm and uniform throughout  
 days run, uniform cut behind planer.

## 15. Edges of Concrete

No honeycomb in pavement edges.

## 7. Installation of Joints

All Joint Installations O.K.  
 All Dowel Holders O.K.

## 16. Joint Sealing

All joints sealed 7-29

## 17. Pictures

---- Remarks ----

Cleaning and sealing of joints begun at station 737+00, July 29, 1940. The joints were thoroughly scraped with a steel scraper and all loose material removed with a broom. Immediately after cleaning the joints were filled slightly less than flush with crack and joint filler OA-2 which has been previously heated to a temperature of approximately 250°F. This method of joint sealing was used throughout the project. While the workmanship of sealing the joints was satisfactory later inspection showed the seal to be very unsatisfactory for two reasons. The inherent quality of the OA-2, and granular material which had worked into the joints during shoulder construction.

8. Omit

9. See Joint Filler Depth Book

## 10. Longitudinal Joint Depth

Good Alignment  
1/2"-5/8"-1/2"-7/16"

## 11. Description of Mix

- Workability Plastic and workable
- Slump 1-3/4"
- Mortar Sufficient
- Segregation None
- Bleeding Slight in scattered spots A.M. and P.M.
- Time req. to harden \_\_\_\_\_



## COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Davies County Kentucky

Owensboro-Hartford FA-125-F(2)S

Daily Observations

Date July 9, 1940

## 1. Weather

Temp. 9:00 a.m. 74°F. Clear  
 12:00 m. 86°F. Cloudy  
 3:00 p.m. 84°F. Cloudy  
 Rain 12:30 p.m. to 1:00 p.m.  
 Slight wind from South.

2. Station Start 731+09.5 at 5:00 a.m.  
 Station Stop 725+40.0 at 12:30 p.m.  
 Lin. Ft. 569.5

3. See Daily Report

4. Temp. Conc. Final Finish (Broom)

5. Time	10:25 a.m.	11:52 a.m.
Placing	727+50	726+00
Screeds	727+50	726+00
	728+00	726+60
B-Float	728+10	726+60
	728+40	727+10
Belt	728+90	727+40
Broom	729+10	727+50
B'lap	729+30	727+90
W-B'lap	729+30	727+90
		12:10 p.m.
		727+50

## 6. Condition of Subgrade

Subgrade firm and uniform throughout  
 days run, uniform cut behind planer.

## 7. Installation of Joints

All Joint Installations O.K.  
 All Dowel Holders O.K.

## 8. Omit

## 9. See Joint Filler Depth Book

## 10. Longitudinal Joint Depth

Good Alignment  
1/2"-7/16"-3/4"-1/2"-1/2"

## 11. Description of Mix

a. Workability Plastic and Workable  
 b. Slump 1-3/4"  
 c. Mortar Sufficient  
 d. Segregation None  
 e. Bleeding Slight in scattered spots a.m. and p.m.  
 f. Time req. to harden \_\_\_\_\_

## 12. Edging of Joints

Contraction joints 726+40, 60, 80,  
 edged roughly due to rain. No extra  
 water or mortar required.

## 13. Curing

a. One thickness burlap thoroughly wet  
 during pour 7-9  
 b. Begin burlap  
 removal 731+09.5 at 6:00 a.m. 7-10  
 c. Burlap removed 725+40 at 8:00 a.m. 7-10  
 d. Pav. thoro. wet 725+40 at 8:00 a.m. 7-10  
 e. Paper in place 727+50 at 8:00 a.m. 7-10  
 f. Pav. thoro. wet all paper in  
 place 9:00 a.m. 7-10  
 g. Curing complete all paper 8:00 a.m.) 7-13  
 removed 9:30 a.m.)

## 14. Report on Construction Equipment.

## 15. Edges of Concrete

No honeycomb in pavement edges.

## 16. Joint Sealing

All joints sealed 7-29.

## 17. Pictures

---- Remarks ----

P.R.A. Beam Sec. No. 7 725+80 at 12:30 p.m.

Several batches mixed after start of rain at  
 12:30 p.m. Concrete exposed to rain 726+50  
 to header at 725+40, finishing completed at  
 1:00 p.m.

Finishing machine makes two to three trips  
 over concrete.

Bull float makes two to four trips over  
 concrete.

Contraction joints 1" in width when com-  
 pletely finished.

High spot left of C.L. at 726+50 rubbed down  
 with carborundum 7-10.

Final broom 9:00 p.m.



# COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Daviess County Kentucky

Owensboro-Hartford FA-125-F(2)S

Daily Observations

Date July 10, 1948

## 1. Weather

Temp. 7:30 a.m. 74°F. Clear  
1:45 p.m. 90°F. "  
4:00 p.m. 89°F. "  
slight wind from south.

## 12. Edging of Joints

Extra mortar used in finishing Jt. 725+40 worked in by Bull Float. No extra water or mortar used in finishing remainder.

## 2. Station Start

Station Stop 716+00 at 6:15 p.m.

Lin. Ft. 940.0

## 13. Curing

- One thickness burlap thoroughly wet during pour 7-10
- Begin burlap removal 725+40 at 5:30 a.m. 7-11
- Burlap removed 716+00 at 8:50 a.m. 7-11
- Pav. thoro. wet 716+00 at 8:50 a.m. 7-11
- Paper in place 720+85 at 8:00 a.m. 7-11
- Pav. thoro. wet all paper in place 10:30 a.m. 7-11
- Curing complete all paper removed 6:30 a.m. 7-15  
11:00 a.m. 7-15

## 3. See Daily Report

## 4. Temp. Conc. Final Finish (Broom)

11:45 (T. Conc. 98° 4:00 ( 99°  
p.m. (T. Air 90° p.m. ( 89°

	9:30 a.m.	11:02 a.m.	1:30 p.m.	2:52 p.m.
Placing	722+70	720+94	719+50	718+50
Screeds	722+80	721+54	719+50	718+70
	723+20	721+84	720+00	718+90
B-Float	723+20	722+34	720+00	719+00
	723+30	722+64	720+60	719+25
Belt	724+00	722+64	720+60	719+25
Broom	724+60	722+70	720+60	719+50
B'lap	725+00	723+34	721+20	719+90
W-B'lap	725+00	723+34	721+20	720+10
	11:15 a.m.	3:10 p.m.		
	722+70	719+50		

## 6. Condition of Subgrade

Subgrade firm and uniform throughout days run, uniform cut behind planer.

## 14. Report on Construction Equipment.

Delay of 25 min. at 6:30 a.m. 725+20. Assemblying strike off for wire mesh. Delay of 20 min. at 3:10 p.m. 718+00. Setting subgrade template for curve.

## 15. Edges of Concrete

Slight honeycomb five places left edge of pavement. Honeycomb in back of lip curb.

## 16. Joint Sealing

All joints sealed 7-29.

## 7. Installation of Joints

Cap for expansion joint 723+80 caught on screed, and joint tipped. Attempt to straighten very unsatisfactory. Expansion joint filler 721+40 trimmed at C.L., 1/8" opening, wire rack O.K. Some of spot welds on dowel holders for exp. and cent. jts. 721+40 to 725+00 broken in trucking. Attempt to wire holder together in broken spots very unsatisfactory. Inspection made of all dowel holders and broken ones discarded. Error in handling holders corrected.

## 8. Omit

## 9. See Joint Filler Depth Book

## 10. Longitudinal Joint Depth

Good Alignment.

5/8"-1/2"-1/2"-5/8"-7/16"

## 11. Description of Mix

- Workability Plastic and Workable.
- Slump 1-7/8"
- Mortar Sufficient
- Segregation None
- Bleeding Slight in four spots a.m. Slight p.m.
- Time req. to harden

## 17. Pictures

----- Remarks -----

Beams 1, 2, 3 720+70 at 11:30 a.m.  
F.R.A. Beam Sec. No. 6 720+70 at 11:30 a.m.

Section 7 completed, begin Sec. 6 7:00 a.m. 725+00.

No dowels installed in expansion joint 725+00.

Practice of oiling dowels with crankcase oil and large brush and sweeping with gloved hand stopped. Beginning at 722 dowels oiled with cylinder oil and paint brush.

Beginning at 719+60 concretehand placed around dowels before finishing machine.

Delay of 10 min. at 2:00 p.m. 719+00. Installing flume accessories. Very wet batch 716+40 rt. side near C.L., mixer trouble. Succeeding and preceding batches O.K.



# COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

aviess County Kentucky

Owensboro-Hartford FA-125-F(2)S

Daily Observations

Date July 11, 1940

1. Weather

Temp. 8:00 a.m. 80°F. Clear  
12:00 m. 90°F. "  
3:00 p.m. 94°F. "  
Slight wind from South.

12. Edging of Joints

Joint edging good, no extra water or mortar required.

2. Station Start 715+00 at 5:15 a.m.  
Station Stop 705+40 at 5:25 p.m.  
Lin. Ft. 1050.0

13. Curing

- One thickness burlap thoroughly wet during pour 7-11.
- Begin burlap removal 715+00 at 6:30 a.m. 7-12
- Burlap removed 705+40 at 7:45 a.m. 7-12
- Pav. thoro. wet 705+40 at 7:45 a.m. 7-12
- Paper in place 711+50 at 7:45 a.m. 7-12
- Pav. thoro. wet all paper in place 9:20 a.m. 7-12
- Curing complete all paper removed 6:30 a.m. 7-12  
11:00 a.m. 7-12

3. See Daily Report

4. Temp. Conc. Final Finish (Broom)  
9:25 a.m. ( T. Conc. 85°  
( T. Air 86°

	a.m.		p.m.	
Time	9:00	10:20	2:00	3:27
Placing	712+75	711+95	708+30	707+40
Screeds	713+00	712+10	708+35	707+45
	713+25	712+35	708+70	707+60
B-Float	713+25	712+35	708+90	707+60
	713+50	712+75	709+30	708+00
Belt	713+60	712+75	709+35	708+05
Broom	714+20	713+85	710+00	708+30
B'lap	715+20	714+05	710+00	708+65
W-B'lap	715+20	714+05	710+00	708+65
	10:40 a.m.		3:40 p.m.	
	712+75		708+30	

6. Condition of Subgrade

Subgrade firm and uniform throughout  
days run, uniform cut behind planer.

14. Report on Construction Equipment.

Cap for cont. jt. filler changed from  
5/8" out to out width to 1/2" out to out  
width at station 712+40.

7. Installation of Joints

All Joint Installations O.K.  
All Boxed Borders O.K.

15. Edges of Concrete

Numerous honeycomb spots in lip curb.  
No honeycomb in pavement edges.

16. Joint Sealing

All joints sealed 7-23.

17. Pictures

----- Remarks -----

Beams 4, 5, 6 710+75 at 10:30 a.m.

Section 6 completed, begin Sec. 5  
12:00 m. 710+00.

New width finished contraction joint 3/4"

Contraction joints show 1/32" opening  
7:30 a.m. 7-12

Finishing completed 7:15 p.m. 7-11.

8. Omit

9. See Joint Filler Depth Book

10. Longitudinal Joint Depth

Good Alignment  
5/8"-11/16"-1/2"-5/8"-11/16"

11. Description of Mix

- Workability Plastic and Workable, very uniform.
- Slump 1-3/4"
- Mortar O.K. Good mortar roll on rear screed.
- Segregation None
- Bleeding Slight spots near C.L. a.m., none p.m.
- Time req. to harden



## COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Davies County Kentucky

Owensboro-Hartford FA-125-F(2)S

Daily Observations

Date July 12, 1940

## 1. Weather

Temp. 7:30 a.m. 72°F. Cloudy  
 12:00 m. 82°F. "  
 3:00 p.m. 83°F. "

No wind. Rain 12:15 p.m. to  
 1:30 p.m., Rain 4:00 p.m.

2. Station Start 705+40 at 9:27 a.m.  
 Station Stop 703+40 at 12:45 p.m.  
 Lin. Ft. 200.0

3. See Daily Report

4. Temp. Conc. Final Finish (Broom)

12:00 m. (T. Conc. 88°  
 (T. Air 82°

5. Time 12:00 m.

Placing 703+75

Screeds 704+00

704+25

B-Float 704+50

704+75

Belt 704+95

Broom 705+20

B'lap 705+40

W-B'lap 705+40

6. Condition of Subgrade

Subgrade firm and uniform,  
 uniform cut behind planer.

7. Installation of Joints

All Joint Installations O.K.

All Dowel Holders O.K.

## 12. Edging of Joints

Extra mortar required in finishing  
 joints sta. 704+00 & 704+20. No  
 extra water or mortar required in  
 finishing remainder.

## 13. Curing

- a. One thickness burlap thoroughly wet  
 during pour None applied.  
 b. Begin burlap  
 removal 705+40 at 6:30 a.m. 7-13  
 c. Burlap removed 703+40 at 6:45 a.m. 7-13  
 d. Pav. thoro. wet 703+40 at 7:15 a.m. 7-13  
 e. Paper in place 703+40 at 7:15 a.m. 7-13  
 f. Pav. thoro. wet all paper in  
 place 7:15 a.m. 7-13  
 g. Curing complete all paper 9:30 a.m. 7-17  
 removed 1:00 p.m.

## 14. Report on Construction Equipment.

New 1/8" radius edger for joints.

## 15. Edges of Concrete

No honeycomb in pavement edges.

## 16. Joint Sealing

All joints sealed 7-29.

## 17. Pictures

----- Remarks -----

Beams 7, 8, 9 703+75 at 12:15 p.m.

Pavement surface covered with burlap  
 during rain. Burlap removed surface  
 finished 1:30 p.m. to 2:45 p.m.,  
 burlap replaced 2:55 p.m. Burlap  
 thoroughly wet, no water applied.

8. Omit

9. See Joint Filler Depth Book

10. Longitudinal Joint Depth

Good Alignment  
 3/4"-5/8"-5/8"-1/2"

11. Description of Mix

- a. Workability Plastic and Workable, uniform.  
 b. Slump 1-3/4"  
 c. Mortar O.K. Good mortar roll on rear screed.  
 d. Segregation None  
 e. Bleeding Slight over entire surface.  
 f. Time req. to harden \_\_\_\_\_



## COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Davies County Kentucky

Owensboro-Hartford FA-125-F(2)S

Daily Observations

Date July 13, 1940

## 1. Weather

Temp.

8:15 a.m. 67°F. Clear  
 12:00 m. 81°F. "  
 3:35 p.m. 80°F. "  
 Moderate wind from East

## 12. Edging of Joints

Joint edging O.K.  
 No extra water or mortar required.

## 2. Station Start

703+40 at 6:15 a.m.

## Station Stop

693+29.5 at 5:45 pm.

Lin. Ft.

1010.5

## 13. Curing

a. One thickness burlap thoroughly wet during pour 7-13

b. Begin burlap

removal 703+40 at 6:00 a.m. 7-14c. Burlap removed 697+80 at 8:30 a.m. 7-14d. Pav. thoro. wet 697+80 at 8:30 a.m. 7-14e. Paper in place 698+20 at 8:30 a.m. 7-14f. Pav. thoro. wet all paper in place 9:30 a.m. 7-14g. Curing complete all paper removed 9:30 a.m. 7-17  
1:00 p.m.

## 3. See Daily Report

## 4. Temp. Conc. Final Finish (Broom)

10:50 (T. Conc. 82° 3:35 (88°  
 a.m. (T. Air 74° p.m. (80°

	a.m.	p.m.
Time	9:45 11:58 3:20 4:25	
Placing	699+45 698+55 695+55 694+40	
Screeds	699+70 698+65 695+65 694+50	
	699+80 698+80 696+00 694+75	
B-Float	700+20 698+90 696+85 695+00	
	700+32 699+30 696+35 695+20	
Belt	700+80 699+75 696+35 695+40	
Broom	701+15 699+45 696+40 695+55	
B'lap	702+05 699+85 697+30 696+70	
W-B'lap	702+25 699+85 697+30 696+70	
	12:22 p.m. 4:55 p.m.	
	699+45 695+55	

## 6. Condition of Subgrade

Subgrade firm and uniform, uniform cut behind planer 695+00 to 703+40.  
 Subgrade spongy and non-uniform 693+29.5 to 695+00.

## 14. Report on Construction Equipment.

1/8" Edger for cont. jts. working O.K.  
 handle moved and width put to 3-1/2".  
 Finished cont. jts. 3/4" wide.

## 15. Edges of Concrete

No honeycomb in pavement edges.  
 Slight honeycomb in back of lip curb rt. side.

## 16. Joint Sealing

All joints sealed 7-29.

## 17. Pictures

---- Remarks ----

Beams 10,11,12 698+50 at 11:40 a.m.

Paver stopped 10:42 a.m. to 11:06 a.m.  
 broken clam cable.

## 8. Omit

## 9. See Joint Filler Depth Book

## 10. Longitudinal Joint Depth

Good Alignment

3/4"-7/16"-1/2"-5/8"-5/8"-1/2"

## 11. Description of Mix

a. Workability Plastic and workable, uniform.b. Slump 1-3/4"c. Mortar O.K. Good mortar roll on rear screed.d. Segregation Nonee. Bleeding Slight bleeding throughout day.

f. Time req. to harden



COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Daviess County Kentucky

Owensboro-Hartford FA-125-F(2)S

Daily Observations

Date July 14, 1940 (Sun.)

1. Weather

Temp. 8:45 a.m. 76°F. Clear  
12:00 m. 84°F. "  
3:00 p.m. 86°F. "

Slight wind from S.E.  
No Concrete Placed.

12. Edging of Joints

2. Station Start

Station Stop

Lin. Ft.

13. Curing

a. One thickness burlap thoroughly wet during pour

b. Begin burlap removal

c. Burlap removed

d. Pav. thoro. wet

e. Paper in place

f. Pav. thoro. wet all paper in place

g. Curing complete all paper removed

3. See Daily Report

4. Temp. Conc. Final Finish (Broom)

5.

Time

Placing

Screeds

B-Float

Belt

Broom

B'lap

W-B'lap

14. Report on Construction Equipment.

6. Condition of Subgrade

15. Edges of Concrete

16. Joint Sealing

7. Installation of Joints

17. Pictures

---- Remarks ----

8. Omit

9. See Joint Filler Depth Book

10. Longitudinal Joint Depth

11. Description of Mix

a. Workability

b. Slump

c. Mortar

d. Segregation

e. Bleeding

f. Time req. to harden



## COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Daviss County Kentucky

Owensboro-Hartford FA-125-F(2)S

Daily Observations

Date July 15, 1940

## 1. Weather

Temp. 8:15 a.m. 79°F. Cloudy  
3:00 p.m. 86°F. "Sun shining through clouds.  
Slight wind from Southwest.

## 12. Edging of Joints

No accumulation of mortar.  
No extra mortar used in finish.

## 2. Station Start

693+29.5 at 5:15 a.m.

## Station Stop

681+00.6 at 5:40 p.m.

## Lin. Ft.

1228.9 12 hr. 25 min.

## 13. Curing

a. One thickness burlap thoroughly wet during pour 7-15

b. Begin burlap

removal 5:00 a.m. 7-16

c. Burlap removed 684+20 at 8:15 a.m. 7-16

d. Pav. thoro. wet 684+50 at 8:15 a.m. 7-16

e. Paper in place 685+00 at 8:15 a.m. 7-16

f. Pav. thoro. wet all paper in place

9:30 a.m. 7-16

g. Curing complete all paper removed 9:00 a.m. } 7-19  
12:00 m.

## 3. See Daily Report

## 4. Temp. Conc. Final Finish (Broom)

9:00 (Tem. Conc. 82°F. 4:10 ( 92°F.  
a.m. (Tem. Air 79°F. p.m. ( 85°F.

## 5.

a.m.

p.m.

Time 9:40 11:10 2:00 3:30

Placing 689+20 687+70 685+00 683+35

Screeds 689+30 687+85 685+10 683+40

689+60 688+20 685+35 683+80

B-Float 689+70 688+30 685+40 684+00

690+40 688+70 685+90 684+50

Belt 690+45 688+90 686+00 684+60

Broom 691+00 689+20 686+10 685+00

B'lap 692+40 690+50 687+00 685+40

W-B'lap 692+40 690+50 687+50 685+40

12:15 p.m. 4:05 p.m.  
689+20 685+00

## 6. Condition of Subgrade

693+29.5 to 691+00 very spongy

691+00 681+00 O.K.

Sprinkled before paper placed.

691+00 to 692+30 scarified and  
allowed to dry all day 7-14-40.

## 14. Report on Construction Equipment.

No delays

## 15. Edges of Concrete

No honeycomb in pav. edges or  
lip curb.

## 16. Joint Sealing

All joints sealed 7-29.

## 7. Installation of Joints

690+20 3/4" Gap in Ex. Jt.

at C.L.

691+20 Cont. Jt. hit by B-Float, bad align.

691+40 " " " " " "

691+60 " " " " " "

Dowel holders O.K. throughout pour.

## 17. Pictures

---- Remarks ----

Beams 13, 14, 15 687+50 at 11:00 a.m.

P.R.A. Beam Sec. No. 4 -  
687+50 at 11:00 a.m.

## 8. Omit

## 9. See Joint Filler Depth Book

## 10. Longitudinal Joint Depth

Good alignment.

3/4"-7/8"-5/8"-5/8"

## 11. Description of Mix

a. Workability Plastic and Workable, uniform

b. Slump 1-1/2"

c. Mortar O.K. Good mortar roll on rear screed.

d. Segregation None

e. Bleeding Slight 5 spots

f. Time req. to harden Initial Set Placed at 687+70 - 11:10 a.m.

Hardened at " - 2:10 p.m.

3 hr.



## COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Davies County Kentucky

Owensboro-Hartford FA-125-F(2)S

Daily Observations

Date July 16, 1940

## 1. Weather

Temp. 8:15 a.m. 78°F. Cloudy  
 9:50 a.m. 68°F. Rain (Started)  
 11:00 a.m. 63°F. " (Stopped)  
 Slight Wind from North

## 12. Edging of Joints

No excess of mortar.  
 No extra mortar required.

2. Station Start 681+00.6 at 5:15 a.m.  
 Station Stop 676+39.6 at 10:00 am.  
 Lin. Ft. 461.0

13. Curing damp placed to  
 a. One thickness burlap ~~XXXXXXXXXX~~  
~~XXXXXXXXXX~~ 680+50 before rain, no  
 b. Begin burlap sprinkling.  
 removal 5:30 a.m. 7-17  
 c. Burlap removed 678+25 at 7:30 a.m. 7-17  
 d. Pav. thoro. wet 678+50 at 7:30 a.m. 7-17  
 e. Paper in place 679+00 at 7:30 a.m. 7-17  
 f. Pav. thoro. wet all paper in  
 place 9:45 a.m. 7-17  
 g. Curing complete all paper 7:30 a.m. }  
 removed 9:30 a.m. } 7-20

## 3. See Daily Report

## 4. Temp. Conc. Final Finish (Broom)

9:45 (T. Conc. 84°F.  
 a.m. (T. Air 70°F.

5.  
 Time 8:30 a.m.  
 Placing 677+80  
 Screeds 677+85  
 678+20  
 B-Float 678+40  
 678+85  
 Belt 678+90  
 Broom 680+60  
 B'lap None  
 W-B'lap None

## 14. Report on Construction Equipment.

No breakdowns.

## 6. Condition of Subgrade

Sprinkled before paper placed.  
 Firm and smooth.

## 15. Edges of Concrete

No honeycomb in pav. edges.  
 Few scattered spots in lip curb.

## 7. Installation of Joints

(Exp. Jt. Installed at 676+60  
 belonged at 676+80. Concrete  
 removed and Jt. moved to 676+80.  
 Installation O.K.  
 Dowel holders O.K.

## 17. Pictures

---- Remarks ----

No Beams or Cylinders made.  
 (Sec. 4 Completed at 6:30 a.m.  
 Sta. 680+00 Begin Sec. 3)

677+90 to 676+39.6 1:2 Mortar used  
 over entire surface to repair rain  
 damage.

681+00.6 to 677+90 1:2 Mortar used  
 in spots to repair rain damage.

681+00.6 to 679+00 1:2 Mortar used  
 over entire lip curb Right C.L. to  
 repair rain damage.

## 8. Omit

## 9. See Joint Filler Depth Book

## 10. Longitudinal Joint Depth

1/2"-5/8"-5/8"

## 11. Description of Mix

a. Workability O.K. (except 681+00 to 680+25)  
 b. Slump No test (Rain)  
 c. Mortar (Scales Out, Def. 681 to 680+25)  
 d. Segregation None O.K. Remainder)  
 e. Bleeding Slight in 5 spots.  
 f. Time req. to harden Final Set-No observation (Rain)



## COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Davies County Kentucky

Owensboro-Hartford FA-125-F(2)S

Daily Observations

Date July 17, 1940

## 1. Weather

Temp.

9:50 a.m. 78°F. Clear-Sun  
 2:30 p.m. 83°F. Clear-Sun  
 Moderate Wind from North.

## 12. Edging of Joints

No extra mortar required.

2. Station Start 676+39.6 at 7:30 a.m.  
 Station Stop 667+19.6 at 6:15 p.m.  
 Lin. Ft. Lin. Ft. 920.0

## 13. Curing

a. One thickness burlap thoroughly wet during pour 7-17b. Begin burlap removal 6:00 a.m. 7-18c. Burlap removed 669+00 at 7:45 a.m. 7-18d. Pav. thoro. wet 669+00 at 7:45 a.m. 7-18e. Paper in place 669+75 at 7:45 a.m. 7-18f. Pav. thoro. wet all paper in place 8:30 a.m. 7-18g. Curing complete all paper removed 4:00 a.m. 7-21  
7:30 a.m. 7-21

## 3. See Daily Report

## 4. Temp. Conc. Final Finish (Broom)

10:50 (T. Conc. 84°F. 2:30 (92°F.  
 a.m. (T. Air 79°F. p.m. (83°F.

	a.m.	p.m.
5. Time	10:15 11:25 1:35 2:35	
Placing	674+40 673+20 671+50 670+45	
Screeds	674+50 673+25 671+60 670+50	
	674+75 673+60 671+85 670+75	
B-Float	674+80 673+70 671+95 670+85	
	675+00 674+00 672+25 671+25	
Belt	675+05 674+15 672+30 671+30	
Broom	675+40 674+40 672+35 671+50	
B'lap	675+80 674+90 672+80 672+15	
W-B'lap	675+80 674+90 672+80 672+15	
	12:00 m. 2:50 p.m.	
	674+40 671+50	

## 6. Condition of Subgrade

Sprinkled before paper placed.  
 Uniform, and firm, planer cuts  
 good.

## 14. Report on Construction Equipment.

9:10 to 9:50 a.m. mixer stopped  
 (Crane) 674+75

## 15. Edges of Concrete

No honeycomb in pav. edges or  
 lip curb.

## 16. Joint Sealing

All joints sealed 8-22.

## 7. Installation of Joints

Exp. Jt. 672+80 O.K.  
 Exp. Jt. 668+80 O.K. (Picture)

17. Pictures (Mixer 668+60  
 1 to 12 (Exp. Jt. 668+80

---- Remarks ----

Beams 16,17,18 - 669+75 3:00 p.m.

P.R.A. Beam Sec. No. 3 - 669+75  
 3:00 p.m.

## 8. Omit

## 9. See Joint Filler Depth Book

## 10. Longitudinal Joint Depth

Good Alignment

1/2"-7/16"-3/8"-3/8"-3/8"

## 11. Description of Mix

a. Workability Plastic and Workable, uniform.b. Slump 1-1/2"c. Mortar O.K. Good mortar roll on rear screed.d. Segregation Nonee. Bleeding None a.m., slight at c.l. p.m.

f. Time req. to harden placed at 670+45 2:35 p.m.  
hardened at " 6:00 p.m.

3 hr. 25 min.



## COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Davies County Kentucky

Owensboro-Hartford FA-125-F(2)S

Daily Observations

Date July 18, 1940

## 1. Weather

Temp. 7:45 a.m. 74°F. Clear-Sun  
1:35 p.m. 88°F.  
 Numerous W. Clouds-Sun.  
 Slight wind from East.

## 12. Edging of Joints

O.K. no extra mortar required.

2. Station Start 667+19.6 at 5:05 a.m.  
 Station Stop 654+00.0 at 6:05 p.m.  
 Lin. Ft. Lin. Ft. 1319.6

## 13. Curing

a. One thickness burlap thoroughly wet during pour 7-18.b. Begin burlap removal 5:00 a.m. 7-19c. Burlap removed 658+00 at 8:00 a.m. 7-19d. Pav. thoro. wet 658+00 at 8:00 a.m. 7-19e. Paper in place 659+00 at 8:00 a.m. 7-19f. Pav. thoro. wet all paper in place 9:30 a.m. 7-19g. Curing complete all paper removed 5:40 a.m. 7-22  
6:00 a.m.)

## 3. See Daily Report

## 4. Temp. Conc. Final Finish (Broom)

10:45 (T. Conc. 88°F. 12:00 (90°F.  
a.m. (T. Air 82°F. m. (84°F.

5. Time	<u>10:20 a.m.</u>	<u>11:40 a.m.</u>
Placing	<u>662+00</u>	<u>660+60</u>
Screeds	<u>662+05</u>	<u>660+65</u>
	<u>662+35</u>	<u>661+00</u>
B-Float	<u>662+50</u>	<u>661+05</u>
	<u>662+80</u>	<u>661+30</u>
Belt	<u>663+10</u>	<u>661+70</u>
Broom	<u>663+35</u>	<u>662+00</u>
B'lap	<u>663+50</u>	<u>662+60</u>
W-B'lap	<u>664+00</u>	<u>662+80</u>
		<u>12:20 p.m.</u>
		<u>662+00</u>

## 6. Condition of Subgrade

Excellent, Firm, and uniform.

## 14. Report on Construction Equipment.

No delays.

## 15. Edges of Concrete

No honeycomb in pavement edges.  
 Slight honeycomb in lip curb.

## 7. Installation of Joints

Exp. Jt. O.K.

Cont. Jts. O.K. Finished

Width 5/8".

## 16. Joint Sealing

All joints sealed 8-22

17. Pictures (Mixer 663+00  
 12 to 22 (Finishing 663+00

---- Remarks ----

Beams 19, 20, 21 661+00 11:15 a.m.

## 8. Omit

## 9. See Joint Filler Depth Book

## 10. Longitudinal Joint Depth

3/8"-3/4"-11/16"-1/2"

## 11. Description of Mix

a. Workability Plastic and Workable, uniform.b. Slump 1-1/2"c. Mortar O.K. uniform roll on rear screed.d. Segregation Nonee. Bleeding Slight near edges a.m.; none p.m.

f. Time req. to harden



## COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Davies County Kentucky

Owensboro-Hartford - FA-125-F(2)S

Daily Observations

Date July 19, 1940

## 1. Weather

Temp. 8:00 a.m. 80°F. Clear-Sun  
 1:45 p.m. 88°F. Clear  
 Few W. Clouds - Sun.  
 Moderate wind from S.W.

## 12. Edging of Joints

Joints edging good, no extra  
 mortar or water required.

2. Station Start 654+00.0 at 4:55 a.m.  
 Station Stop 640+99.7 at 6:00 p.m.  
 Lin. Ft. Lin. Ft. 1300.3

## 13. Curing

a. One thickness burlap thoroughly wet  
 during pour 7-19

b. Begin burlap  
 removal 5:00 a.m. 7-20

c. Burlap removed 641+80 at 10:00 a.m. 7-20

d. Pav. thoro. wet 641+80 at 10:00 a.m. 7-20

e. Paper in place 642+00 at 10:00 a.m. 7-20

f. Pav. thoro. wet all paper in  
 place 10:20 a.m. 7-20

g. Curing complete all paper  
 removed 9:45 a.m.) 7-23  
12:30 p.m.)

## 3. See Daily Report

## 4. Temp. Conc. Final Finish (Broom)

9:55 (T. Conc. Pl. 88° 1:25 (92°  
 a.m. " " F. Fin. 88° p.m. (94°  
 (T. Air 82° (88°

5.	a.m.	p.m.
Time	9:55 10:50 1:10 2:30	
Placing	649+00 648+15 645+80 644+50	
Screeds	649+05 648+25 646+85 644+55	
	649+40 648+50 646+15 644+70	
B-Float	649+50 648+55 646+30 644+80	
	650+00 648+30 646+65 645+25	
Belt	650+40 648+95 646+75 645+75	
Broom	650+42 649+00 646+80 645+80	
B'lap	651+45 650+40 647+75 646+20	
W-B'lap	651+45 650+75 647+75 646+20	
	11:40 a.m. 2:50 p.m.	
	643+00 645+80	

## 6. Condition of Subgrade

Soft spot entire area Left C.L.  
 647+20 to 647+60  
 Soft and spongy entire width pav.  
 644+30 to 647+20

Remainder spongy spots.

## 14. Report on Construction Equipment.

No delays.

Water device on mixer checked, found  
 to deliver 160.5# at 160.8# and  
 170# at 170#.

## 15. Edges of Concrete

No honeycomb in pav. edges or  
 lip curb.

## 16. Joint Sealing

All joints sealed 8-22.

## 7. Installation of Joints

Exp. Jt. 648+80 O.K.

## 17. Pictures

----- Remarks -----

Beams 22,23,24 - 647+00 12:15 p.m.

## 8. Omit

## 9. See Joint Filler Depth Book

## 10. Longitudinal Joint Depth

11/16" - 1/2"

## 11. Description of Mix

a. Workability Plastic and Workable, Uniform.

b. Slump 1-7/8"

c. Mortar No excess, uniform roll on rear screed.

d. Segregation None

e. Bleeding Slight Spots.

f. Time req. to harden



## COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Daviness County Kentucky

Owensboro-Hartford FA-125-F(2)S

Daily Observations

Date July 20, 1940

## 1. Weather

Temp.

9:00 a.m. 85°F. Clear-Sun  
3:00 p.m. 93°F. " "

Moderate wind from S.W. All Day.

## 12. Edging of Joints

Joint edging O.K. No extra mortar or water required to finish.

## 2. Station Start

640+99.7 at 5:10 a.m.

Station Stop

629+29.6 at 5:45 p.m.

Lin. Ft.

Lin. Ft. 1170.1

## 13. Curing

a. One thickness burlap thoroughly wet during pour 7-20

b. Begin burlap

removal

4:40 a.m. 7-21

c. Burlap removed

630+00 7:55 a.m. 7-21

d. Pav. thoro. wet

631+00 7:55 a.m. 7-21

e. Paper in place

635+00 7:55 a.m. 7-21

f. Pav. thoro. wet all paper in

place

10:00 a.m. 7-21

g. Curing complete all paper

removed

10:00 a.m.

1:30 p.m. 7-24

## 3. See Daily Report

## 4. Temp. Conc. Final Finish (Broom)

(T. Conc. Pl. 91° 5:00 (92°  
9:35 (T. " F. Fin. 91° p.m. (92°  
a.m. (T. Air 87° (89°

## 5.

Time	9:20 a.m.	10:30 a.m.
Placing	637+00	635+85
Screeds	637+10	635+95
	637+35	636+20
B-Float	637+40	636+25
	637+65	636+60
Belt	637+68	636+90
Broom	638+40	637+00
B'lap	639+30	637+70
W-B'lap	639+75	637+70
		11:10
		637+70

## 6. Condition of Subgrade

632 to 632+30 Very Spongy, planer out uniform. Spongy spots throughout, uniform cut behind planer.

## 14. Report on Construction Equipment.

O.K. No delays.

## 15. Edges of Concrete

No honeycomb in edges of pav. Slight honeycomb in lip curb.

## 7. Installation of Joints

Exp. Jt. 632+80 O.K.

Cont. Jt. Width 3/4" Finished, good line.

## 16. Joint Sealing

All joints sealed 8-22.

## 17. Pictures

---- Remarks ----

Beams 25, 26, 27 634+00 12:15 p.m.

P.R.A. Beam Sec. No. 2-634+00 12:15 p.m.

Finished Sec. 2 at 630+00 4:45 p.m.

Begin Std. Sec. at 630+00 4:45 p.m.

## 8. Omit

## 9. See Joint Filler Depth Book

## 10. Longitudinal Joint Depth

Alignment O.K.

9/16"-3/8"-3/8"-3/8"-7/16"-1/2"

## 11. Description of Mix

a. Workability Plastic and Workable, uniform.

b. Slump 1-7/8"

c. Mortar O.K. Good mortar roll on rear screed.

d. Segregation None

e. Bleeding Slight spots at C.L. a.m., none p.m.

f. Time req. to harden



# COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Daviess County Kentucky

Owensboro-Hartford, FA-125-F(2)S.

Daily Observations

Date July 21, 1940 (Sun.)

1. Weather

Temp. \_\_\_\_\_

12. Edging of Joints

7:25 a.m. 76°F. Alt. Cloudy & Sun  
(7:15 a.m. to 7:25 a.m. Light Rain)  
3:00 p.m. 88°F. Clear-Sun.  
No Wind.

2. Station Start \_\_\_\_\_

Station Stop \_\_\_\_\_

Lin. Ft. \_\_\_\_\_

13. Curing

a. One thickness burlap thoroughly wet during pour \_\_\_\_\_

b. Begin burlap removal \_\_\_\_\_

c. Burlap removed \_\_\_\_\_

d. Pav. thoro. wet \_\_\_\_\_

e. Paper in place \_\_\_\_\_

f. Pav. thoro. wet all paper in place \_\_\_\_\_

g. Curing complete all paper removed \_\_\_\_\_

3. See Daily Report

4. Temp. Conc. Final Finish (Broom)

5.

Time \_\_\_\_\_

Placing \_\_\_\_\_

Screeds \_\_\_\_\_

B-Float \_\_\_\_\_

Belt \_\_\_\_\_

Broom \_\_\_\_\_

B'lap \_\_\_\_\_

W-B'lap \_\_\_\_\_

14. Report on Construction Equipment.

6. Condition of Subgrade

15. Edges of Concrete

16. Joint Sealing

7. Installation of Joints

17. Pictures

----- Remarks -----

8. Omit

9. See Joint Filler Depth Book

10. Longitudinal Joint Depth

11. Description of Mix

a. Workability \_\_\_\_\_

b. Slump \_\_\_\_\_

c. Mortar \_\_\_\_\_

d. Segregation \_\_\_\_\_

e. Bleeding \_\_\_\_\_

f. Time req. to harden \_\_\_\_\_



## COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Davies County Kentucky

Owensboro-Hartford, FA-125-F(2)S

Daily Observations

Date July 22, 1940

## 1. Weather

Temp.

9:00 a.m. 88°F. Clear-Sun  
 12:25 p.m. 94°F. " "  
 3:00 p.m. 93°F. " Alt. Cloudy  
 and Sun.

Moderate wind from S.W. All Day.

2. Station Start 620+29.6 at 5:00 am.Station Stop 620+10.0 at 6:00 pm.Lin. Ft. 919.6 (10 hr. 30 min. Breakdown)

## 3. See Daily Report

## 4. Temp. Conc. Final Finish (Broom) p.m.

11:40 (T. Conc. 95°F. 1:15 (97° 3:30  
 a.m. (T. Air 90°F. p.m. (95° 98°  
 91°

5. Time 11:20 12:50 3:45 5:20  
 Placing 626+10 624+80 622+00 620+80  
 Screeds 626+20 624+90 622+12 620+85  
626+50 625+20 622+36 621+00  
 B-Float 626+55 625+30 622+42 621+10  
626+75 625+65 622+62 621+30  
 Belt 626+80 625+65 622+90 621+30  
 Broom 627+10 626+10 623+20 622+00  
 B'lap 627+70 626+30 623+80 622+45  
 W-B'lap 627+70 626+30 623+80 622+45  
1:00 p.m. 5:45 p.m.  
626+10 622+00

## 6. Condition of Subgrade

624+00 to 628+25 Spongy Spots.  
 Uniform cut behind planer.  
 Remainder of subgrade fair and  
 uniform cut behind planer.  
 This days pour thru shale cut.

## 7. Installation of Joints

Dowel holders O.K.  
 Alignment and construction  
 of Joints O.K.

## 12. Edging of Joints

Joint edging good, no extra mortar  
 or water required.

## 13. Curing

- a. One thickness burlap thoroughly wet  
 during pour 7-22  
 b. Begin burlap  
 removal 5:00 a.m. 7-23  
 c. Burlap removed 620+50 at 8:55 a.m. 7-23  
 d. Pav. thoro. wet 621+70 at 8:55 a.m. 7-23  
 e. Paper in place 621+80 at 8:55 a.m. 7-23  
 f. Pav. thoro. wet all paper in  
 place 9:30 a.m. 7-23  
 g. Curing complete all paper  
 removed 8:00 a.m. 7-26  
10:30 a.m. 7-26

## 14. Report on Construction Equipment.

Placing concrete stopped from 5:45 a.m.  
 to 8:30 a.m. due to broken cable on  
 skip. Conc. Pl. 628 to +50.

## 15. Edges of Concrete

Spots of honeycomb in pav. edge at  
 620+40 Lt. of C.L., remainder of pav.  
 edge O.K. Lip curb slight spots of  
 honeycomb throughout.

## 16. Joint Sealing

All joints sealed 8-23.

17. Pictures (Removing paper  
23 & 24 (657+00 to 655.

---- Remarks ----

Beams 28, 29, 30 620+50 5:00 p.m.

## 8. Omit

## 9. See Joint Filler Depth Book

## 10. Longitudinal Joint Depth

Longitudinal Jt. Alignment O.K.  
 9/16"-1 5/16"-7/16"-1/2"-1/2"

L. Spot

## 11. Description of Mix

- a. Workability Plastic and Workable, Uniform.  
 b. Slump 1"  
 c. Mortar O.K. Good mortar roll on rear screed.  
 d. Segregation None  
 e. Bleeding Slight bleeding near C.L. a.m. & p.m.  
 f. Time req. to harden



## COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Daviss County Kentucky

Owensboro-Hartford FA-125-F(2)S

Daily Observations

Date July 23, 1940

## 1. Weather

Temp.

9:00 a.m. 89°F. Clear-Sun  
 12:00 m. 94°F. Alt. Clouds & Sun  
 3:00 p.m. 92°F. " " "

No Wind, Section thru Wooded Area.

## 12. Edging of Joints

Good, no extra mortar or water required to finish.

2. Station Start 620+10.0 at 5:00 a.m.Station Stop 610+82.0 (End Bridge)Lin. Ft. 928.0 at 5:40 pm.

## 13. Curing

a. One thickness burlap thoroughly wet during pour 7-23b. Begin burlap removal 5:30 a.m. 7-24c. Burlap removed 610+82 at 8:00 a.m. 7-24d. Pav. thoro. wet 610+82 at 8:00 a.m. 7-24e. Paper in place None at 8:00 a.m. 7-24f. Pav. thoro. wet all paper in place 10:00 a.m. 7-24g. Curing complete all paper removed 8:30 a.m. 7-27  
11:30 a.m.

\*No paper in place at 8:00 due to difficulty in carrying forms ahead.

## 3. See Daily Report

## 4. Temp. Conc. Final Finish (Broom)

9:55 (T. Conc. 92°F. 1:30 (98°F.  
 a.m. (T. Air 90°F. p.m. (90°F.

5. Time	9:20 a.m.	11:10 a.m.
Placing	616+00	614+20
Screeds	616+05	614+30
	616+25	614+50
B-Float	616+30	614+60
	616+50	614+80
Belt	617+25	614+80
Broom	617+70	616+00
B'lap	618+80	616+00
W-B'lap	619+00	616+40
		11:20 a.m.
		616+00

## 6. Condition of Subgrade

Good, uniform cut behind planer throughout pour.

## 14. Report on Construction Equipment.

Finishing machine down from 9:20 a.m. to 9:35, paver stopped during this time. Placing Conc. Stopped 1:30 p.m. to 2:00 p.m., out of steel.

## 15. Edges of Concrete

No lip curb on this pour.  
 Slight honeycomb spots, scattered throughout on both sides of C.L.

## 16. Joint Sealing

All joints sealed 8-23.

## 7. Installation of Joints

Installation of Exp. & Cont. Joints O.K. Finished Exp. & Cont. Jts. slightly crooked. LaGlede dowel holders omitted from Exp. Jt. 611+02 due to length of bridge approach slab steel.

## 17. Pictures

---- Remarks ----

Beams 31, 32, 33 611+50 at 2:45 p.m.

Hard rain 3:30 p.m. to 4:15 p.m.  
 Placing stopped 3:30 p.m. to 4:45 p.m. - rain. Placing started 4:45 p.m. bridge approach slab poured 610+82 to 611+02, completed 5:30 p.m. Pavement 611+75 to 620+10 covered with burlap before rain, good condition. Pavement 611+02 to 611+32 very wet concrete due to rain.

Tem. Air at 6:00 p.m. 80°F.

## 8. Omit

## 9. See Joint Filler Depth Book

## 10. Longitudinal Joint Depth

9/16"-7/16"-7/16"-7/16"

## 11. Description of Mix

a. Workability Plastic and Workable, Uniform.b. Slump 1-7/8"c. Mortar O.K., uniform mortar roll rear screed.d. Segregation Nonee. Bleeding Slight near C.L. a.m. & p.m.

f. Time req. to harden



COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Daviess County Kentucky

Owensboro-Hartford FA-125-F(2)S

Daily Observations

Date July 24, 1940

1. Weather  
Temp.

9:00 a.m. 84°F. Cloudy  
12:00 m. 92°F. Alt. Clouds & Sun  
3:00 p.m. 77°F. Cloudy  
No Wind, Hard rain, 2:30 p.m.  
to 2:50 p.m. at 8:25 a.m.

2. Station Start 609+16.6 (End Bridge)  
Station Stop 604+73.0 at 3:00 p.m.  
Lin. Ft. 443.6

3. See Daily Report

4. Temp. Conc. Final Finish (Broom)

5.  
Time 2:10 p.m.  
Placing 605+30  
Screeds 605+40  
605+70  
B-Float 605+75  
606+05  
Belt 606+30  
Broom 606+40  
B'lap 606+85  
W-B'lap 606+85

6. Condition of Subgrade

Moist and firm, uniform cut  
behind planer.

7. Installation of Joints

Installation of Exp. & Cont.  
Joints O.K.  
Dowel Holders O.K.

12. Edging of Joints

Joints edging good, no extra mortar  
or water required to finish

13. Curing

a. One thickness burlap thoroughly wet  
during pour 7-24  
b. Begin burlap  
removal 5:30 a.m. 7-25  
c. Burlap removed 604+73.0 at 7:00 a.m. 7-25  
d. Pav. thoro. wet 604+73.0 at 7:30 a.m. 7-25  
e. Paper in place None at 7:30 7-25  
f. Pav. thoro. wet all paper in  
place 9:00 a.m. 7-25  
g. Curing complete all paper  
removed 6:00 a.m. 7-29  
9:00 a.m.)

14. Report on Construction Equipment.

No Delays.

15. Edges of Concrete

No lip curb on this Section  
Pavement edges O.K.

16. Joint Sealing

All joints sealed 8-23

17. Pictures

---- Remarks ----

No Beams.

8. Omit

9. See Joint Filler Depth Book

10. Longitudinal Joint Depth

1/2"-7/16"-9/16"-3/8"

11. Description of Mix

a. Workability Plastic and Workable, Uniform.  
b. Slump No test.  
c. Mortar O.K. Good mortar roll rear screed.  
d. Segregation None  
e. Bleeding Slight, near C.L. a.m. & p.m.  
f. Time req. to harden



## COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Davies County Kentucky

Owensboro-Hartford FA-125-F(2)S

Daily Observations

Date July 25, 19401. Weather  
Temp.

9:00 a.m. 89°F. Clear-Sun  
12:00 m. 93°F. Alt. Clouds & Sun  
3:00 p.m. 92°F. Clear-Sun  
Slight wind from S.W.

## 12. Edging of Joints

Joints edging O.K.; no extra water or mortar required.

New 1/8" radius edging tool on project.

2. Station Star 604+73.0 at 7:15 am.  
Station Stop 602+99.5 at 10:15 am.  
~~xxxxx~~ 601+14.5 at 11:00 am.  
Bridge End 596+66.0 at 6:00 pm.

## 13. Curing

a. One thickness burlap thoroughly wet during pour 7-25b. Begin burlap removal 5:30 a.m. 7-26.c. Burlap removed 596+66.0 at 7:00 a.m. 7-26d. Pav. thoro. wet 596+66.0 at 7:00 a.m. 7-26e. Paper in place None at 7:00 a.m. 7-26f. Pav. thoro. wet all paper in place 8:30 a.m. 7-26g. Curing complete all paper removed 6:00 a.m. 7-29  
9:00 a.m. 7-29

## 3. See Daily Report

## 4. Temp. Conc. Final Finish (Broom)

11:30 (T. Conc. 98° 3:00 (100° (98°  
a.m. (T. Air 94° p.m. (92° (89°

Time	2:30 p.m.	4:15 p.m.
Placing	599+00	597+40
Screeds	599+10	597+50
	599+35	597+80
B-Float	599+50	597+90
	599+70	598+30
Belt	599+75	598+40
Broom	600+35	599+00
B'lap	600+90	599+45
W-B'lap	600+90	599+45
		4:35 p.m.
		599+00

## 6. Condition of Subgrade

Bridge approach slab 602+99.5 to 603+49.5 subgrade very spongy and nonuniform. Remainder of subgrade firm and uniform.

## 14. Report on Construction Equipment.

No delays.

## 15. Edges of Concrete

No lip curb on this section.  
No honeycomb in pav. edges.

## 7. Installation of Joints

Joint Installation O.K.  
Dowel Holders O.K.

## 16. Joint Sealing

All joints sealed 8-23

## 17. Pictures

---- Remarks ----

Beams 34,35,36 600+40 at 12:30 p.m.

10:15 a.m. to 11:00 a.m. equipment crossing bridge.

## 8. Omit

## 9. See Joint Filler Depth Book

## 10. Longitudinal Joint Depth

Splice at Joint ends wired-begin today. 7/16"-1/2"-3/8"-7/16"

## 11. Description of Mix

a. Workability Plastic & Workable, Uniformb. Slump 2"c. Mortar O.K. good mortar roll on rear screed.d. Segregation Nonee. Bleeding Slight bleeding over entire surface a.m.f. Time req. to harden and p.m.



## COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Daviness County Kentucky

Owensboro-Hartford FA-125-F(2)S

Daily Observations

Date July 26, 1940

## 1. Weather

Temp. 9:00 a.m. 89°F. Clear-Sun  
 12:00 m. 91°F. " "  
 3:00 p.m. 94°F. " "  
 No wind.

## 12. Edging of Joints

593+00 to 595+01 difficulty in  
 edging joints due to delay in  
 getting equip. through bridge.  
 Remainder of Joints O.K.

(Bridge End)

2. Station Start (595+01.0 at 5:05 a.m.)  
 Station Stop (588+26.0 at 4:00 p.m.)  
 " " (586+61.0 at 5:00 p.m.)  
 " " (585+81.0 at 7:05 p.m.)  
 Lin. Ft. 590.0

## 13. Curing

a. One thickness burlap thoroughly wet  
 during pour 7-26  
 b. Begin burlap  
 removal 5:00 a.m. 7-27  
 c. Burlap removed 585+81.0 at 6:30 a.m. 7-27  
 d. Pav. thoro. wet 585+81.0 at 6:30 a.m. 7-27  
 e. Paper in place None at 6:30 a.m. 7-27  
 f. Pav. thoro. wet all paper in  
 place 9:00 a.m. 7-27  
 g. Curing complete all paper  
 removed 5:30 a.m. 7-30  
7:00 a.m. 7-30

## 3. See Daily Report

## 4. Temp. Conc. Final Finish (Broom)

10:15 (T. Conc. 93° 2:30 (96°  
 a.m. (T. Air 90° p.m. (94°

## 5.

Time	9:35 a.m.	11:05 a.m.
Placing	592+20	591+09
Screeds	592+30	591+15
	592+75	591+35
B-Float	592+85	591+40
	593+15	591+75
Belt	593+70	592+05
Broom	594+40	592+20
B'lap	None	592+40
W-B'lap	None	592+40
		11:20 a.m.
		592+20

## 14. Report on Construction Equipment.

No delays.

## 6. Condition of Subgrade

(594+51.0 to 595+01.0 brdg. appr.  
 Subgrade uniform and firm.) (588+26  
 to 594+51.0 Subgrade, spongy, non-  
 uniform and rutted.) (585+81.0 to  
 586+61.0 Subgrade, very spongy and  
 nonuniform, paver run on boards,  
 grade leveled and tamped.)

## 15. Edges of Concrete

No lip curb on this section.  
 Slight honeycomb in pavement edges.

## 7. Installation of Joints

All Joint Installations O.K.  
 All dowel holders O.K.

## 16. Joint Sealing

All joints sealed 8-24.

## 17. Pictures

---- Remarks ----

Beams 37, 38, 39 591+50 at 10:30 a.m.  
 P.R.A. Sec. Std. 591+50 at 10: a.m.

## 8. Omit

## 9. See Joint Filler Depth Book

## 10. Longitudinal Joint Depth

Good Alignment  
 3/8"-9/16"-1/2"-7/16"

## 11. Description of Mix

a. Workability Plastic & Workable, Uniform.  
 b. Slump 1-3/4"  
 c. Mortar O.K.  
 d. Segregation None  
 e. Bleeding None  
 f. Time req. to harden \_\_\_\_\_



COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Daviess County Kentucky

Owensboro-Hartford FA-125-F(2)S

Daily Observations

Date July 27, 1940

1. Weather

Temp. 9:00 a.m. 86°F. Clear  
12:00 m.  
3:00 p.m. 96°F. Clear-Sun  
Slight wind from Southwest.

12. Edging of Joints

No extra water or mortar required, edging O.K.

2. Station Start 585+81.0 at 5:00 a.m.  
 Station Stop 582+67.0 Brdg. End  
" Lin. Ft. " 581+02.0 "  
" Lin. Ft. " 579+02.0 at 3:15 p.m.  
Lin. Ft. 514.0

13. Curing

a. One thickness burlap thoroughly wet during pour 7-27  
 b. Begin burlap removal 3:00 a.m. 7-28  
 c. Burlap removed \_\_\_\_\_  
 d. Pav. thoro. wet \_\_\_\_\_  
 e. Paper in place \_\_\_\_\_  
 f. Pav. thoro. wet all paper in place 5:45 a.m. 7-28  
 g. Curing complete all paper removed 8:00 a.m. 7-31  
10:00 a.m. 7-31

3. See Daily Report

4. Temp. Conc. Final Finish (Broom)

5. Time \_\_\_\_\_  
 Placing \_\_\_\_\_  
 Screeds \_\_\_\_\_  
 B-Float \_\_\_\_\_  
 Belt \_\_\_\_\_  
 Broom \_\_\_\_\_  
 B'lap \_\_\_\_\_  
 W-B'lap \_\_\_\_\_

14. Report on Construction Equipment.

No delays.

6. Condition of Subgrade

584+17.0 to 585+81.0 Subgrade very spongy and nonuniform, paver run on boards, grade leveled and tamped.  
582+67.0 to 584+17.0 Subgrade firm and uniform. 580+52.0 to 581+02.0 Subgrade spongy and nonuniform, grade leveled and tamped behind paver.  
579+02.0 to 580+52 Subgrade firm and uniform.

15. Edges of Concrete

No honeycomb in pavement edges.

16. Joint Sealing

All joints sealed 8-24.

17. Pictures

All Joint Installations O.K.

All Dowel Holders O.K.

---- Remarks ----

Beams 40,41,42 579+50 at 3:00 p.m.

8. Omit

9. See Joint Filler Depth Book

10. Longitudinal Joint Depth

Good Alignment

3/4"-1/2"-5/8"-7/16"-1/2"

11. Description of Mix

a. Workability Plastic and workable.  
 b. Slump 2"  
 c. Mortar Sufficient  
 d. Segregation None  
 e. Bleeding None a.m. or p.m.  
 f. Time req. to harden \_\_\_\_\_



# COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Daviess County Kentucky

Owensboro-Hartford FA-125-F(2)S

Daily Observations

Date July 28, 1940 (Sun.)

1. Weather

Temp.

9:00 a.m. 88°F. Clear-Sun  
12:00 m. " "  
3:00 p.m. 96°F.

12. Edging of Joints

2. Station Start

Station Stop

Lin. Ft.

13. Curing

a. One thickness burlap thoroughly wet during pour

b. Begin burlap removal

c. Burlap removed

d. Pav. thoro. wet

e. Paper in place

f. Pav. thoro. wet all paper in place

g. Curing complete all paper removed

3. See Daily Report

4. Temp. Conc. Final Finish (Broom)

5.

Time

Placing

Screeds

B-Float

Belt

Broom

B'lap

W-B'lap

14. Report on Construction Equipment.

6. Condition of Subgrade

15. Edges of Concrete

16. Joint Sealing

7. Installation of Joints

17. Pictures

----- Remarks -----

8. Omit

9. See Joint Filler Depth Book

10. Longitudinal Joint Depth

11. Description of Mix

a. Workability

b. Slump

c. Mortar

d. Segregation

e. Bleeding

f. Time req. to harden



## COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Daviss County Kentucky

Owensboro-Hartford FA-125-F(2)S

Daily Observations

Date July 29, 1940

## 1. Weather

Temp.

9:00 a.m. 91°F. Clear-Sun  
 12:00 m. 97°F. " "  
 3:00 p.m. 97°F. " "

Moderate wind from Southwest.

## 12. Edging of Joints

Joint edging O.K., no extra mortar  
 or water required.

2. Station Start 579+02.0 at 5:15 a.m.  
 Station Stop 568+00.5 at 6:00 p.m.  
 Lin. Ft. 1101.5 11 hr. 45 min.

## 13. Curing

a. One thickness burlap thoroughly wet  
 during pour 7-29

b. Begin burlap

removal 5:00 a.m. 7-30c. Burlap removed 568+00.5 at 6:30 a.m. 7-30d. Pav. thoro. wet 568+00 at 8:00 a.m. 7-30e. Paper in place 572+00.0 at 8:00 a.m. 7-30f. Pav. thoro. wet all paper in  
place 8:50 a.m. 7-30g. Curing complete all paper  
removed 5:00 a.m.) 8-2  
9:00 a.m.)

## 3. See Daily Report

## 4. Temp. Conc. Final Finish (Broom)

10:30 (T. Conc. 96° 3:00 (101° 4:30 (100°  
 a.m. (T. Air 94° p.m. ( 97° p.m. (93°

5. a.m. p.m.  
 Time 10:10 11:30 2:45 4:10

Placing 574+10 573+10 571+00 569+55Screeds 574+15 573+15 571+05 569+65574+45 573+50 571+25 570+00B-Float 574+60 573+60 571+65 570+10575+00 573+90 571+85 570+30Belt 575+20 574+00 571+90 570+35Broom 575+60 574+10 572+30 571+00B'lap 575+90 574+50 572+50 571+15W-B'lap 575+90 574+50 572+50 571+1511:554:20 p.m.574+10571+00

## 14. Report on Construction Equipment.

12:00 m. to 1:00 p.m. mixer shut  
 down, cable broke.

## 15. Edges of Concrete

No Lip Curb on this section.  
 4 slight honeycomb spots in  
 pavement edge.

## 16. Joint Sealing

All joints sealed 8-24.

## 17. Pictures

---- Remarks ----

Beams 43, 44, 45 567+50 at 5:00 p.m.

12:00 m. to 1:00 p.m. paver stopped,  
 no bulkhead placed. Concrete in  
 front covered with wet burlap,  
 condition O.K. at start.

## 8. Omit

## 9. See Joint Filler Depth Book

## 10. Longitudinal Joint Depth

Good Alignment

3/8"-3/8"-9/16"-7/16"-3/8"-3/8"

## 11. Description of Mix

a. Workability Plastic and Workable, Uniformb. Slump 1-3/8"c. Mortar O.K. Good mortar roll on rear screed.d. Segregation Nonee. Bleeding Very slight a.m. and p.m.f. Time req. to harden placed at 573+10-11:30 a.m.hardened " "3:45 p.m.4 hr. 15 min.



COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Daviess County Kentucky

Owensboro-Hartford FA-125-F(2)S

Daily Observations

Date July 30, 1940

1. Weather

Temp. 9:00 a.m. 91°F. Clear-Sun  
12:00m. 97°F. " "  
3:00 p.m. 82°F. Cloudy-No Sun  
Moderate wind from West.

12. Edging of Joints

Edging O.K. No extra mortar or water required.

2. Station Start 568+00.5 at 5:00a.m.  
Station Stop 557+60.3 at 5:50 p.m.  
Lin. Ft. 1040.2

13. Curing

- a. One thickness burlap thoroughly wet during pour 7-30  
b. Begin burlap removal 5:00 a.m. 7-31  
c. Burlap removed 562+00 at 5:30 a.m. 7-31  
d. Pav. thoro. wet 562+00 at 5:30 a.m. 7-31  
e. Paper in place 562+00 at 6:15 a.m. 7-31  
f. Pav. thoro. wet all paper in place 8:00 a.m. 7-31  
g. Curing complete all paper removed 5:00 a.m. 8-3  
8:00 a.m.

3. See Daily Report

4. Temp. Conc. Final Finish (Broom)

8:30 (T. Con. 90° 12:30 (101° 4:30 (94°  
a.m. (T. Air 89° p.m. (98° p.m. (84°

	a.m.	p.m.
Time	11:25 12:40	3:50 5:50
Placing	563+40 562+30	559+60 557+60.3
Screeds	563+50 562+40	559+65 557+65
	563+70 562+80	560+00 558+20
B-Float	563+75 562+90	560+10 558+60
	563+95 563+05	560+40 559+00
Belt	564+45 563+08	560+45 559+10
Broom	564+55 563+40	561+00 559+60
B'lap	564+70 563+65	561+10 560+00
W-B'lap	564+70 563+65	561+25 560+00
	1:00 p.m. 6:20 p.m.	
	563+40	559+60

14. Report on Construction Equip.

8:50 a.m. to 9:40 a.m. paver stopped, water device broken.

6. Condition of Subgrade

567+80 to 568+00.5 Soft and spongy, width of pavement leveled and tamped behind paver. 560+45 to 560+70 soft and spongy right C.L. 558+00 to 559+70 soft and spongy entire width pavement, leveled and tamped behind paver. Remainder O.K.

15. Edges of Concrete

No lip curb on this section. 7 slight honeycomb spots in pavement edge.

7. Installation of Joints

Cont. Jt. 560+00 first joint in direction of pour without dowels.

17. Pictures

Std. Load transference installed in Const. Joint at 557+60.3

---- Remarks ----

Beams 46, 47, 48 559+00 at 4:20 p.m.

Finished Std. Sec. 3:15 p.m.  
Started on Sec. No. 1

Wire mesh and load transference bars stopped 560+00

8. Omit

9. See Joint Filler Depth Book

10. Longitudinal Joint Depth

Good Alignment  
3/8"-3/8"-7/16"-7/16"-9/16"-1/2"

11. Description of Mix

- a. Workability Plastic and Workable, uniform.  
b. Slump 2-1/2"  
c. Mortar O.K. good mortar roll on rear screed.  
d. Segregation None  
e. Bleeding Excess bleeding 560+00 to 560+50-Wet Concrete  
f. Time req. to harden Placed at 562+30 - 12:40 p.m.  
hardened " " - 5:00 p.m.  
4 hr. 20 min.



## COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Daviss County Kentucky

Qwensboro-Hartford FA-125-F(2)S

Daily Observations

Date July 31, 1940

## 1. Weather

Temp. 9:00 a.m. 84°F. Alt. Cloudy-Sun.12:00 m. 94°F. Clear-Sun3:00 p.m. 96°F. " "Moderate wind from Southwest.

## 12. Edging of Joints

O.K. No extra mortar or water required.2. Station Start 557+60.3 at 5:10 a.m.Station Stop 546+31.8 at 6:00 p.m.Lin. Ft. 1128.5

## 13. Curing

a. One thickness burlap thoroughly wet during pour 7-31b. Begin burlap removal 5:00 a.m. 8-1c. Burlap removed 546+31.8 at 6:30 a.m. 8-1d. Pav. thoro. wet 550+00 at 7:45 a.m. 8-1e. Paper in place 551+30 at 7:45 a.m. 8-1f. Pav. thoro. wet all paper in place 9:30 a.m. 8-1g. Curing complete all paper removed 5:00 a.m. 8-5  
7:00 a.m. 8-5

## 3. See Daily Report

## 4. Temp. Conc. Final Finish (Broom)

10:00 (T. Con. 92° 12:00 (96° 3:45 (99°  
a.m. (T. Air 88° m. (94° p.m. (97°5. 

	a.m.		p.m.	
Time	<u>9:05</u>	<u>10:40</u>	<u>3:30</u>	<u>5:00</u>

Placing 553+90 552+30 547+85 547+10Screeds 553+95 552+35 547+90 547+15554+35 552+65 548+20 547+30B-Float 554+50 552+75 548+30 547+30554+70 552+90 548+60 547+50Belt 554+75 553+35 548+70 547+60Broom 555+80 553+90 549+00 547+85B'lap 556+00 554+20 549+60 548+30W-B'lap 556+00 554+20 549+60 548+3011:00 a.m. 5:10 p.m.553+90 547+85

## 6. Condition of Subgrade

Sprinkled in front of paver.  
Subgrade throughout pour firm  
and uniform, uniform cut behind  
paver.

## 14. Report on Construction Equipment.

No delays.

## 15. Edges of Concrete

No honeycomb in pav. edges.  
Slight honeycomb in lip curb.

## 7. Installation of Joints

Contraction Joint Cutter out of  
alignment 557+00 to 552, result-  
ing in crooked joints. Cutter  
straightened, contraction joints  
552 to 546 O.K. No load trans-  
ference bars used in contraction  
joints. Standard Load Transference  
Installed in Construction Joint  
at 546+31.8.

## 16. Joint Sealing

All joints sealed 8-24

## 17. Pictures

---- Remarks ----

Beams 49,50,51 547+00 at 3:45 p.m.Paver stopped 11:30 a.m. to 11:45,  
waiting on information concerning  
Wye Construction.Butt joint between Wye and pavement,  
no recess joint or tie bars.

## 8. Omit

Paver stopped 4:30 p.m. to 4:45 p.m.  
truck delay.

## 9. See Joint Filler Depth Book

## 10. Longitudinal Joint Depth

Good Alignment7/16"-7/16" 1/2"-9/16"-1/2"

## 11. Description of Mix

a. Workability Plastic & Workable, uniform.b. Slump 1-1/2"c. Mortar O.K. Good mortar roll on rear screed.d. Segregation Nonee. Bleeding None a.m. or p.m.

f. Time req. to harden \_\_\_\_\_



## COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Davies County Kentucky

Owensboro-Hartford FA-125-F(2)S

Daily Observations

Date August 1, 1940

## 1. Weather

Temp.

9:00 a.m. 82°F. Clear-Sun  
 12:00 m. 89°F. " "  
 3:00 p.m. 94°F. " "

Moderate wind from Southwest.

## 12. Edging of Joints

Contraction Joints edged O.K.  
 No extra mortar or water required.

2. Station Start 546+31.8 at 5:15 a.m.  
 Station Stop 534+44.0 at 5:45 p.m.  
 Lin. Ft. 1187.8

## 13. Curing

a. One thickness burlap thoroughly wet during pour 8-1

b. Begin burlap removal 5:00 a.m. 8-2

c. Burlap removed 540+00 at 8:00 a.m. 8-2

d. Pav. thoro. wet 540+00 at 8:00 a.m. 8-2

e. Paper in place 542+00 at 8:00 a.m. 8-2

f. Pav. thoro. wet all paper in place 10:10 a.m. 8-2

g. Curing complete all paper removed 7:00 a.m. 8-5  
9:00 a.m. 8-5

## 3. See Daily Report

## 4. Temp. Conc. Final Finish (Broom)

9:30 (T. Con. 88° 1:10 (98° 3:15 (97°  
 a.m. (T. Air 81° p.m. (92° p.m. (92°

	a.m.	p.m.
5. Time	9:25 11:00	1:00 2:40
Placing	542+55 540+90	539+00 537+25
Screeds	542+60 540+95	539+00 537+30
	543+00 541+20	539+20 537+60
B-Float	543+10 541+50	539+30 537+70
	543+30 541+70	539+50 537+90
Belt	543+35 541+75	539+60 537+95
Broom	544+25 542+55	540+20 539+00
B'lap	545+40 542+60	540+40 539+30
W-B'lap	545+40 542+90	540+40 539+30
	11:20 a.m.	2:50 p.m.
	542+55	539+00

## 6. Condition of Subgrade

Sprinkled in front of Paver.  
 Subgrade throughout pour firm and uniform, uniform cut behind paver.

## 14. Report on Construction Equipment.

No delays.

## 15. Edges of Concrete

Slight honeycomb spots throughout lip curb.  
 No honeycomb in pavement edges.

## 16. Joint Sealing

All joints sealed 8-26.

## 7. Installation of Joints

Contraction Joint Cutter straightened, Joint Alignment O.K.  
 No load transference bars used in Contraction Joints.  
 Std. Load Transference Installed in construction joint at 534+44.0

## 17. Pictures

Form Grader 532+00. Paver 539+00

---- Remarks ----

Beams 52, 53, 54 538+75 at 1:00 p.m.  
 P.R.A. Beam Sec. No. 1 538+75 at 1:00 p.m.

## 8. Omit

## 9. See Joint Filler Depth Book

## 10. Longitudinal Joint Depth

Good Alignment

3/8"-7/16"-3/8"-3/8"-7/16"-7/16"-3/8"-3/8"

## 11. Description of Mix

a. Workability Plastic and Workable, uniform

b. Slump 2-1/2"

c. Mortar O.K. Good mortar roll on rear sensed.

d. Segregation None

e. Bleeding Slight near C.L. a.m.

f. Time req. to harden placed 542+55 = 9:25 a.m.  
 hardened " = 1:40 p.m.

4 hr. 15 min.



## COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Davies County Kentucky

Owensboro-Hartford FA-125-F(2)S

Daily Observations

Date August 2, 1940

## 1. Weather

Temp.

9:00 a.m. 84°F. Clear-Sun

12:00 m. 89°F. " "

3:00 p.m. 96°F. " "

Slight wind from East

## 12. Edging of Joints

Joint edging O.K.

No extra water or mortar required.

## 2. Station Start

534+44.0 at 5:05 a.m.

Station Stop

521+24.0 at 6:30 p.m.

Lin. Ft.

1320.0

## 13. Curing

One thickness burlap thoroughly wet during pour 8-2

b. Begin burlap

removal 5:00 a.m. 8-3c. Burlap removed 521+24.0 at 6:15 a.m. 8-3d. Pav. thoro. wet 521+24.0 at 6:20 a.m. 8-3e. Paper in place 526+00 at 8:00 a.m. 8-3f. Pav. thoro. wet all paper in place 10:00 a.m. 8-3g. Curing complete all paper removed 5:30 a.m. 8-6  
9:00 a.m. 8-6

## 3. See Daily Report

## 4. Temp. Conc. Final Finish (Broom)

9:40 (T. Con. 88° 12:00 (94° 3:00 (100°  
a.m. (T. Air 86° m. (89° p.m. (96°5. Time 8:20 10:20 12:50 1:55Placing 531+10 529+18 526+75 525+65Screeds 531+15 529+20 526+80 525+80531+40 529+40 527+00 526+00B-Float 531+45 529+70 527+25 526+05531+85 529+90 527+45 526+30Belt 531+90 530+00 527+50 526+55Broom 533+40 531+10 528+00 526+75B'lap 533+90 531+50 528+40 526+90W-B'lap 533+90 531+50 528+40 526+9010:35 a.m. 2:10 p.m.531+10 526+75

## 6. Condition of Subgrade

Subgrade sprinkled in front of paver. Soft, loose spot in subgrade entire width roadway. 527+25 to 527+90. Remainder of subgrade firm and uniform, uniform cut behind planer.

## 15. Edges of Concrete

Slight honeycomb spots in lip curb.  
No honeycomb in pavement edges.

## 7. Installation of Joints

Bad line on all contraction joints due to grade and B-Float distorting joint caps.

Std. Load Transference Installed in construction joint at 521+24.0

## 16. Joint Sealing

All joints sealed 8-26

## 17. Pictures

---- Remarks ----

Beams 55,56,57 523+00 at 4:00 p.m.

## 8. Omit

## 9. See Joint Filler Depth Book

## 10. Longitudinal Joint Depth

Good Alignment

3/8"-1/2"-7/16"-7/16"-5/8"-11/16"  
7/16"-1/2"

## 11. Description of Mix

a. Workability Plastic and Workable, uniform.b. Slump 2"c. Mortar O.K. Good mortar roll on rear screed.d. Segregation Nonee. Bleeding None a.m. or p.m.

f. Time req. to harden



COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Daviess County Kentucky

Owensboro-Hartford FA-125-F(2)S

Daily Observations

Date August 3, 1940

1. Weather

Temp.

9:00 a.m. 85°F. Clear

12:00 m. 92°F. "

3:00 p.m. 93°F. "

Slight wind from South.

No placing of Concrete.

12. Edging of Joints

2. Station Start

Station Stop

Lin. Ft.

13. Curing

a. One thickness burlap thoroughly wet during pour

b. Begin burlap removal

c. Burlap removed

d. Pav. thoro. wet

e. Paper in place

f. Pav. thoro. wet all paper in place

g. Curing complete all paper removed

3. See Daily Report

4. Temp. Conc. Final Finish (Broom)

5.

Time

Placing

Screeds

B-Float

Belt

Broom

B'lap

W-B'lap

14. Report on Construction Equipment.

6. Condition of Subgrade

15. Edges of Concrete

16. Joint Sealing

7. Installation of Joints

17. Pictures

----- Remarks -----

8. Omit

9. See Joint Filler Depth Book

10. Longitudinal Joint Depth

11. Description of Mix

a. Workability

b. Slump

c. Mortar

d. Segregation

e. Bleeding

f. Time req. to harden



# COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Daviess County Kentucky

Owensboro-Hartford, FA-125-F(2)S

Daily Observations

Date August 3, 1940

1. Weather  
Temp.

12. Edging of Joints

9:00 a.m. 85°F. Clear

12:00 m. 92°F. "

3:00 p.m. 93°F. "

Slight wind from South.

No placing of Concrete.

2. Station Start

13. Curing

Station Stop

a. One thickness burlap thoroughly wet during pour

Lin. Ft.

b. Begin burlap removal

3. See Daily Report

c. Burlap removed

4. Temp. Conc. Final Finish (Broom)

d. Pav. thoro. wet

e. Paper in place

f. Pav. thoro. wet all paper in place

g. Curing complete all paper removed

5.

Time

Placing

Screeds

B-Float

Belt

Broom

B'lap

W-B'lap

14. Report on Construction Equipment.

6. Condition of Subgrade

15. Edges of Concrete

16. Joint Sealing

7. Installation of Joints

17. Pictures

---- Remarks ----

8. Omit

9. See Joint Filler Depth Book

10. Longitudinal Joint Depth

11. Description of Mix

a. Workability

b. Slump

c. Mortar

d. Segregation

e. Bleeding

f. Time req. to harden



COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Daviess County Kentucky

Owensboro-Hartford - FA-125-F(2)S

Daily Observations

Date August 4, 1940 (Sunday)

1. Weather. . . . .  
Temp. . . . .  
9:00 a.m. 84°F. Cloudy  
12:00 m. 92°F. "  
3:00 p.m. 91°F. "  
Slight wind from Southeast.  
No concrete placed.

2. Station Start \_\_\_\_\_  
Station Stop \_\_\_\_\_  
Lin. Ft. \_\_\_\_\_

3. See Daily Report

4. Temp. Conc. Final Finish (Broom)

5. \_\_\_\_\_  
Time \_\_\_\_\_  
Placing \_\_\_\_\_  
Screeds \_\_\_\_\_  
B-Float \_\_\_\_\_  
Belt \_\_\_\_\_  
Broom \_\_\_\_\_  
B'lap \_\_\_\_\_  
W-B'lap \_\_\_\_\_

6. Condition of Subgrade

7. Installation of Joints

8. Omit

9. See Joint Filler Depth Book

10. Longitudinal Joint Depth

11. Description of Mix

a. Workability \_\_\_\_\_  
b. Slump \_\_\_\_\_  
c. Mortar \_\_\_\_\_  
d. Segregation \_\_\_\_\_  
e. Bleeding \_\_\_\_\_  
f. Time req. to harden \_\_\_\_\_

12. Edging of Joints

13. Curing  
a. One thickness burlap thoroughly wet during pour \_\_\_\_\_  
b. Begin burlap removal \_\_\_\_\_  
c. Burlap removed \_\_\_\_\_  
d. Pav. thoro. wet \_\_\_\_\_  
e. Paper in place \_\_\_\_\_  
f. Pav. thoro. wet all paper in place \_\_\_\_\_  
g. Curing complete all paper removed \_\_\_\_\_

14. Report on Construction Equipment.

15. Edges of Concrete

16. Joint Sealing

17. Pictures

---- Remarks ----



## COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Davies County Kentucky

Owensboro-Hartford FA-125-F(2)S

Daily Observations

Date August 5, 1940

## 1. Weather

Temp.

9:00 a.m. 86°F. Clear-Sun  
 12:00 m. 93°F. " "  
 3:00 p.m. 91°F. Alt. Cloudy-Sun  
 Moderate wind from Southwest.

## 12. Edging of Joints

Pavement 517+00 to 521 partially set before Joint edging, edges rough and uneven, remainder O.K. No extra mortar or water required.

2. Station Start 521+24.0 at 5:10 a.m.  
 Station Stop 508+80.0 at 6:00 p.m.  
 Lin. Ft. 1244.0 12 hr. 50 min.

## 13. Curing

a. One thickness burlap thoroughly wet during pour 8-5

b. Begin burlap

removal 5:00 a.m. 8-6

c. Burlap removed 508+80.0 at 8:40 a.m. 8-6

d. Pav. thoro. wet 508+80.0 at 8:40 a.m. 8-6

e. Paper in place 514+00 at 8:40 a.m. 8-6

f. Pav. thoro. wet all paper in

place 9:50 a.m. 8-6

g. Curing complete all paper

removed 11:00 a.m.) 8-8  
2:00 p.m.)

\* Curing Incomplete 508+80 to 515+00 24 hrs. burlap and water plus 44 hrs. paper from time of placing, error.

## 3. See Daily Report

## 4. Temp. Conc. Final Finish (Broom)

11:00 (T. Con. 92° 3:00 (96° 4:45 (95°  
 a.m. (T. Air 90° p.m. (91° p.m. (91°

5. a.m. p.m.  
 Time 9:15 10:35 2:00 3:40

Placing 517+00 515+60 512+95 511+15

Screeds 517+05 515+65 513+00 511+25

517+45 516+10 513+25 511+55

B-Float 517+65 516+50 513+40 511+85

517+85 516+75 513+60 512+20

Belt 517+90 516+80 513+80 512+35

Broom 518+60 517+00 513+90 512+95

B'lap 519+70 518+20 514+00 513+10

W-B'lap 519+70 518+20 514+00 513+10

11:00 a.m. 3:50 p.m.

517+00 512+95

## 6. Condition of Subgrade

Subgrade sprinkled in front of paver. Subgrade throughout days run firm and uniform, uniform cut behind paver.

## 14. Report on Construction Equipment.

No delays.

## 15. Edges of Concrete

No lip curb on this section.

No honeycomb in pavement edges.

## 16. Joint Sealing

All joints sealed 8-26.

## 7. Installation of Joints

Good Alignment on Contraction Joints throughout run.  
 Expansion Joint Installation 510+00 O.K. Std. Load Transference Installed in construction Joint 508+80.0

17. Pictures Cont. Jt. 514+00, Curing days run 512+50. Broom finish 512+50.  
 1 to 3

---- Remarks ----

Beams 58,59,60 512+75 at 2:30 p.m.

Paver running slow 12:15 p.m. to 12:45 p.m. due to truck delay.

Finished Sec. No. 1 4:15 p.m.

Started on Sec. No. 2.

## 8. Omit

## 9. See Joint Filler Depth Book

## 10. Longitudinal Joint Depth

Good Alignment  
 3/8"-5/16"-1/2"-3/8"-7/16"

## 11. Description of Mix

a. Workability Plastic and Workable, uniform.

b. Slump 1-1/2"

c. Mortar O.K. Good mortar roll on rear screed.

d. Segregation None

e. Bleeding Slight over entire surface a.m. & p.m.

f. Time req. to harden placed 515+00 - 11:45 a.m.

hardened "

5:30 p.m.

5 hr. 45 min.



COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Daviess County Kentucky

Owensboro-Hartford FA-125-F(2)S

Daily Observations

Date August 6, 1940

1. Weather

Temp.

9:00 a.m. 83°F. Alt. Cloudy-Sun

12:00 m. 82°F. Cloudy

3:00 p.m. 81°F. "

Very light rain 10:30 a.m. to 11:45 a.m. Slight Wind from Southwest.

12. Edging of Joints

Joint edging O.K.

No extra water or mortar required.

2. Station Start

508+80.0 at 5:30 a.m.

Station Stop

497+00.0 at 5:55 p.m.

Lin. Ft.

1180.0

13. Curing

a. One thickness burlap thoroughly wet during pour 8-6

b. Begin burlap

removal 508+80 at 5:00 a.m. 8-7

c. Burlap removed 497+00 at 7:30 a.m. 8-7

d. Pav. thoro. wet 497+00 at 7:40 a.m. 8-7

e. Paper in place 500+75 at 7:25 a.m. 8-7

f. Pav. thoro. wet all paper in place 9:00 a.m. 8-7

g. Curing complete all paper removed 3:30 a.m. 8-10  
6:00 a.m.)

3. See Daily Report

4. Temp. Conc. Final Finish (Broom)

9:40 (T. Con. 88° 12:40 (90° 3:10 (91°  
a.m. (T. Air 84° p.m. (82° p.m. (81°

5.

a.m.

p.m.

Time 9:25 10:30 12:55 2:35

Placing 506+50 505+28 502+70 501+00

Screeds 506+55 505+40 502+75 501+08

506+85 505+60 503+00 501+33

B-Float 506+90 505+90 503+10 501+50

507+20 506+05 503+35 501+70

Belt 507+40 506+10 503+50 501+75

Broom 507+60 506+50 504+40 502+70

B'lap 507+80 506+80 504+70 502+90

W-B'lap 507+80 506+80 504+70 502+90

11:15 a.m.

2:45 p.m.

506+50

502+70

6. Condition of Subgrade

Subgrade sprinkled in front of paver. Subgrade throughout days run firm and uniform, uniform cut behind paver.

14. Report on Construction Equipment.

P aver stopped 6:05 a.m. to 7:00 a.m. due to failure of water supply pump.

15. Edges of Concrete

No lip curb on this section. Slight scattered spots of honeycomb in pavement edges.

16. Joint Sealing

All joints sealed 8-26.

7. Installation of Joints

Good Alignment on contraction Joints throughout run.

Expansion Joint Installation 502+00 O.K.

Std. Load Transference Installed in construction Joint 497+00.0.

17. Pictures

---- Remarks ----

Beams 61, 62, 63 500+30 at 2:45 p.m.

8. Omit

9. See Joint Filler Depth Book

10. Longitudinal Joint Depth

Good Alignment

7/16"-1/2"-1/2"-9/16"-1/2"-1/2"

7/16"-7/16"-1/2"

11. Description of Mix

a. Workability Workable and Plastic, uniform.

b. Slump 1-1/2"

c. Mortar O.K. good mortar roll on rear screed.

d. Segregation None

e. Bleeding Slight over entire surface a.m. & p.m.

f. Time req. to harden placed 506+50 - 9:25 a.m.

hardened " - 2:30 p.m.

5 hr. 5 min.



## COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Daviss County Kentucky

Owensboro-Hartford FA-125-F(2)S

Daily Observations

Date August 7, 1940

## 1. Weather

Temp.

9:00 a.m. 81°F. Clear-Sun

12:00 m. 87°F. " "

3:00 p.m. 92°F. " "

Moderate wind from Southeast.

## 12. Edging of Joints

Joint edging O.K.

No extra water or mortar required.

## 2. Station Start

497+00.0 at 5:00 a.m.

Station Stop

482+32.3 at 6:15 a.m.

Lin. Ft.

1467.7

## 13. Curing

a. One thickness burlap thoroughly wet during pour 8-7

b. Begin burlap

removal 497+00 at 5:00 a.m. 8-8

c. Burlap removed 488+00 at 6:15 a.m. 8-8

d. Pav. thoro. wet 488+00 at 6:15 a.m. 8-8

e. Paper in place 488+00 at 7:30 a.m. 8-8

f. Pav. thoro. wet all paper in place 3:30 p.m. 8-8

g. Curing complete all paper

removed \*\* 488+00 to 482+32 One

thickness burlap continuously

sprinkled until 3:30 p.m. paper

applied 2:30 p.m. to 3:30 p.m. 8-8

## 3. See Daily Report

## 4. Temp. Conc. Final Finish (Broom)

9:40 (T. Con. 86° 12:00 (94° 3:00 (96°

a.m. (T. Air 81° m. (87° p.m. (92°

5. Time 9:25 10:55 2:30 4:15

Placing 492+00 490+25 486+40 484+35

Screeds 492+10 490+30 486+50 484+45

492+35 490+55 486+75 484+75

B-Float 492+65 490+70 486+85 485+00

492+95 490+95 487+10 485+20

Belt 493+10 491+15 487+30 485+25

Broom 494+60 492+00 488+00 486+40

B'lap 495+60 492+50 488+20 486+65

W-B'lap 495+60 492+50 488+20 486+65

11:15 a.m. 4:25 p.m.

492+00 486+40

## 6. Condition of Subgrade

Subgrade sprinkled in front of paver. Subgrade throughout days run firm and uniform, uniform cut behind paver.

## 14. Report on Construction Equipment.

No Delays.

## 7. Installation of Joints

Expansion Joint Installation

494+00 O.K.

Expansion Joint Installation

486+00 O.K.

Good Alignment on Contraction

Joints throughout run.

Std. Load Transference Installed

in Construction Joint 482+32.3

## 15. Edges of Concrete

No lip curb on this section.

No honeycomb in pavement edges.

## 16. Joint Sealing

All joints sealed 8-26.

## 17. Pictures

---- Remarks ----

Beams 64, 65, 66 490+50 at 10:45 a.m.

P.R.A. Beam Sec. No. 2 490+50 at 10:45 a.m.

\* Burlap placing behind because of truck breakdown.

Consistency of mix nonuniform throughout day, due to nonuniform moisture content of aggregate.

\*\* Cure Complete all paper removed

497+00 to 491+00 4:00 a.m. to 8:00 a.m. 8-11

Cure Complete all paper removed 491+00 to 482+32.3 9:00 a.m. to 10:00 a.m. 8-12.

## 8. Omit

## 9. See Joint Filler Depth Book

## 10. Longitudinal Joint Depth

Good Alignment

3/8"-7/16"-3/8"-5/16"-7/16"-5/8"-5/16"

5/16"-9/16"-9/16"

## 11. Description of Mix

a. Workability Plastic and Workable

b. Slump 2-1/4"

c. Mortar O.K. good mortar roll on rear screed.

d. Segregation None

e. Bleeding None

f. Time req. to harden placed 490+25 - 10:55 a.m. -

hardened "

3:35 p.m.

4 hr. 40 min.



## COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Daviness County Kentucky

Owensboro-Hartford FA-125-F(2)S

Daily Observations

Date Aug. 8, 19401. Weather  
Temp.

9:00 a.m. 79°F. Cloudy-Clear 9:25  
 12:00 m. 87°F. Clear-Sun a.m.  
 3:00 p.m. 89°F. " " " "  
 Moderate wind from Southeast

12. Edging of Joints

Joint edging O.K.

No extra water or mortar required.

2. Station Start

482+32.3 at 5:00 a.m.

Station Stop

469+21.4 at 5:25 p.m.

Lin. Ft.

1310.9

3. See Daily Report

4. Temp. Conc. Final Finish (Broom)

9:10 (T. Conc. 82° 12:00 (90° 3:00 (95°  
 a.m. (T. Air 80° m. (87° p.m. (89°

	a.m.	p.m.
Time	9:25 11:15 12:50 2:10	
Placing	477+85 476+00 474+15 472+75	
Screeds	477+90 476+05 474+20 472+80	
	478+20 476+35 474+40 473+00	
B-Float	478+30 476+55 474+65 473+25	
	478+55 476+85 474+90 473+50	
Belt	478+80 477+20 475+00 473+60	
Broom	480+00 477+85 475+45 474+15	
B'lap	480+50 478+10 476+40 474+50	
W-B'lap	480+50 478+10 476+40 474+50	
	11:30 a.m. 2:20 p.m.	
	477+85 474+15	

6. Condition of Subgrade

Subgrade sprinkled in front of  
 paver. Subgrade throughout this  
 run firm and uniform, uniform  
 out behind planer.

15. Edges of Concrete

Slight honeycomb spots in lip curb.  
 No honeycomb in pavement edges.

7. Installation of Joints

Expansion Joint Installation  
 478+00 O.K.  
 Expansion Joint Installation  
 474+00 O.K.  
 Expansion Joint Installation 470+00  
 O.K.  
 Good Alignment on Contraction  
 Joints.  
 Std. Load Transference Installed  
 in Construction Joint 469+21.4

17. Pictures Cutting Joint and Installing  
Filler Contraction Joint 470+40.

---- Remarks ----

Beams 67, 68, 69 475+25 at 11:30 a.m.

Consistency of mix nonuniform  
 throughout day due to nonuniform  
 moisture content of aggregate.  
 Two lines of hose sprinkling  
 pavement 469+21.4 to 478+25,  
 8-10-40 to 8-15-40.

Cure Complete all paper removed  
 482+32.3 to 478+25 10:00 a.m. to  
 11:00 a.m. 8-12.

All curing earth removed 478+25 to  
 469+21.4 1:00 p.m. to 2:00 p.m. 8-29.

8. Omit

9. See Joint Filler Depth Book

10. Longitudinal Joint Depth

Good Alignment

3/8"-1/2"-9/16"-1/2"-7/16"-1/2"  
 3/8"-3/8"

11. Description of Mix

a. Workability Plastic and Workable.

b. Slump 1-3/4"

c. Mortar O.K. good mortar roll on rear screed.

d. Segregation None

e. Bleeding Slight over entire surface a.m. &amp; p.m.

f. Time req. to harden placed 476+00 - 11:15 a.m.

hardened " - 5:00 p.m.

5 hr. 45 min.



## COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Daviness County Kentucky

Owensboro-Hartford FA-125-F(2)S

Daily Observations

Date August 9, 19401. Weather  
Temp.

9:00 a.m. 83°F. Clear-Sun  
 12:00 m. 90°F. " "  
 3:00 p.m. 86°F. Cloudy  
 Light rain 3:50 p.m. to 4:30 p.m.  
 Slight wind from Southwest.

## 12. Edging of Joints

Edging of Joints O.K.  
 No extra mortar or water required.

2. Station Start 469+21.4 at 4:55 a.m.  
 Station Stop 459+31.0 at 3:20 p.m.  
 Lin. Ft. 990.4

## 13. Curing

- a. One thickness burlap thoroughly wet during pour 8-9  
 b. Begin burlap removal 469+21.4 at 5:00 a.m. 8-10  
 c. Burlap removed 459+31 at 7:45 a.m. 8-10  
 d. Pav. thoro. wet 461+00 at 8:20 a.m. 8-10  
 e. Paper in place 461+60 at 8:20 a.m. 8-10  
 f. Pav. thoro. wet all paper in place 9:00 a.m. 8-10  
 g. Curing complete all paper removed 5:00 a.m. 8-14  
8:30 a.m. 8-14

## 3. See Daily Report

## 4. Temp. Conc. Final Finish (Broom)

9:00 (T. Con. 85° 12:00 (92° 3:00 (95°  
 a.m. (T. Air 83° m. (90° p.m. (86°

5. a.m.  
 Time 9:45 11:15  
 Placing 464+15 462+50  
 Screeds 464+20 462+55  
464+40 462+80  
 B-Float 464+80 463+05  
465+05 463+25  
 Belt 465+10 463+27  
 Broom 466+30 464+15  
 B'lap 466+70 464+60  
 W-B'lap 466+70 464+60  
11:40 a.m.  
464+15

## 6. Condition of Subgrade

Subgrade sprinkled in front of paver. Subgrade throughout this run firm and uniform, uniform cut behind planer.

## 14. Report on Construction Equipment.

Paver running slow 12:45 p.m. to 2:40 p.m. Water supply pump out of order. Vibrator out of order 12:00 m. to 3:20 p.m.

## 15. Edges of Concrete

No lip curb on this section. Pavement edge badly honeycombed Rt. of C.L. and slightly honeycombed Lt. of C.L. 459+31 to 462+00. No honeycomb in remainder of pavement edge.

## 16. Joint Sealing

All joints sealed 8-27.

## 7. Installation of Joints

Expansion Joint Installation  
 466+00 O.K.  
 Expansion Joint Installation  
 462+00 O.K.  
 Good Alignment on Contraction Joints.  
 Std. Load Transference Installed in Construction Joint 459+31.0

## 17. Pictures

---- Remarks ----

Beams 70, 71, 72 463+00 at 10:30 a.m.  
 P.R.A. Beam Sec. No. 3 463+00 at 10:30 a.m.  
 Curing water lines shut off enabling paver to run normal 2:40 p.m. to 3:20 p.m. Placing of concrete stopped at 3:20 p.m. and curing water lines opened.

## 8. Omit

## 9. See Joint Filler Depth Book

## 10. Longitudinal Joint Depth

Good Alignment  
5/8"-5/8"-5/8"-1/2"-1/2"-5/8"  
7-16"

## 11. Description of Mix

- a. Workability Workable and plastic, uniform.  
 b. Slump 1-3/4"  
 c. Mortar O.K. Good mortar roll on rear screed.  
 d. Segregation None  
 e. Bleeding None a.m. Slight over entire surface p.m.  
 f. Time req. to harden placed 464+15 - 9:45 a.m.  
hardened " 3:15 p.m.  
5 hr. 30 min.



## COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Daviness County Kentucky

Owensboro-Hartford FA-125-F(2)S

Daily Observations

Date August 10, 1941

## 1. Weather

Temp.

9:00 a.m. 77°F. Cloudy  
 12:00 m. 83°F. "  
 3:00 p.m. 85°F. "  
 Slight wind from Southwest.

## 12. Edging of Joints

Edging of Joints O.K.

No extra water or mortar required.

## 2. Station Start

Station Stop

Lin. Ft.

459+31.0 at 5:30 a.m.

447+90.5 at 5:00 p.m.

1140.5

## 13. Curing

a. One thickness burlap thoroughly wet during pour 8-10

b. Begin burlap

removal 459+31.0 at 5:00 a.m. 8-11

c. Burlap removed 450+25 at 7:55 a.m. 8-11

d. Pav. thoro. wet 451+00 at 7:55 a.m. 8-11

e. Paper in place 452+75 at 7:55 a.m. 8-11

f. Pav. thoro. wet all paper in place 8:45 a.m. 8-11

g. Curing complete all paper removed 8:30 a.m. 10:30 a.m. 8-14.

## 3. See Daily Report

## 4. Temp. Conc. Final Finish (Broom)

9:15 (T. Con. 82° 12:00 (85° 3:00 (90°  
 a.m. (T. Air 77° m. (83° p.m. (85°

## 5.

Time

Placing

Screeds

B-Float

Belt

Broom

B'lap

W-B'lap

	a.m.	p.m.
Time	9:20 11:20 1:10 3:15	
Placing	455+60 453+45 452+00 449+70	
Screeds	455+65 453+50 452+05 449+75	
B-Float	455+95 454+10 452+55 450+10	
Belt	456+15 454+30 452+75 450+30	
Broom	458+00 455+60 453+80 452+00	
B'lap	458+80 456+00 454+20 452+10	
W-B'lap	458+80 456+00 454+20 452+10	
	11:50 a.m. 3:20 p.m.	
	455+60 452+00	

## 6. Condition of Subgrade

Subgrade sprinkled in front of paver. Soft, loose spot in subgrade entire width rdwy. 459+00 to 459+25. Remainder of subgrade firm and uniform, uniform cut behind planer.

## 14. Report on Construction Equipment.

New engine for vibrator installed, operating O.K. Paver stopped 11:30 a.m. to 11:50 a.m., repair bucket.

## 15. Edges of Concrete

No lip curb on this section.

No honeycomb in pavement edges.

## 16. Joint Sealing

All joints sealed 8-27.

## 7. Installation of Joints

Exp. Jt. Installation 458+00 O.K.  
 " " " 454+00 O.K.  
 " " " 452+80 O.K.  
 " " " 451+60 O.K.  
 " " " 450+40 O.K.  
 " " " 449+20 O.K.  
 " " " 448+00 O.K.

## 17. Pictures

---- Remarks ----

Beams 73, 74, 75 451+50 at 1:45 p.m.

Good Alignment on contraction joints.  
 Change in construction of contraction joints 450+21. Two steel strips 1-1/2" x 1/4" x 10' inserted 1/4" below surface, no filler used. Std. Load Trans. 447+90.5

## 8. Omit

## 9. See Joint Filler Depth Book

## 10. Longitudinal Joint Depth

Good Alignment

9/16"-1/2"-5/8"-5/8"-7/16"-1/2"  
 9/16"-1/2"

## 11. Description of Mix

a. Workability

b. Slump

c. Mortar

d. Segregation

e. Bleeding

f. Time req. to harden

Plastic and Workable, uniform.

1-1/2"

O.K. Good mortar roll on rear screed.

None

Over entire surface a.m., slight p.m.

placed 455+60 -

hardened

9:20 a.m.

3:00 p.m.

5 hr. 40 min.



# COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Daviess County Kentucky

Qwensboro-Hartford FA-125-F(2)S

Daily Observations

Date August 11, 1940 (Sunday)

1. Weather  
Temp.

12. Edging of Joints

9:00 a.m. 86°F. Clear

12:00 m. 90°F. "

3:00 p.m. 91°F. Cloudy

Slight wind from South.

2. Station Start

Station Stop

Lin. Ft.

13. Curing

a. One thickness burlap thoroughly wet during pour

b. Begin burlap removal

c. Burlap removed

d. Pav. thoro. wet

e. Paper in place

f. Pav. thoro. wet all paper in place

g. Curing complete all paper removed

3. See Daily Report

4. Temp. Conc. Final Finish (Broom)

5.

Time

Placing

Screeds

B-Float

Belt

Broom

B'lap

W-B'lap

14. Report on Construction Equipment.

6. Condition of Subgrade

15. Edges of Concrete

16. Joint Sealing

7. Installation of Joints

17. Pictures

---- Remarks ----

8. Omit

9. See Joint Filler Depth Book

10. Longitudinal Joint Depth

11. Description of Mix

a. Workability

b. Slump

c. Mortar

d. Segregation

e. Bleeding

f. Time req. to harden



## COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Daviess County Kentucky

Owensboro-Hartford FA-125-F(2)S

Daily Observations

Date August 12, 1940

## 1. Weather

Temp.

9:00 a.m. 86°F. Clear

12:00 m. 94°F. "

3:00 p.m. 94°F. "

Moderate wind a.m., hard wind  
from Southeast.2. Station Start 447+90.5 at 4:50 a.m.  
Station Stop 433+82.5 at 6:00 p.m.  
Lin. Ft. 1408.0

## 3. See Daily Report

## 4. Temp. Conc. Final Finish (Broom)

9:00 (T. Con. 86° 12:00 (97° 3:00 (97°  
a.m. (T. Air 86° m. (94° p.m. (94°

	a.m.		p.m.	
5. Time	8:40	10:10	2:35	3:40
Placing	444+14	442+50	437+74	436+44
Screeds	444+15	442+55	437+80	436+50
	444+46	442+86	438+10	436+75
B-Float	444+80	443+10	438+20	437+00
	445+10	443+40	438+50	437+20
Belt	445+20	443+50	438+60	437+25
Broom	446+10	444+14	438+75	437+74
B'lap	446+40	444+70	439+60	438+30
W-B'lap	446+40	444+70	439+60	438+30
	10:30 a.m.		4:00 p.m.	
	444+14		437+74	

## 6. Condition of Subgrade

Subgrade sprinkled in front of  
paver. Subgrade throughout this  
run firm and uniform, uniform cut  
behind planer.

## 7. Installation of Joints

All Expansion Joint  
Installations O.K.  
Standard Load Transference  
Installed in First Contraction  
Joint Sec. 5 440+00. Contraction  
Joints Formed by Steel Strips  
O.K. Better alignment than by use  
of filler and caps. Standard Load  
Transference Installed in Con-  
struction Joint 433+82.5

## 8. Omit

## 9. See Joint Filler Depth Book

## 10. Longitudinal Joint Depth

Good Alignment  
1/2"-9/16"-5/8"-5/8"-9/16"-5/8"  
9/16"-1/2"-5/8"

## 11. Description of Mix

a. Workability Plastic and Workable, uniform.  
b. Slump 1-3/4"  
c. Mortar O.K. Good mortar roll on rear screed.  
d. Segregation None  
e. Bleeding None a.m. or p.m.  
f. Time req. to harden \_\_\_\_\_

## 12. Edging of Joints

Joint edging O.K.

No extra water or mortar required.

## 13. Curing

a. One thickness burlap thoroughly wet  
during pour 8-12  
b. Begin burlap  
removal 447+90.5 at 5:30 a.m. 8-13  
c. Burlap removed 433+82.5 at 6:30 a.m. 8-13  
d. Pav. thoro. wet 433+82.5 at 8:30 a.m. 8-13  
e. Paper in place 440+00 at 8:00 a.m. 8-13  
f. Pav. thoro. wet all paper in  
place 11:20 a.m. 8-13  
g. Curing complete all paper 6:00 a.m.) 8-16  
removed 10:00 a.m.)

## 14. Report on Construction Equipment.

No Delays.

## 15. Edges of Concrete

No lip curb on this section.  
No honeycomb in pav. edges.

## 16. Joint Sealing

All joints sealed 8-27.

17. Pictures Inst. Cont. Jt.

---- Remarks ----

Beams 76, 77, 78 441+00 at 12:30 p.m.  
P.R.A. Beam Sec. No. 4 441+00 at  
12:30 p.m.  
Finished Sec. No. 4 12:30 p.m.,  
started on Sec. 5.  
New curing paper 440+00 to 433+82.5



## COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Daviss County Kentucky

Owensboro-Hartford FA-125-F(2)S

Daily Observations

Date August 13, 19401. Weather  
Temp.

9:00 a.m. 78°F. Cloudy

12:00 m. 80°F. "

3:00 p.m. 84°F. "

Light rain 7:30 a.m. to 1:00 p.m.

No Wind.

2. Station Start 433+82.5 at 5:00 a.m.Station Stop 429+21.0 at 11:30 a.m.Lin. Ft. 461.5

3. See Daily Report

4. Temp. Conc. Final Finish (Broom)

9:00(T. Conc. 83° 12:00(87°  
a.m.(T. Air 78° m. (80°

5.	
Time	<u>10:30 a.m.</u>
Placing	<u>430+29</u>
Screeds	<u>430+30</u>
	<u>430+55</u>
B-Float	<u>430+70</u>
	<u>430+90</u>
Belt	<u>431+30</u>
Broom	<u>432+00</u>
B'lap	<u>432+00</u>
W-B'lap	<u>432+00</u>

6. Condition of Subgrade

Subgrade sprinkled in front of paver. Subgrade throughout this run firm and uniform, uniform cut behind planer.

7. Installation of Joints

All Expansion Joint Installations O.K. Good Alignment on Contraction Joints. Standard Load Transference Installed in Construction Joint 429+21.0

8. Omit

9. See Joint Filler Depth Book

10. Longitudinal Joint Depth

Good Alignment

5/8"-5/8"-7/16"-9/16"-1/2"-7/16"

11. Description of Mix

a. Workability Plastic and Workable, uniform.b. Slump No test.c. Mortar O.K. Good mortar roll on rear screed.d. Segregation Nonee. Bleeding Not distinguishable.

f. Time req. to harden

12. Edging of Joints

Joint edging O.K.

No extra water or mortar required.

13. Curing

a. One thickness burlap thoroughly wet during pour 8-13b. Begin burlap removal 433+82.5 at 6:00 a.m. 8-14c. Burlap removed 429+21.0 at 7:00 a.m. 8-14d. Pav. thoro. wet 429+21.0 at 7:00 a.m. 8-14e. Paper in place 431+00.0 at 7:15 a.m. 8-14f. Pav. thoro. wet all paper in place 8:00 a.m. 8-14g. Curing complete all paper removed 5:00 a.m. 8-17  
6:00 a.m. 8-17

14. Report on Construction Equipment.

No delays.

15. Edges of Concrete

No lip curb on this section.

No honeycomb in pavement edges.

16. Joint Sealing

All joints sealed 8-27.

17. Pictures

----- Remarks -----

No beams or cylinders.

Paver stopped 8:00 a.m. to 9:20 a.m. on account of light rain. Concrete covered with burlap.



## COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Daviness County Kentucky

Owensboro-Hartford FA-125-F(2)S

Daily Observations

Date August 14, 19401. Weather  
Temp.

9:00 a.m. 86°F. Clear  
 12:00 m. 92°F. "  
 3:00 p.m. 89°F. Cloudy  
 No wind.

12. Edging of Joints

Joint edging O.K.

No extra water or mortar required.

2. Station Start 429+21.0 at 5:10 a.m.  
 Station Stop 419+81.0 at 5:45 p.m.  
 Lin. Ft. 940.0

13. Curing

a. One thickness burlap thoroughly wet during pour 8-14

b. Begin burlap

removal 429+21.0 at 5:30 a.m. 8-15c. Burlap removed 421+30 at 7:45 a.m. 8-15d. Pav. thoro. wet 422+00 at 7:45 a.m. 8-15e. Paper in place 423+20 at 7:45 a.m. 8-15f. Pav. thoro. wet all paper in place 9:30 a.m. 8-15g. Curing complete all paper removed 7:00 a.m. 8-19  
9:00 a.m. 8-19

3. See Daily Report

4. Temp. Conc. Final Finish (Broom)

9:00 (T. Con. 88° 3:00 (96° 6:00 (91°  
 a.m. (T. Air 86° p.m. (89° p.m. (86°

	a.m.	p.m.
5. Time	8:00 9:40 4:00 5:50	
Placing	426+12 424+60 421+35 419+81	
Screeds	426+20 424+70 421+40 419+86	
	426+45 425+10 421+65 420+15	
B-Float	426+65 425+25 421+80 420+20	
	426+90 425+45 422+00 420+45	
Belt	427+00 425+50 422+02 420+50	
Broom	428+80 426+12 423+25 421+35	
B'lap	None 426+50 423+50 421+80	
W-B'lap	None 426+50 423+50 421+80	
	10:05 a.m. 6:30 p.m.	
	426+12 421+35	

14. Report on Construction Equipment.

Paver stopped at 424+06, 10:30 a.m.  
 to 1:30 p.m. repairing vibrator.

6. Condition of Subgrade

Subgrade sprinkled in front of  
 paver. Subgrade throughout days run  
 firm and uniform, uniform cut  
 behind planer.

15. Edges of Concrete

No honeycomb in pavement edges.

7. Installation of Joints

Dowel holder on Lt. of C.L.  
 damaged, Cont. Jt. 425+80

All Joint Installations O.K.  
 All Dowel Holders O.K. (See  
 above note.)

16. Joint Sealing

All joints sealed 8-27.

17. Pictures

---- Remarks ----

Beams 79.80.81 427+00 at 8:00 a.m.  
 P.R.A. Beam Sec. No. 5 427+00 at  
 8:00 a.m.

Begin 70 lb. wire fabric 425+20

8. Omit

9. See Joint Filler Depth Book

10. Longitudinal Joint Depth

Good Alignment  
 5/8"-9/16"-5/8"-9/16"-9/16"-5/8"  
 9/16"-9/16"

11. Description of Mix

a. Workability Plastic and workable.b. Slump 1-1/2"c. Mortar Correct amount, good roll on rear screed.d. Segregation Nonee. Bleeding Slight in scattered spots a.m. and p.m.

f. Time req. to harden



## COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Daviness County Kentucky

Owensboro-Hartford FA-125-F(2)S

Daily Observations

Date August 15, 19401. Weather  
Temp.

9:00 a.m. 87°F. Clear  
 12:00 m. 92°F. "  
 3:00 p.m. 95°F. "  
 Slight wind from Southeast.

12. Edging of Joints

Joint edging O.K.

No extra water or mortar required.

2. Station Start 419+81.0 at 5:00 a.m.  
 Station Stop 406+81.4 at 6:05 p.m.  
 Lin. Ft. 1299.6

13. Curing

a. One thickness burlap thoroughly wet during pour 8-15b. Begin burlap removal 419+81.0 at 5:00 a.m. 8-16c. Burlap removed 409+00 at 7:45 a.m. 8-16d. Pav. thoro. wet 409+80 at 7:45 a.m. 8-16e. Paper in place 410+50 at 7:45 a.m. 8-16f. Pav. thoro. wet all paper in place 9:00 a.m. 8-16g. Curing complete all paper removed 9:00 a.m. 8-19  
11:30 a.m. 8-19

3. See Daily Report

4. Temp. Conc. Final Finish (Broom)

9:00 (T. Con. 89° 12:00 (95° 3:00 (101°  
 a.m. (T. Air 87° m. (92° p.m. (95°

5. Time 8:45 a.m. 11:00 12:45 p.m. 2:00  
 Placing 416+20 413+75 412+00 410+60  
 Screeds 416+30 413+90 412+10 410+70  
416+70 414+15 412+35 411+00  
 B-Float 416+75 414+35 412+40 411+05  
416+95 414+65 412+80 411+35  
 Belt 417+00 414+75 412+90 411+75  
 Broom 419+20 416+20 413+20 412+00  
 B'lap 419+30 416+40 413+75 412+10  
 W-B'lap 419+30 416+40 413+75 412+10  
11:05 a.m. 2:10 p.m.  
416+20 412+00

14. Report on Construction Equipment.

Unsatisfactory broom finish 417+50 to  
 419+81, broken broom. New broom  
 secured. Planer adjusted to 7"  
 uniform thickness 410+21.

6. Condition of Subgrade

Soft loose spot entire width roadway  
 at 418+40 to 418+70, 409+00 to  
 410+50, 406+50 to 407+80.  
 Remainder of subgrade firm and  
 uniform.

15. Edges of Concrete

No honeycomb in pavement edges.

7. Installation of Joints

All Joint Installations O.K.  
 All Dowel Holders O.K.

Last contraction joint with  
 load transfer bars 410+21.

16. Joint Sealing

All joints sealed 8-28.

17. Pictures

---- Remarks ----

Beams 82, 83, 84 417+00 at 9:00 a.m.  
 P.R.A. Beam Sec. No. 6 417+00  
 at 9:00 a.m.  
 End wire mesh in Sec. 6 410+21.  
 Finished Sec. 6 3:00 p.m.,  
 started on Sec. 7.

8. Omit

9. See Joint Filler Depth Book

10. Longitudinal Joint Depth

3/8"-5/8"-1/2"-9/16"-5/8"-3/4"  
5/8"-5/8"

11. Description of Mix

a. Workability Plastic and workable.b. Slump 1-1/2"c. Mortar Sufficient, good mortar roll on rear screed.d. Segregation Nonee. Bleeding Slight scattered spots a.m. and p.m.

f. Time req. to harden



## COOPERATIVE INVESTIGATION OF JOINT SPACING IN CONCRETE PAVEMENTS.

Daviss County Kentucky

Owensboro-Hartford FA-125-F(2)S

Daily Observations

Date August 16, 1940

1. Weather  
Temp.  
9:00 a.m. 90° Clear  
12:00 m. 94° Cloudy  
3:00 p.m. 79° Cloudy  
Slight Wind from Southwest
2. Station Start 406+81.4 at 5:00 a.m.  
Station Stop 397+49.4 at 3:10 p.m.  
Lin. Ft. 932.0
3. See Daily Report
4. Temp. Conc. Final Finish (Broom)  
9:00 (T. Con. 90° 12:00 (98° 3:00 (94°  
a.m. (T. Air 90° m. (94° p.m. (79°
- |         | a.m.                        | p.m. |
|---------|-----------------------------|------|
| Time    | 9:00 10:30 12:15 1:30       |      |
| Placing | 403+50 401+90 400+00 398+80 |      |
| Screeds | 403+60 402+00 400+05 398+90 |      |
|         | 403+80 402+25 400+45 399+15 |      |
| B-Float | 404+10 402+45 400+75 399+25 |      |
|         | 404+30 402+70 401+10 399+45 |      |
| Belt    | 404+65 402+75 401+15 399+50 |      |
| Broom   | 405+40 403+50 401+35 400+00 |      |
| B'lap   | 405+75 404+20 401+50 400+40 |      |
| W-B'lap | 405+75 404+20 401+50 400+40 |      |
|         | 10:50 a.m. 1:40 p.m.        |      |
|         | 403+50 400+00               |      |
5. Condition of Subgrade  
Soft loose spot entire width rdwy.  
at 399+70 to 400+00. Remainder of  
subgrade firm and uniform.
6. Installation of Joints  
All Joint Installations O.K.  
Expansion joint filler without  
dowel bars held in place by steel  
pins driven on each side of filler  
Sec. 7. Alignment of completed  
joints is satisfactory.
7. Omit
8. See Joint Filler Depth Book
9. Longitudinal Joint Depth  
Good Alignment  
15/16"-1"-1-1/4"-13/16"-7/8"-3/4"-7/8"
10. Description of Mix  
a. Workability Plastic and Workable  
b. Slump 1-1/2"  
c. Mortar Sufficient, good mortar roll on rear screed.  
d. Segregation None  
e. Bleeding Slight scattered spots a.m. and p.m.  
f. Time req. to harden \_\_\_\_\_
11. Edging of Joints  
Joint Edging O.K.  
No extra water or mortar required.
12. Curing  
a. One thickness burlap thoroughly wet  
during pour 8-16  
b. Begin burlap  
removal 406+81.4 at 5:00 a.m. 8-17  
c. Burlap removed 397+49.4 at 6:45 a.m. 8-17  
d. Pav. thoro. wet 397+49.4 at 6:45 a.m. 8-17  
e. Paper in place 402+00 at 6:45 a.m. 8-17  
f. Pav. thoro. wet all paper in  
place 8:00 a.m. 8-17  
g. Curing complete all paper  
removed 11:30 a.m. 8-19  
1:30 p.m. 8-19
13. Report on Construction Equipment.  
No delays.
14. Edges of Concrete  
No honeycomb in pavement edges.
15. Joint Sealing  
All joints sealed 8-28.
16. Pictures
- Remarks -----  
Beams 85, 86, 87 402+50 at 10:00 a.m.  
P.R.A. Beam Sec. No. 7 402+50 at  
10:00 a.m.  
70 lb. wire mesh installed in odd  
length section from beginning of  
project 397+49.4 to 397+61.1  
Placing of concrete on project com-  
pleted at 397+49.4, 3:10 p.m.  
August 16, 1940.